

# JONES & BEACH ENGINEERS INC.

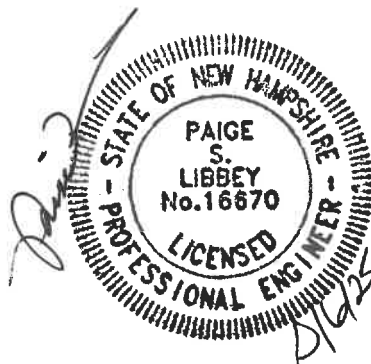
## DRAINAGE ANALYSIS

## EROSION AND SEDIMENT CONTROL PLAN

**35 Madbury Road  
Tax Map 106 / Lot 19  
Durham, NH 03824**

**Prepared for:**

**DWS 35, LLC  
288 Calef Highway  
Lee, NH 03861**



**Prepared by:**

**Jones & Beach Engineers, Inc.  
85 Portsmouth Avenue  
P.O. Box 219  
Stratham, NH 03885  
(603) 772-4746  
July 2, 2025  
Rev. #1 – August 6, 2025  
JBE Project No. 25073**

## 1. EXECUTIVE SUMMARY

The purpose of this project is to construct a parking addition and associated driveway on Town of Durham Tax Map 106, Lot 19. The development will include the construction of the parking and driveway area with associated stormwater management practices. Two models were compiled, one for the area in its existing (pre-development) condition, and a second for its proposed (post-development) condition. The analysis was conducted using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment.

A summary of the existing and proposed conditions peak rates of runoff is as follows:

	<b>EXECUTIVE SUMMARY TABLE – PEAK FLOW</b>							
<b>Analysis Point</b>	<b>1 Inch (cfs)</b>		<b>2 Year (cfs)</b>		<b>10 Year (cfs)</b>		<b>17 Year (cfs)</b>	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.35	0.33	2.94	2.84	5.36	5.23	6.06	5.90
Analysis Point #2	0.03	0.01	0.27	0.06	0.50	0.11	0.57	0.11

A summary of the existing and proposed conditions peak volumes of runoff is as follows:

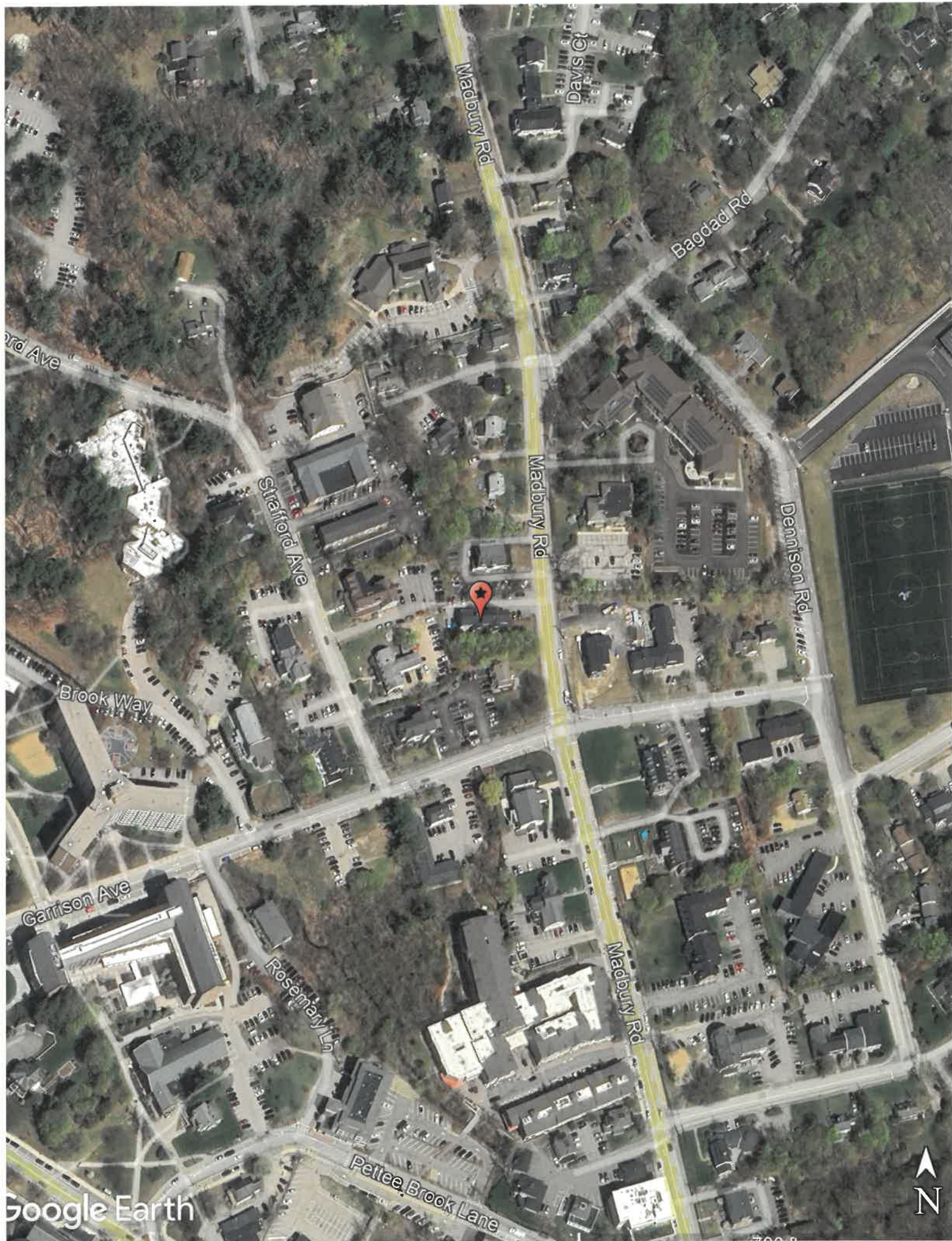
	<b>EXECUTIVE SUMMARY TABLE – VOLUME</b>							
<b>Analysis Point</b>	<b>1 Inch (cf)</b>		<b>2 Year (cf)</b>		<b>10 Year (cf)</b>		<b>17 Year (cf)</b>	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.039	0.037	0.296	0.291	0.552	0.552	0.628	0.630
Analysis Point #2	0.002	0.001	0.020	0.005	0.037	0.008	0.043	0.010

\* A minor increase in the post-construction volume of runoff towards Analysis Point #1 throughout the 17-Year storm event is due to the proposed construction of the driveway and parking area. Infiltration in this location is limited due to a poor infiltration rate and relatively high water table, however, stormwater discharged from the proposed development will be treated and will not negatively impact abutting property owners as the increase is only 0.002 C.F. at the most. Peak discharge is also decreased to this Analysis Point throughout all modeled storm events.

Section 15.5.3(c) in the Durham, NH Site Plan Regulations states “For sites meeting the definition of a redevelopment project and having more than 40% existing impervious surface coverage, stormwater shall be managed for water quality in accordance with the following technique: Implement other LID (Low impact development) techniques onsite to the maximum extent practicable to provide treatment for at least 50% of the entire site area”. Since the existing site is already developed and is over the 40% impervious threshold, this project qualifies to meet the aforementioned criteria listed within the regulation. The existing site contains no stormwater management practices and has an impervious area of ±8,339 S.F. requiring treatment under current regulations. The proposed site adds ±684 S.F. of impervious area and the proposed porous asphalt will capture and treat ±5,037 S.F. of the now ±9,023 S.F. needing treatment, providing treatment to over 50% of the required level stated in the regulation. The porous asphalt will also capture and treat ±1,400 S.F. of offsite impervious area, previously left untreated in the pre-construction condition. Therefore, the drainage design intent for this site is to effectively treat stormwater from at least 50% of impervious surfaces of the proposed site. This has been accomplished through the use of porous asphalt to treat runoff from impervious surfaces.

In addition, the potential for increased erosion and sedimentation is handled by way of a riprap outlet protection apron and silt fence. Abutting property owners will suffer minimal impact resultant from this development.





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## **2. DRAINAGE ANALYSIS**

### **3.1 INTRODUCTION**

The purpose of this project is to construct a parking addition and associated driveway on Town of Durham Tax Map 106, Lot 19. The development will include the construction of the parking and driveway area with associated stormwater management practices.

### **3.2 METHODOLOGY**

The existing and proposed watersheds were modeled utilizing HydroCad stormwater software, version 9.10. The watersheds were analyzed utilizing the SCS TR-20 methodology for hydrograph development and the TR-55 methodology for Time of Concentration ( $T_c$ ) determination. The Dynamic-Storage-Indicating method for reach and pond routing was utilized. Type III, 24-hour hydrographs were developed for the 1-inch, 2-year, 10-year, and 17-year storm events, corresponding to rainfall events of 1.00", 3.30", 5.29", 5.87" respectively. The 17-Year storm event was determined via interpolation between the published 10-Year and 25-Year rainfall events.

Existing topography and site features were obtained through on-ground topography completed by Jones & Beach Engineers. Existing soil conditions were derived from NRCS Web Soil Survey.

### **3.3 EXISTING CONDITIONS ANALYSIS**

The study area consists of the subject property and upstream contributing area. The study area contains  $\pm 1.75$  acres including offsite contributing areas. The existing site is currently developed and includes a dwelling utilized by one of the fraternities of the University of New Hampshire as well as a paved driveway and parking area. The surrounding area is mostly developed and contains other dwellings, paved surfaces, woods, and grass cover. The existing site contains a high point that traverses North to South, resulting in the Analysis Points as defined below.

The entirety of the soils for this site are described as Hydrological Soils "D".

Two (2) Analysis Points (AP) were defined for this project.

Analysis Point #1 (AP1) represents the Southwest corner of the subject lot. Runoff that reaches this point flows onto the abutting property. Subcatchment 100 represents the area that flows to this Analysis Point.

Analysis Point #2 (AP2) represents the Southeast corner of the subject. Runoff that reaches this point flows onto Madbury Road, where a network of catch basins is in place to capture and transport stormwater. Subcatchment 101 represents the area the flows to this Analysis Point.

### **3.4 PROPOSED CONDITIONS ANALYSIS**

The proposed site will include the construction of the proposed parking area, driveway, and stormwater management practices.

The addition of the proposed impervious paved areas causes an increase in the curve number ( $C_n$ ) and a decrease in the time of concentration ( $T_c$ ), the net result being a potential increase in peak rates of

runoff from the site. To effectively treat the subsequent stormwater runoff to the extent practicable and required under current regulations, the following Best Management Practices (BMP's) have been employed at the Analysis Points as follows:

Subcatchment 200 represents the area of land that flows directly to Analysis Point #1, similarly to Subcatchment 100 in the pre-construction model.

Subcatchment 201 represents the area of land that flows directly to Analysis Point #2, similarly to Subcatchment 101 in the pre-construction model.

Runoff from the southern portion of the roof and the majority of the proposed parking area and driveway, represented by Subcatchment 202, will be captured and treated via porous asphalt (Pond P1) before discharging via culvert and flowing overland (Reach 20R) to Analysis Point #1. Infiltration has also been modeled within the porous asphalt system. The infiltration rate was determined by attaining the lowest published Ksat value for the in-situ soil from the Ksat Values for New Hampshire Soils sponsored by the Society of Soil Scientists of Northern New England. In this case, 0.6 in/hr is the lowest published value and a factor of safety of two was applied in order to arrive at a Ksat value of 0.3 in/hr used in the model.

### 3.6 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures or properties by way of stormwater runoff or siltation if properly constructed in accordance with this Drainage Analysis and approved project plan set. Appropriate steps will be taken to control erosion and sedimentation; these will be accomplished through the construction of a drainage system consisting of site grading, porous asphalt, and a riprap outlet protection apron. The use of Best Management Practices developed by the State of New Hampshire have been utilized in the design of this system.

Respectfully Submitted,  
**JONES & BEACH ENGINEERS, INC.**



Nicholas Lorenz  
Project Engineer

## APPENDIX 3.7 DRAINAGE CALCUALTIONS

### PRE-DEVELOPMENT CONDITIONS ANALYSIS

1-Inch 24-Hour Complete Analysis  
2-Year 24-Hour Summary Analysis  
10-Year 24-Hour Complete Analysis  
17-Year 24-Hour Summary Analysis





EX-WS-100



ANALYSIS POINT #1



EX-WS-101



ANALYSIS POINT #2



**Routing Diagram for EXISTING**

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### Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.586	80	>75% Grass cover, Good, HSG D (100, 101)
0.164	98	Gravel, HSG D (100)
0.015	98	Patio/Stairs, HSG D (100)
0.461	98	Pavement, HSG D (100, 101)
0.245	98	Roof, HSG D (100, 101)
0.009	98	Sidewalk, HSG D (100, 101)
0.000	98	Stairs, HSG D (101)
0.274	77	Woods, Good, HSG D (100, 101)
<b>1.754</b>	<b>89</b>	<b>TOTAL AREA</b>

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### Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
1.754	HSG D	100, 101
0.000	Other	
<b>1.754</b>		<b>TOTAL AREA</b>

**EXISTING***Type III 24-hr 1 INCH Rainfall=1.00"*

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment100: EX-WS-100**Runoff Area=71,445 sf 51.45% Impervious Runoff Depth>0.28"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=0.35 cfs 0.039 af**Subcatchment101: EX-WS-101**Runoff Area=4,964 sf 44.56% Impervious Runoff Depth>0.25"  
Flow Length=188' Tc=6.0 min CN=88 Runoff=0.03 cfs 0.002 af**Link AP1: ANALYSISPOINT #1**Inflow=0.35 cfs 0.039 af  
Primary=0.35 cfs 0.039 af**Link AP2: ANALYSISPOINT #2**Inflow=0.03 cfs 0.002 af  
Primary=0.03 cfs 0.002 af**Total Runoff Area = 1.754 ac Runoff Volume = 0.041 af Average Runoff Depth = 0.28"**  
**49.00% Pervious = 0.860 ac 51.00% Impervious = 0.895 ac**

**EXISTING***Type III 24-hr 1 INCH Rainfall=1.00"*

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**Summary for Subcatchment 100: EX-WS-100**

Runoff = 0.35 cfs @ 12.27 hrs, Volume= 0.039 af, Depth> 0.28"  
Routed to Link AP1 : ANALYSIS POINT #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 1 INCH Rainfall=1.00"

	Area (sf)	CN	Description
	11,440	77	Woods, Good, HSG D
*	10,379	98	Roof, HSG D
*	267	98	Sidewalk, HSG D
*	640	98	Patio/Stairs, HSG D
*	18,321	98	Pavement, HSG D
*	7,149	98	Gravel, HSG D
	23,249	80	>75% Grass cover, Good, HSG D
	71,445	89	Weighted Average
	34,689		48.55% Pervious Area
	36,756		51.45% Impervious Area



**EXISTING**

Type III 24-hr 1 INCH Rainfall=1.00"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	100	0.0082	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.30"
0.1	2	0.0082	0.63		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	23	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	19	0.0465	1.08		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0571	1.19		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0476	1.09		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	5	0.0476	1.53		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	2	0.0476	4.43		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.6	100	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	17	0.0588	4.92		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	23	0.0435	4.23		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	13	0.0465	4.38		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	8	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	1.43		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	3.29		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.6	64	0.0143	1.93		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.3	13	0.0143	0.84		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
17.6	483	Total			

**Summary for Subcatchment 101: EX-WS-101**

Runoff = 0.03 cfs @ 12.10 hrs, Volume= 0.002 af, Depth> 0.25"  
Routed to Link AP2 : ANALYSIS POINT #2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 1 INCH Rainfall=1.00"

**EXISTING**

Type III 24-hr 1 INCH Rainfall=1.00"

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	Area (sf)	CN	Description
*	310	98	Roof, HSG D
*	1,765	98	Pavement, HSG D
*	133	98	Sidewalk, HSG D
*	4	98	Stairs, HSG D
	482	77	Woods, Good, HSG D
	2,270	80	>75% Grass cover, Good, HSG D
	4,964	88	Weighted Average
	2,752		55.44% Pervious Area
	2,212		44.56% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.1	25	0.3333	3.26		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.30"
0.9	6	0.0251	0.11		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.30"
0.5	37	0.0251	1.25		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.30"
0.6	32	0.0122	0.91		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.30"
0.1	16	0.0122	2.24		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.7	34	0.0122	0.77		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	4	0.0309	1.23		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	3	0.0309	3.57		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.2	13	0.0309	1.23		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	13	0.0309	0.88		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	5	0.0562	1.66		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
3.5	188	Total, Increased to minimum Tc = 6.0 min			

**Summary for Link AP1: ANALYSIS POINT #1**

Inflow Area = 1.640 ac, 51.45% Impervious, Inflow Depth > 0.28" for 1 INCH event  
 Inflow = 0.35 cfs @ 12.27 hrs, Volume= 0.039 af  
 Primary = 0.35 cfs @ 12.27 hrs, Volume= 0.039 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**EXISTING***Type III 24-hr 1 INCH Rainfall=1.00"*

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**Summary for Link AP2: ANALYSIS POINT #2**

Inflow Area = 0.114 ac, 44.56% Impervious, Inflow Depth > 0.25" for 1 INCH event  
Inflow = 0.03 cfs @ 12.10 hrs, Volume= 0.002 af  
Primary = 0.03 cfs @ 12.10 hrs, Volume= 0.002 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**EXISTING***Type III 24-hr 2 YEAR Rainfall=3.30"*

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment100: EX-WS-100**Runoff Area=71,445 sf 51.45% Impervious Runoff Depth>2.17"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=2.94 cfs 0.296 af**Subcatchment101: EX-WS-101**Runoff Area=4,964 sf 44.56% Impervious Runoff Depth>2.09"  
Flow Length=188' Tc=6.0 min CN=88 Runoff=0.27 cfs 0.020 af**Link AP1: ANALYSISPOINT #1**Inflow=2.94 cfs 0.296 af  
Primary=2.94 cfs 0.296 af**Link AP2: ANALYSISPOINT #2**Inflow=0.27 cfs 0.020 af  
Primary=0.27 cfs 0.020 af**Total Runoff Area = 1.754 ac Runoff Volume = 0.316 af Average Runoff Depth = 2.16"**  
**49.00% Pervious = 0.860 ac 51.00% Impervious = 0.895 ac**

**EXISTING***Type III 24-hr 10 YEAR Rainfall=5.29"*

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment100: EX-WS-100**Runoff Area=71,445 sf 51.45% Impervious Runoff Depth>4.04"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=5.36 cfs 0.552 af**Subcatchment101: EX-WS-101**Runoff Area=4,964 sf 44.56% Impervious Runoff Depth>3.94"  
Flow Length=188' Tc=6.0 min CN=88 Runoff=0.50 cfs 0.037 af**Link AP1: ANALYSISPOINT #1**Inflow=5.36 cfs 0.552 af  
Primary=5.36 cfs 0.552 af**Link AP2: ANALYSISPOINT #2**Inflow=0.50 cfs 0.037 af  
Primary=0.50 cfs 0.037 af**Total Runoff Area = 1.754 ac Runoff Volume = 0.590 af Average Runoff Depth = 4.03"**  
**49.00% Pervious = 0.860 ac 51.00% Impervious = 0.895 ac**



**EXISTING**

Type III 24-hr 10 YEAR Rainfall=5.29"

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**Summary for Subcatchment 100: EX-WS-100**

Runoff = 5.36 cfs @ 12.24 hrs, Volume= 0.552 af, Depth> 4.04"  
Routed to Link AP1 : ANALYSIS POINT #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 10 YEAR Rainfall=5.29"

	Area (sf)	CN	Description
	11,440	77	Woods, Good, HSG D
*	10,379	98	Roof, HSG D
*	267	98	Sidewalk, HSG D
*	640	98	Patio/Stairs, HSG D
*	18,321	98	Pavement, HSG D
*	7,149	98	Gravel, HSG D
	23,249	80	>75% Grass cover, Good, HSG D
	71,445	89	Weighted Average
	34,689		48.55% Pervious Area
	36,756		51.45% Impervious Area

**EXISTING**

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Type III 24-hr 10 YEAR Rainfall=5.29"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	100	0.0082	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.30"
0.1	2	0.0082	0.63		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	23	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	19	0.0465	1.08		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0571	1.19		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0476	1.09		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	5	0.0476	1.53		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	2	0.0476	4.43		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.6	100	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	17	0.0588	4.92		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	23	0.0435	4.23		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	13	0.0465	4.38		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	8	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	1.43		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	3.29		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.6	64	0.0143	1.93		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.3	13	0.0143	0.84		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
17.6	483	Total			

### Summary for Subcatchment 101: EX-WS-101

Runoff = 0.50 cfs @ 12.09 hrs, Volume= 0.037 af, Depth> 3.94"  
 Routed to Link AP2 : ANALYSIS POINT #2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10 YEAR Rainfall=5.29"

**EXISTING**

Type III 24-hr 10 YEAR Rainfall=5.29"

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	Area (sf)	CN	Description
*	310	98	Roof, HSG D
*	1,765	98	Pavement, HSG D
*	133	98	Sidewalk, HSG D
*	4	98	Stairs, HSG D
	482	77	Woods, Good, HSG D
	2,270	80	>75% Grass cover, Good, HSG D
	4,964	88	Weighted Average
	2,752		55.44% Pervious Area
	2,212		44.56% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.1	25	0.3333	3.26		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.30"
0.9	6	0.0251	0.11		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.30"
0.5	37	0.0251	1.25		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.30"
0.6	32	0.0122	0.91		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.30"
0.1	16	0.0122	2.24		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.7	34	0.0122	0.77		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	4	0.0309	1.23		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	3	0.0309	3.57		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.2	13	0.0309	1.23		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	13	0.0309	0.88		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	5	0.0562	1.66		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
3.5	188	Total, Increased to minimum Tc = 6.0 min			

**Summary for Link AP1: ANALYSIS POINT #1**

Inflow Area = 1.640 ac, 51.45% Impervious, Inflow Depth > 4.04" for 10 YEAR event  
 Inflow = 5.36 cfs @ 12.24 hrs, Volume= 0.552 af  
 Primary = 5.36 cfs @ 12.24 hrs, Volume= 0.552 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**EXISTING***Type III 24-hr 10 YEAR Rainfall=5.29"*

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**Summary for Link AP2: ANALYSIS POINT #2**

Inflow Area = 0.114 ac, 44.56% Impervious, Inflow Depth > 3.94" for 10 YEAR event  
Inflow = 0.50 cfs @ 12.09 hrs, Volume= 0.037 af  
Primary = 0.50 cfs @ 12.09 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**EXISTING***Type III 24-hr 17 YEAR Rainfall=5.87"*

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

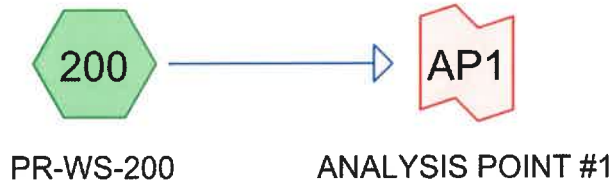
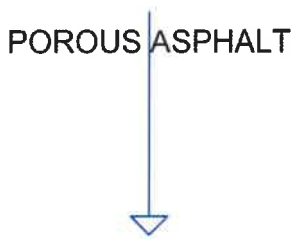
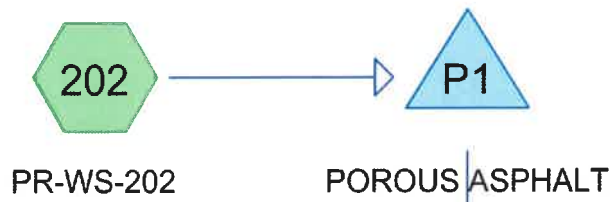
**Subcatchment100: EX-WS-100**Runoff Area=71,445 sf 51.45% Impervious Runoff Depth>4.60"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=6.06 cfs 0.628 af**Subcatchment101: EX-WS-101**Runoff Area=4,964 sf 44.56% Impervious Runoff Depth>4.50"  
Flow Length=188' Tc=6.0 min CN=88 Runoff=0.57 cfs 0.043 af**Link AP1: ANALYSISPOINT #1**Inflow=6.06 cfs 0.628 af  
Primary=6.06 cfs 0.628 af**Link AP2: ANALYSISPOINT #2**Inflow=0.57 cfs 0.043 af  
Primary=0.57 cfs 0.043 af**Total Runoff Area = 1.754 ac Runoff Volume = 0.671 af Average Runoff Depth = 4.59"**  
**49.00% Pervious = 0.860 ac 51.00% Impervious = 0.895 ac**



## APPENDIX 3.8 DRAINAGE CALCULATIONS

### POST-DEVELOPMENT CONDITIONS ANALYSIS

- 1-Inch 24-Hour Complete Analysis
- 2-Year 24-Hour Summary Analysis
- 10-Year 24-Hour Complete Analysis
- 17-Year 24-Hour Summary Analysis
- 100-Year 24-Hour Pond Summary



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### Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.521	80	>75% Grass cover, Good, HSG D (200, 201, 202)
0.002	98	Concrete, HSG D (202)
0.164	98	Gravel, HSG D (200)
0.015	98	Patio/Stairs, HSG D (200, 202)
0.453	98	Pavement, HSG D (200, 201)
0.098	98	Porous Asphalt, HSG D (202)
0.262	98	Roof, HSG D (200, 202)
0.239	77	Woods, Good, HSG D (200)
<b>1.754</b>	<b>90</b>	<b>TOTAL AREA</b>

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### Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
1.754	HSG D	200, 201, 202
0.000	Other	
<b>1.754</b>		<b>TOTAL AREA</b>

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Type III 24-hr 1 INCH Rainfall=1.00"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment200: PR-WS-200**Runoff Area=67,282 sf 53.36% Impervious Runoff Depth>0.28"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=0.33 cfs 0.037 af**Subcatchment201: PR-WS-201**Runoff Area=1,090 sf 50.37% Impervious Runoff Depth>0.28"  
Tc=6.0 min CN=89 Runoff=0.01 cfs 0.001 af**Subcatchment202: PR-WS-202**Runoff Area=8,013 sf 85.05% Impervious Runoff Depth>0.56"  
Tc=6.0 min CN=95 Runoff=0.12 cfs 0.009 af**Reach 20R: OVERLAND FLOW**Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af  
n=0.030 L=20.3' S=0.0163 '/' Capacity=10.08 cfs Outflow=0.00 cfs 0.000 af**Pond P1: POROUS ASPHALT**Peak Elev=70.66' Storage=111 cf Inflow=0.12 cfs 0.009 af  
Discarded=0.03 cfs 0.009 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.009 af**Link AP1: ANALYSISPOINT #1**Inflow=0.33 cfs 0.037 af  
Primary=0.33 cfs 0.037 af**Link AP2: ANALYSISPOINT #2**Inflow=0.01 cfs 0.001 af  
Primary=0.01 cfs 0.001 af**Total Runoff Area = 1.754 ac Runoff Volume = 0.046 af Average Runoff Depth = 0.31"**  
**43.36% Pervious = 0.760 ac 56.64% Impervious = 0.993 ac**



**PROPOSED**

Type III 24-hr 1 INCH Rainfall=1.00"

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**Summary for Subcatchment 200: PR-WS-200**

Runoff = 0.33 cfs @ 12.27 hrs, Volume= 0.037 af, Depth> 0.28"  
Routed to Link AP1 : ANALYSIS POINT #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 1 INCH Rainfall=1.00"

	Area (sf)	CN	Description
	10,404	77	Woods, Good, HSG D
*	9,221	98	Roof, HSG D
*	354	98	Patio/Stairs, HSG D
*	19,180	98	Pavement, HSG D
*	7,149	98	Gravel, HSG D
	20,974	80	>75% Grass cover, Good, HSG D
	67,282	89	Weighted Average
	31,378		46.64% Pervious Area
	35,904		53.36% Impervious Area

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Type III 24-hr 1 INCH Rainfall=1.00"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	100	0.0082	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.30"
0.1	2	0.0082	0.63		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	23	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	19	0.0465	1.08		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0571	1.19		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0476	1.09		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	5	0.0476	1.53		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	2	0.0476	4.43		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.6	100	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	17	0.0588	4.92		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	23	0.0435	4.23		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	13	0.0465	4.38		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	8	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	1.43		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	3.29		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.6	64	0.0143	1.93		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.3	13	0.0143	0.84		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
17.6	483	Total			

**Summary for Subcatchment 201: PR-WS-201**

Runoff = 0.01 cfs @ 12.10 hrs, Volume= 0.001 af, Depth> 0.28"  
Routed to Link AP2 : ANALYSIS POINT #2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 1 INCH Rainfall=1.00"

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Type III 24-hr 1 INCH Rainfall=1.00"

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Area (sf)	CN	Description
* 549	98	Pavement, HSG D
541	80	>75% Grass cover, Good, HSG D
1,090	89	Weighted Average
541		49.63% Pervious Area
549		50.37% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment 202: PR-WS-202**

Runoff = 0.12 cfs @ 12.09 hrs, Volume= 0.009 af, Depth> 0.56"  
 Routed to Pond P1 : POROUS ASPHALT

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 1 INCH Rainfall=1.00"

Area (sf)	CN	Description
* 2,178	98	Roof, HSG D
* 286	98	Patio/Stairs, HSG D
1,198	80	>75% Grass cover, Good, HSG D
* 4,251	98	Porous Asphalt, HSG D
* 100	98	Concrete, HSG D
8,013	95	Weighted Average
1,198		14.95% Pervious Area
6,815		85.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Reach 20R: OVERLAND FLOW**

Inflow Area = 0.184 ac, 85.05% Impervious, Inflow Depth = 0.00" for 1 INCH event  
 Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min  
 Routed to Link AP1 : ANALYSIS POINT #1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs  
 Average Depth at Peak Storage= 0.00'  
 Bank-Full Depth= 0.50' Flow Area= 3.3 sf, Capacity= 10.08 cfs

**PROPOSED**

Type III 24-hr 1 INCH Rainfall=1.00"

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10.00' x 0.50' deep Parabolic Channel, n= 0.030 Earth, grassed &amp; winding

Length= 20.3' Slope= 0.0163 '/'

Inlet Invert= 70.70', Outlet Invert= 70.37'

**Summary for Pond P1: POROUS ASPHALT**

Inflow Area = 0.184 ac, 85.05% Impervious, Inflow Depth > 0.56" for 1 INCH event  
 Inflow = 0.12 cfs @ 12.09 hrs, Volume= 0.009 af  
 Outflow = 0.03 cfs @ 12.48 hrs, Volume= 0.009 af, Atten= 73%, Lag= 23.0 min  
 Discarded = 0.03 cfs @ 12.48 hrs, Volume= 0.009 af  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af  
 Routed to Reach 20R : OVERLAND FLOW

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 70.66' @ 12.48 hrs Surf.Area= 4,251 sf Storage= 111 cf

Flood Elev= 73.50' Surf.Area= 4,251 sf Storage= 2,568 cf

Plug-Flow detention time= 40.4 min calculated for 0.009 af (99% of inflow)

Center-of-Mass det. time= 35.3 min ( 858.8 - 823.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	70.49'	4,687 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) <b>4.0" Round Pipe Storage</b> L= 78.0'
#2	70.75'	7 cf	
		4,694 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
70.49	4,251	0.0	0	0
70.50	4,251	15.0	6	6
70.74	4,251	15.0	153	159
70.75	4,251	40.0	17	176
71.41	4,251	40.0	1,122	1,299
71.42	4,251	15.0	6	1,305
71.66	4,251	15.0	153	1,458
71.67	4,251	5.0	2	1,460
72.66	4,251	5.0	210	1,671
72.67	4,251	30.0	13	1,683
73.16	4,251	30.0	625	2,308
73.17	4,251	15.0	6	2,315
73.49	4,251	15.0	204	2,519
73.50	4,251	100.0	43	2,561
74.00	4,251	100.0	2,126	4,687

**PROPOSED**

Type III 24-hr 1 INCH Rainfall=1.00"

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Device	Routing	Invert	Outlet Devices
#1	Primary	70.75'	<b>4.0" Round Culvert</b> L= 10.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 70.75' / 70.70' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Device 1	70.75'	<b>4.0" Vert. PERFORATED UNDERDRAIN #1</b> C= 0.600 Limited to weir flow at low heads
#3	Discarded	70.49'	<b>0.300 in/hr Exfiltration over Surface area</b> Conductivity to Groundwater Elevation = 68.10' Phase-In= 0.10'

**Discarded OutFlow** Max=0.03 cfs @ 12.48 hrs HW=70.66' (Free Discharge)↑**3=Exfiltration** ( Controls 0.03 cfs)**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=70.49' TW=70.70' (Dynamic Tailwater)↑**1=Culvert** ( Controls 0.00 cfs)↑**2=PERFORATED UNDERDRAIN #1**( Controls 0.00 cfs)**Summary for Link AP1: ANALYSIS POINT #1**

Inflow Area = 1.729 ac, 56.74% Impervious, Inflow Depth > 0.25" for 1 INCH event  
 Inflow = 0.33 cfs @ 12.27 hrs, Volume= 0.037 af  
 Primary = 0.33 cfs @ 12.27 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**Summary for Link AP2: ANALYSIS POINT #2**

Inflow Area = 0.025 ac, 50.37% Impervious, Inflow Depth > 0.28" for 1 INCH event  
 Inflow = 0.01 cfs @ 12.10 hrs, Volume= 0.001 af  
 Primary = 0.01 cfs @ 12.10 hrs, Volume= 0.001 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## PROPOSED

Type III 24-hr 2 YEAR Rainfall=3.30"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

### Subcatchment200: PR-WS-200

Runoff Area=67,282 sf 53.36% Impervious Runoff Depth>2.17"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=2.77 cfs 0.279 af

### Subcatchment201: PR-WS-201

Runoff Area=1,090 sf 50.37% Impervious Runoff Depth>2.17"  
Tc=6.0 min CN=89 Runoff=0.06 cfs 0.005 af

### Subcatchment202: PR-WS-202

Runoff Area=8,013 sf 85.05% Impervious Runoff Depth>2.74"  
Tc=6.0 min CN=95 Runoff=0.55 cfs 0.042 af

### Reach 20R: OVERLAND FLOW

Avg. Flow Depth=0.06' Max Vel=0.72 fps Inflow=0.09 cfs 0.012 af  
n=0.030 L=20.3' S=0.0163 '/' Capacity=10.08 cfs Outflow=0.09 cfs 0.012 af

### Pond P1: POROUS ASPHALT

Peak Elev=71.03' Storage=658 cf Inflow=0.55 cfs 0.042 af  
Discarded=0.04 cfs 0.030 af Primary=0.09 cfs 0.012 af Outflow=0.13 cfs 0.042 af

### Link AP1: ANALYSISPOINT #1

Inflow=2.84 cfs 0.291 af  
Primary=2.84 cfs 0.291 af

### Link AP2: ANALYSISPOINT #2

Inflow=0.06 cfs 0.005 af  
Primary=0.06 cfs 0.005 af

**Total Runoff Area = 1.754 ac Runoff Volume = 0.325 af Average Runoff Depth = 2.23"**  
**43.36% Pervious = 0.760 ac 56.64% Impervious = 0.993 ac**

**PROPOSED**

Type III 24-hr 10 YEAR Rainfall=5.29"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment200: PR-WS-200**Runoff Area=67,282 sf 53.36% Impervious Runoff Depth>4.04"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=5.05 cfs 0.520 af**Subcatchment201: PR-WS-201**Runoff Area=1,090 sf 50.37% Impervious Runoff Depth>4.05"  
Tc=6.0 min CN=89 Runoff=0.11 cfs 0.008 af**Subcatchment202: PR-WS-202**Runoff Area=8,013 sf 85.05% Impervious Runoff Depth>4.70"  
Tc=6.0 min CN=95 Runoff=0.91 cfs 0.072 af**Reach 20R: OVERLAND FLOW**Avg. Flow Depth=0.08' Max Vel=0.91 fps Inflow=0.20 cfs 0.032 af  
n=0.030 L=20.3' S=0.0163 ' Capacity=10.08 cfs Outflow=0.20 cfs 0.032 af**Pond P1: POROUS ASPHALT**Peak Elev=71.30' Storage=1,119 cf Inflow=0.91 cfs 0.072 af  
Discarded=0.04 cfs 0.040 af Primary=0.20 cfs 0.032 af Outflow=0.24 cfs 0.072 af**Link AP1: ANALYSISPOINT #1**Inflow=5.23 cfs 0.552 af  
Primary=5.23 cfs 0.552 af**Link AP2: ANALYSISPOINT #2**Inflow=0.11 cfs 0.008 af  
Primary=0.11 cfs 0.008 af**Total Runoff Area = 1.754 ac Runoff Volume = 0.600 af Average Runoff Depth = 4.11"**  
**43.36% Pervious = 0.760 ac 56.64% Impervious = 0.993 ac**

**PROPOSED**

Type III 24-hr 10 YEAR Rainfall=5.29"

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**Summary for Subcatchment 200: PR-WS-200**

Runoff = 5.05 cfs @ 12.24 hrs, Volume= 0.520 af, Depth> 4.04"  
Routed to Link AP1 : ANALYSIS POINT #1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 10 YEAR Rainfall=5.29"

	Area (sf)	CN	Description
	10,404	77	Woods, Good, HSG D
*	9,221	98	Roof, HSG D
*	354	98	Patio/Stairs, HSG D
*	19,180	98	Pavement, HSG D
*	7,149	98	Gravel, HSG D
	20,974	80	>75% Grass cover, Good, HSG D
	67,282	89	Weighted Average
	31,378		46.64% Pervious Area
	35,904		53.36% Impervious Area



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Type III 24-hr 10 YEAR Rainfall=5.29"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	100	0.0082	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.30"
0.1	2	0.0082	0.63		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	23	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	19	0.0465	1.08		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0571	1.19		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.5	35	0.0476	1.09		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	5	0.0476	1.53		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	2	0.0476	4.43		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.6	100	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	17	0.0588	4.92		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	23	0.0435	4.23		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	13	0.0465	4.38		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	8	0.0465	1.51		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	1.43		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	12	0.0417	3.29		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.6	64	0.0143	1.93		<b>Shallow Concentrated Flow,</b> Unpaved Kv= 16.1 fps
0.3	13	0.0143	0.84		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
17.6	483	Total			

**Summary for Subcatchment 201: PR-WS-201**

Runoff = 0.11 cfs @ 12.09 hrs, Volume= 0.008 af, Depth> 4.05"  
Routed to Link AP2 : ANALYSIS POINT #2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
Type III 24-hr 10 YEAR Rainfall=5.29"

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Type III 24-hr 10 YEAR Rainfall=5.29"

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Area (sf)	CN	Description
* 549	98	Pavement, HSG D
541	80	>75% Grass cover, Good, HSG D
1,090	89	Weighted Average
541		49.63% Pervious Area
549		50.37% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment 202: PR-WS-202**

Runoff = 0.91 cfs @ 12.09 hrs, Volume= 0.072 af, Depth> 4.70"  
 Routed to Pond P1 : POROUS ASPHALT

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
 Type III 24-hr 10 YEAR Rainfall=5.29"

Area (sf)	CN	Description
* 2,178	98	Roof, HSG D
* 286	98	Patio/Stairs, HSG D
1,198	80	>75% Grass cover, Good, HSG D
* 4,251	98	Porous Asphalt, HSG D
* 100	98	Concrete, HSG D
8,013	95	Weighted Average
1,198		14.95% Pervious Area
6,815		85.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Reach 20R: OVERLAND FLOW**

Inflow Area = 0.184 ac, 85.05% Impervious, Inflow Depth = 2.07" for 10 YEAR event  
 Inflow = 0.20 cfs @ 12.45 hrs, Volume= 0.032 af  
 Outflow = 0.20 cfs @ 12.45 hrs, Volume= 0.032 af, Atten= 0%, Lag= 0.3 min  
 Routed to Link AP1 : ANALYSIS POINT #1

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs  
 Max. Velocity= 0.91 fps, Min. Travel Time= 0.4 min  
 Avg. Velocity = 0.49 fps, Avg. Travel Time= 0.7 min

Peak Storage= 4 cf @ 12.45 hrs  
 Average Depth at Peak Storage= 0.08' , Surface Width= 4.05'  
 Bank-Full Depth= 0.50' Flow Area= 3.3 sf, Capacity= 10.08 cfs

**PROPOSED**

Type III 24-hr 10 YEAR Rainfall=5.29"

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10.00' x 0.50' deep Parabolic Channel, n= 0.030 Earth, grassed &amp; winding

Length= 20.3' Slope= 0.0163 '/'

Inlet Invert= 70.70', Outlet Invert= 70.37'

**Summary for Pond P1: POROUS ASPHALT**

Inflow Area = 0.184 ac, 85.05% Impervious, Inflow Depth > 4.70" for 10 YEAR event  
 Inflow = 0.91 cfs @ 12.09 hrs, Volume= 0.072 af  
 Outflow = 0.24 cfs @ 12.45 hrs, Volume= 0.072 af, Atten= 74%, Lag= 21.5 min  
 Discarded = 0.04 cfs @ 12.45 hrs, Volume= 0.040 af  
 Primary = 0.20 cfs @ 12.45 hrs, Volume= 0.032 af  
 Routed to Reach 20R : OVERLAND FLOW

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Peak Elev= 71.30' @ 12.45 hrs Surf.Area= 4,251 sf Storage= 1,119 cf

Flood Elev= 73.50' Surf.Area= 4,251 sf Storage= 2,568 cf

Plug-Flow detention time= 80.2 min calculated for 0.072 af (99% of inflow)

Center-of-Mass det. time= 76.1 min ( 842.4 - 766.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	70.49'	4,687 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc) <b>4.0" Round Pipe Storage</b> L= 78.0'
#2	70.75'	7 cf	
		4,694 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
70.49	4,251	0.0	0	0
70.50	4,251	15.0	6	6
70.74	4,251	15.0	153	159
70.75	4,251	40.0	17	176
71.41	4,251	40.0	1,122	1,299
71.42	4,251	15.0	6	1,305
71.66	4,251	15.0	153	1,458
71.67	4,251	5.0	2	1,460
72.66	4,251	5.0	210	1,671
72.67	4,251	30.0	13	1,683
73.16	4,251	30.0	625	2,308
73.17	4,251	15.0	6	2,315
73.49	4,251	15.0	204	2,519
73.50	4,251	100.0	43	2,561
74.00	4,251	100.0	2,126	4,687

**PROPOSED**

Type III 24-hr 10 YEAR Rainfall=5.29"

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Device	Routing	Invert	Outlet Devices
#1	Primary	70.75'	<b>4.0" Round Culvert</b> L= 10.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 70.75' / 70.70' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Device 1	70.75'	<b>4.0" Vert. PERFORATED UNDERDRAIN #1</b> C= 0.600 Limited to weir flow at low heads
#3	Discarded	70.49'	<b>0.300 in/hr Exfiltration over Surface area</b> Conductivity to Groundwater Elevation = 68.10' Phase-In= 0.10'

**Discarded OutFlow** Max=0.04 cfs @ 12.45 hrs HW=71.30' (Free Discharge)↑**3=Exfiltration** ( Controls 0.04 cfs)**Primary OutFlow** Max=0.20 cfs @ 12.45 hrs HW=71.30' TW=70.78' (Dynamic Tailwater)↑**1=Culvert** (Barrel Controls 0.20 cfs @ 2.30 fps)↑**2=PERFORATED UNDERDRAIN #1** (Passes 0.20 cfs of 0.26 cfs potential flow)**Summary for Link AP1: ANALYSIS POINT #1**

Inflow Area = 1.729 ac, 56.74% Impervious, Inflow Depth > 3.83" for 10 YEAR event  
 Inflow = 5.23 cfs @ 12.24 hrs, Volume= 0.552 af  
 Primary = 5.23 cfs @ 12.24 hrs, Volume= 0.552 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**Summary for Link AP2: ANALYSIS POINT #2**

Inflow Area = 0.025 ac, 50.37% Impervious, Inflow Depth > 4.05" for 10 YEAR event  
 Inflow = 0.11 cfs @ 12.09 hrs, Volume= 0.008 af  
 Primary = 0.11 cfs @ 12.09 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

**PROPOSED***Type III 24-hr 17 YEAR Rainfall=5.87"*

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment200: PR-WS-200** Runoff Area=67,282 sf 53.36% Impervious Runoff Depth>4.60"  
Flow Length=483' Tc=17.6 min CN=89 Runoff=5.71 cfs 0.592 af

**Subcatchment201: PR-WS-201** Runoff Area=1,090 sf 50.37% Impervious Runoff Depth>4.61"  
Tc=6.0 min CN=89 Runoff=0.13 cfs 0.010 af

**Subcatchment202: PR-WS-202** Runoff Area=8,013 sf 85.05% Impervious Runoff Depth>5.28"  
Tc=6.0 min CN=95 Runoff=1.01 cfs 0.081 af

**Reach 20R: OVERLAND FLOW** Avg. Flow Depth=0.09' Max Vel=0.94 fps Inflow=0.23 cfs 0.038 af  
n=0.030 L=20.3' S=0.0163 '/' Capacity=10.08 cfs Outflow=0.23 cfs 0.038 af

**Pond P1: POROUS ASPHALT** Peak Elev=71.38' Storage=1,258 cf Inflow=1.01 cfs 0.081 af  
Discarded=0.04 cfs 0.042 af Primary=0.23 cfs 0.038 af Outflow=0.27 cfs 0.080 af

**Link AP1: ANALYSISPOINT #1** Inflow=5.92 cfs 0.630 af  
Primary=5.92 cfs 0.630 af

**Link AP2: ANALYSISPOINT #2** Inflow=0.13 cfs 0.010 af  
Primary=0.13 cfs 0.010 af

**Total Runoff Area = 1.754 ac Runoff Volume = 0.682 af Average Runoff Depth = 4.67"**  
**43.36% Pervious = 0.760 ac 56.64% Impervious = 0.993 ac**

**PROPOSED***Type III 24-hr 17 YEAR Rainfall=5.87"*

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Pond P1: POROUS ASPHALT**

Peak Elev=71.38' Storage=1,258 cf Inflow=1.01 cfs 0.081 af

Discarded=0.04 cfs 0.042 af Primary=0.23 cfs 0.038 af Outflow=0.27 cfs 0.080 af

## APPENDIX 4

### EXTREME PRECIPITATION TABLE



NOAA Atlas 14, Volume 10, Version 3  
 Location name: Durham, New Hampshire, USA\*  
 Latitude: 43.1383°, Longitude: -70.9265°  
 Elevation: 77 ft\*\*  
 \* source: ESRI Maps  
 \*\* source: USGS



## POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriols](#)

### PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.300 (0.242-0.374)	0.363 (0.293-0.452)	0.466 (0.374-0.583)	0.550 (0.439-0.692)	0.667 (0.512-0.876)	0.755 (0.566-1.01)	0.847 (0.613-1.18)	0.951 (0.647-1.35)	1.10 (0.717-1.62)	1.23 (0.776-1.84)
10-min	0.425 (0.343-0.530)	0.514 (0.415-0.641)	0.659 (0.529-0.824)	0.779 (0.622-0.980)	0.944 (0.726-1.24)	1.07 (0.801-1.43)	1.20 (0.869-1.67)	1.35 (0.917-1.91)	1.56 (1.02-2.29)	1.74 (1.10-2.60)
15-min	0.500 (0.404-0.623)	0.604 (0.488-0.754)	0.774 (0.623-0.969)	0.916 (0.732-1.15)	1.11 (0.854-1.46)	1.26 (0.943-1.69)	1.41 (1.02-1.96)	1.58 (1.08-2.25)	1.84 (1.20-2.70)	2.04 (1.29-3.06)
30-min	0.668 (0.540-0.832)	0.807 (0.651-1.01)	1.04 (0.832-1.30)	1.22 (0.977-1.54)	1.48 (1.14-1.95)	1.68 (1.26-2.26)	1.88 (1.37-2.63)	2.12 (1.44-3.02)	2.48 (1.61-3.64)	2.77 (1.75-4.15)
60-min	0.835 (0.675-1.04)	1.01 (0.815-1.26)	1.30 (1.04-1.62)	1.53 (1.22-1.93)	1.86 (1.43-2.44)	2.10 (1.58-2.83)	2.36 (1.72-3.30)	2.66 (1.81-3.78)	3.12 (2.03-4.58)	3.50 (2.21-5.24)
2-hr	1.12 (0.911-1.39)	1.36 (1.11-1.69)	1.76 (1.42-2.19)	2.09 (1.68-2.62)	2.55 (1.97-3.34)	2.88 (2.18-3.87)	3.25 (2.38-4.54)	3.69 (2.52-5.22)	4.37 (2.85-6.38)	4.94 (3.14-7.36)
3-hr	1.32 (1.08-1.63)	1.62 (1.32-2.00)	2.10 (1.70-2.60)	2.50 (2.01-3.11)	3.05 (2.37-3.98)	3.45 (2.62-4.62)	3.89 (2.87-5.44)	4.43 (3.03-6.24)	5.26 (3.44-7.67)	5.98 (3.80-8.88)
6-hr	1.74 (1.43-2.14)	2.14 (1.75-2.62)	2.78 (2.28-3.43)	3.32 (2.70-4.11)	4.06 (3.18-5.28)	4.61 (3.52-6.13)	5.20 (3.85-7.22)	5.93 (4.07-8.30)	7.06 (4.63-10.2)	8.04 (5.13-11.8)
12-hr	2.22 (1.84-2.70)	2.74 (2.26-3.34)	3.59 (2.95-4.38)	4.29 (3.50-5.27)	5.25 (4.13-6.79)	5.97 (4.59-7.89)	6.74 (5.02-9.31)	7.70 (5.30-10.7)	9.18 (6.04-13.2)	10.5 (6.69-15.3)
24-hr	2.63 (2.19-3.18)	3.30 (2.74-3.99)	4.39 (3.63-5.33)	5.29 (4.34-6.46)	6.53 (5.17-8.40)	7.44 (5.76-9.82)	8.45 (6.35-11.6)	9.72 (6.72-13.4)	11.7 (7.73-16.8)	13.5 (8.65-19.6)
2-day	2.92 (2.44-3.50)	3.74 (3.13-4.49)	5.08 (4.23-6.13)	6.20 (5.12-7.52)	7.74 (6.18-9.93)	8.85 (6.92-11.7)	10.1 (7.68-14.0)	11.8 (8.14-16.2)	14.4 (9.55-20.5)	16.9 (10.8-24.4)
3-day	3.14 (2.64-3.76)	4.02 (3.38-4.82)	5.47 (4.57-6.57)	6.67 (5.53-8.05)	8.32 (6.66-10.6)	9.51 (7.46-12.5)	10.9 (8.29-15.0)	12.6 (8.78-17.3)	15.6 (10.3-22.1)	18.2 (11.7-26.2)
4-day	3.37 (2.84-4.02)	4.29 (3.61-5.12)	5.78 (4.84-6.92)	7.02 (5.83-8.45)	8.72 (7.00-11.1)	9.96 (7.82-13.0)	11.3 (8.67-15.6)	13.2 (9.17-18.0)	16.2 (10.8-22.9)	18.9 (12.2-27.2)
7-day	4.09 (3.47-4.85)	5.05 (4.27-5.99)	6.61 (5.57-7.88)	7.91 (6.61-9.47)	9.69 (7.81-12.3)	11.0 (8.66-14.3)	12.4 (9.51-16.9)	14.3 (10.0-19.5)	17.4 (11.6-24.4)	20.1 (13.0-28.7)
10-day	4.78 (4.06-5.65)	5.77 (4.90-6.83)	7.39 (6.24-8.77)	8.73 (7.32-10.4)	10.6 (8.54-13.3)	11.9 (9.40-15.4)	13.4 (10.2-18.1)	15.3 (10.7-20.7)	18.3 (12.2-25.6)	20.9 (13.6-29.8)
20-day	6.76 (5.78-7.93)	7.86 (6.71-9.23)	9.66 (8.21-11.4)	11.2 (9.41-13.2)	13.2 (10.7-16.3)	14.7 (11.6-18.6)	16.4 (12.4-21.5)	18.2 (12.9-24.4)	21.0 (14.1-29.1)	23.2 (15.1-32.9)
30-day	8.32 (7.14-9.72)	9.51 (8.16-11.1)	11.5 (9.79-13.5)	13.1 (11.1-15.5)	15.3 (12.4-18.8)	17.0 (13.4-21.3)	18.8 (14.1-24.3)	20.6 (14.6-27.5)	23.2 (15.6-32.0)	25.1 (16.4-35.4)
45-day	10.2 (8.78-11.9)	11.5 (9.90-13.4)	13.7 (11.7-16.0)	15.4 (13.1-18.2)	17.9 (14.5-21.8)	19.8 (15.6-24.6)	21.7 (16.3-27.7)	23.5 (16.7-31.2)	25.9 (17.5-35.5)	27.6 (18.0-38.7)
60-day	11.7 (10.1-13.6)	13.1 (11.3-15.3)	15.4 (13.3-18.0)	17.4 (14.8-20.4)	20.0 (16.2-24.2)	22.1 (17.4-27.2)	24.1 (18.0-30.5)	25.9 (18.5-34.2)	28.2 (19.1-38.6)	29.7 (19.4-41.6)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

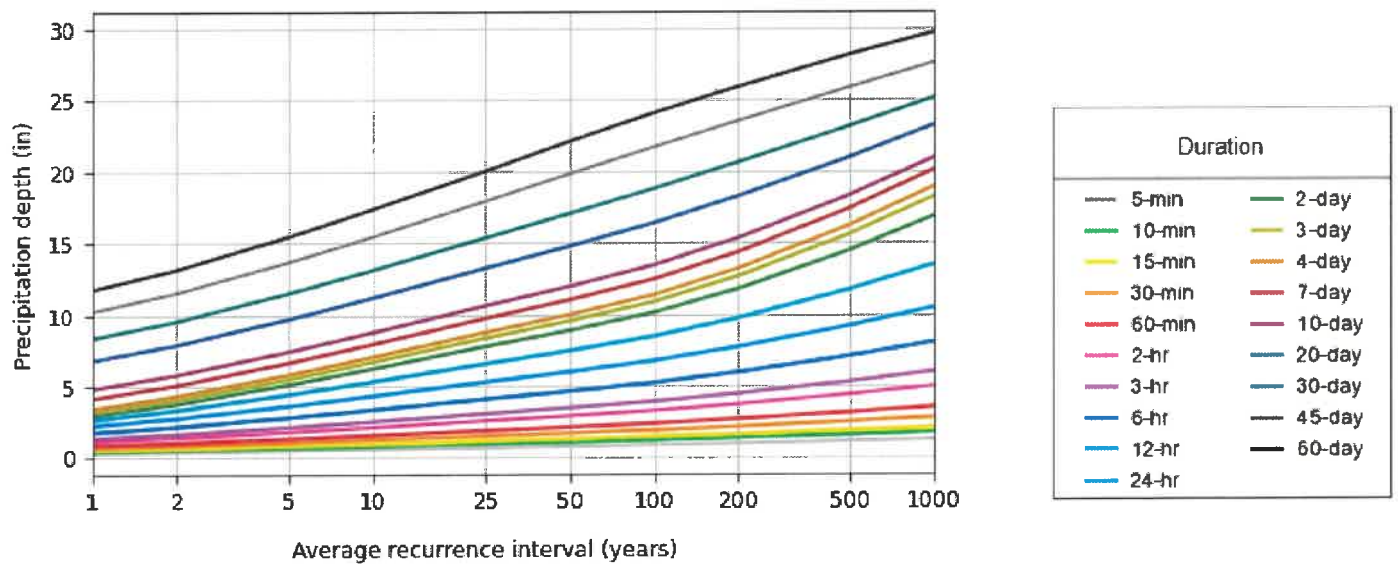
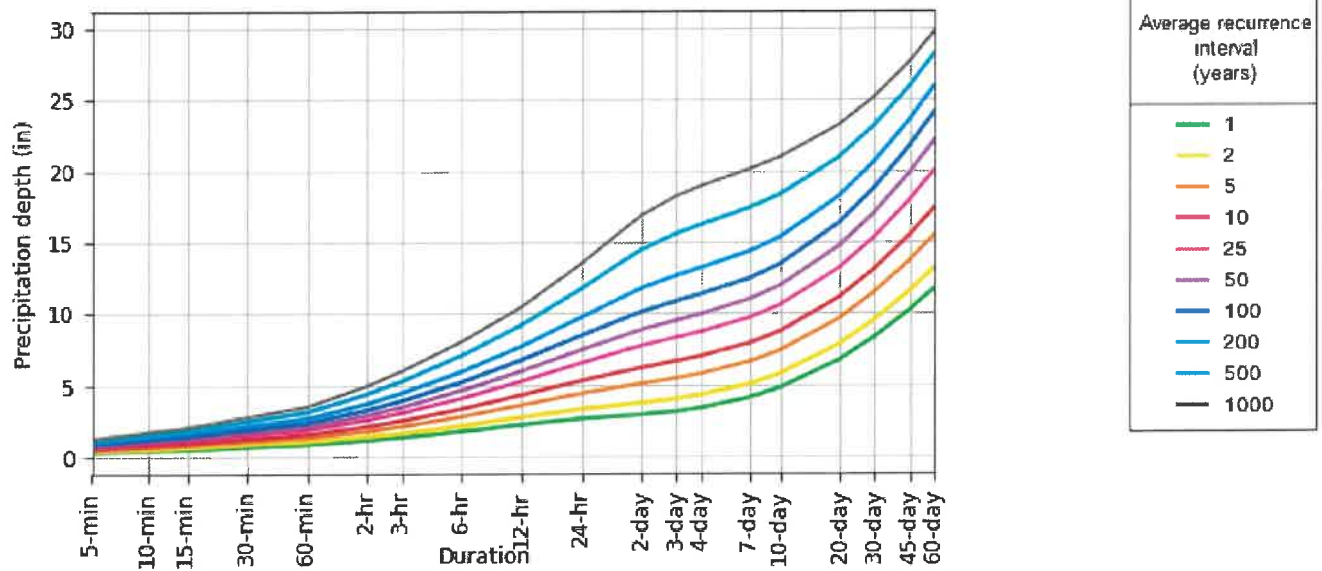
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### PF graphical



## PDS-based depth-duration-frequency (DDF) curves

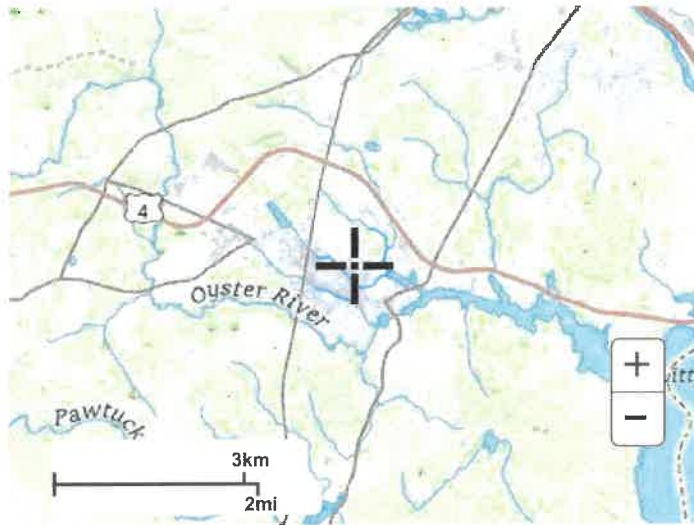
Latitude: 43.1383°, Longitude: -70.9265°



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## Maps & aerials

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



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1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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APPENDIX 5

WEB SOIL SURVEY



# Custom Soil Resource Report Soil Map



MAP LEGEND

**Area of Interest (AOI)**

Area of Interest (AOI)

**Soils**

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

**Special Point Features**

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

**Water Features**

Streams and Canals

**Transportation**

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

**Background**

Aerial Photography

**Special Line Features**

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL: [Web Soil Survey](#)  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Strafford County, New Hampshire  
Survey Area Data: Version 25, Sep 3, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 19, 2020—Sep 20, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BzB	Buxton silt loam, 3 to 8 percent slopes	0.6	2.3%
HcB	Hollis-Charlton fine sandy loams, 3 to 8 percent slopes	18.8	71.1%
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	7.0	26.6%
<b>Totals for Area of Interest</b>		<b>26.4</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

## Custom Soil Resource Report

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.



## APPENDIX 6

### TEST PIT LOG

**TEST PITS  
FOR  
35 MADBURY ROAD  
DURHAM, NEW HAMPSHIRE  
JUNE 19, 2025  
JBE Project No. 25073**

Performed by: Anthony Jones, Jones & Beach Engineers, Inc., SSD #1900

**Test Pit #1**

0"- 14"	10YR 5/6	yellowish brown sand granular, very friable many roots
14" - 36"	10YR 4/4	dark yellowish brown fine sandy loam single grain, very friable common roots
36" - 42"	2.5Y 5/2	grayish brown Loamy fine sand platey, very friable

SHWT = 36"  
Roots: 36"  
No H<sub>2</sub>O observed  
No Refusal observed

**Test Pit #2**

0"- 16"	10YR 5/6	yellowish brown fine sandy loam granular, friable many roots
16" - 40"	10YR 4/4	dark yellowish brown fine sandy loam granular, friable common roots
40" - 48"	2.5Y 5/3	light olive brown Loamy fine sand platey, very friable common roots

SHWT = 40"  
Roots: 40"  
No H<sub>2</sub>O observed  
No Refusal observed

APPENDIX 7

BMP WORKSHEETS

# FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.08)

Type/Node Name: \_\_\_\_\_

**POROUS ASPHALT (POND P1)**

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.08(a).	
0.18	ac	A = Area draining to the practice	
0.16	ac	A <sub>i</sub> = Impervious area draining to the practice	
0.89	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.85	unitless	R <sub>v</sub> = Runoff coefficient = 0.05 + (0.9 x I)	
0.15	ac-in	WQV = 1" x R <sub>v</sub> x A	
555	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
139	cf	25% x WQV (check calc for sediment forebay volume)	
417	cf	75% x WQV (check calc for surface sand filter volume)	
N/A		Method of Pretreatment? (not required for clean or roof runoff)	
	cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
<b>Calculate time to drain if system IS NOT underdrained:</b>			
	sf	A <sub>SA</sub> = Surface area of the practice	
	iph	K <sub>sat</sub> <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>	
		If K <sub>sat</sub> (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	
-	hours	T <sub>DRAIN</sub> = Drain time = V / (A <sub>SA</sub> * I <sub>DESIGN</sub> )	≤ 72-hrs
<b>Calculate time to drain if system IS underdrained:</b>			
72.93	ft	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)	
0.47	cfs	Q <sub>WQV</sub> = Discharge at the E <sub>WQV</sub> (attach stage-discharge table)	
0.66	hours	T <sub>DRAIN</sub> = Drain time = 2WQV/Q <sub>WQV</sub>	≤ 72-hrs
71.67	feet	E <sub>FC</sub> = Elevation of the bottom of the filter course material <sup>2</sup>	
70.75	feet	E <sub>UD</sub> = Invert elevation of the underdrain (UD), if applicable	
68.10	feet	E <sub>SHWT</sub> = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
68.10	feet	E <sub>ROCK</sub> = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
0.92	feet	D <sub>FC to UD</sub> = Depth to UD from the bottom of the filter course	≥ 1'
3.57	feet	D <sub>FC to ROCK</sub> = Depth to bedrock from the bottom of the filter course	≥ 1'
3.57	feet	D <sub>FC to SHWT</sub> = Depth to SHWT from the bottom of the filter course	≥ 1'
72.17	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
73.50	ft	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
<b>If a surface sand filter or underground sand filter is proposed:</b>			
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	≥ 75%WQV
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sheet		Note what sheet in the plan set contains the filter course specification.	
Yes/No		Access grate provided?	← yes

YES	ac	Drainage Area no larger than 5 ac?	← yes
	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	≥ WQV
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sheet		Note what sheet in the plan set contains the filter course specification	
	:1	Pond side slopes	≥ 3:1
Sheet		Note what sheet in the plan set contains the planting plans and surface cover	
<b>If porous pavement is proposed:</b>			
	ASPHALT	Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	0.1 acres	A <sub>SA</sub> = Surface area of the pervious pavement	
2.3	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	12.0 inches	D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA
Sheet	D1	Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- Designer's Notes:**

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**PROPOSED**

Prepared by Jones &amp; Beach Engineers Inc

HydroCAD® 10.20-6a s/n 00762 © 2024 HydroCAD Software Solutions LLC

Type III 24-hr 50 YEAR Rainfall=7.44"

Printed 8/5/2025

Page 1

**Stage-Area-Storage for Pond P1: POROUS ASPHALT**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
70.49	4,251	0	73.09	4,251	2,229
70.54	4,251	32	73.14	4,251	2,292
70.59	4,251	64	73.19	4,251	2,337
70.64	4,251	96	73.24	4,251	2,369
70.69	4,251	128	73.29	4,251	2,401
70.74	4,251	159	73.34	4,251	2,433
70.79	4,275	245	73.39	4,251	2,465
70.84	4,284	332	73.44	4,251	2,497
70.89	<b>4,288</b>	418	73.49	4,251	2,528
70.94	<b>4,288</b>	505	73.54	4,251	2,741
70.99	4,284	592	73.59	4,251	2,954
71.04	4,276	678	73.64	4,251	3,166
71.09	4,251	764	73.69	4,251	3,379
71.14	4,251	849	73.74	4,251	3,591
71.19	4,251	934	73.79	4,251	3,804
71.24	4,251	1,019	73.84	4,251	4,016
71.29	4,251	1,104	73.89	4,251	4,229
71.34	4,251	1,189	73.94	4,251	4,441
71.39	4,251	1,274	73.99	4,251	<b>4,654</b>
71.44	4,251	1,327			
71.49	4,251	1,359			
71.54	4,251	1,391			
71.59	4,251	1,423			
71.64	4,251	<b>1,455</b>			
71.69	4,251	<b>1,474</b>			
71.74	4,251	1,485			
71.79	4,251	1,495			
71.84	4,251	1,506			
71.89	4,251	1,517			
71.94	4,251	1,527			
71.99	4,251	1,538			
72.04	4,251	1,549			
72.09	4,251	1,559			
72.14	4,251	1,570			
72.19	4,251	1,580			
72.24	4,251	1,591			
72.29	4,251	1,602			
72.34	4,251	1,612			
72.39	4,251	1,623			
72.44	4,251	1,634			
72.49	4,251	1,644			
72.54	4,251	1,655			
72.59	4,251	1,665			
72.64	4,251	1,676			
72.69	4,251	1,719			
72.74	4,251	1,782			
72.79	4,251	1,846			
72.84	4,251	1,910			
72.89	4,251	<b>1,974</b>			
72.94	4,251	<b>2,037</b>			
72.99	4,251	2,101			
73.04	4,251	2,165			

**WQV REQUIRED = 555 C.F.****BOTTOM OF FILTER COURSE = 71.67****STORAGE @ 71.67 = 1,470 C.F.****1,470 C.F. + 555 C.F. = 2,025 C.F.****WQV ELEVATION = 72.93**

**PROPOSED**

Prepared by Jones &amp; Beach Engineers Inc

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Type III 24-hr 50 YEAR Rainfall=7.44"

Printed 8/5/2025

Page 2

**Stage-Discharge for Pond P1: POROUS ASPHALT**

Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)	Elevation (feet)	Discharge (cfs)	Discarded (cfs)	Primary (cfs)
70.49	0.00	0.00	0.00	73.09	0.55	0.06	0.49
70.54	0.02	0.02	0.00	73.14	0.56	0.06	0.49
70.59	0.03	0.03	0.00	73.19	0.56	0.06	0.50
70.64	0.03	0.03	0.00	73.24	0.57	0.06	0.51
70.69	0.03	0.03	0.00	73.29	0.58	0.06	0.51
70.74	0.03	0.03	0.00	73.34	0.58	0.07	0.52
70.79	0.04	0.03	0.00	73.39	0.59	0.07	0.52
70.84	0.05	0.03	0.01	73.44	0.59	0.07	0.53
70.89	0.06	0.03	0.03	73.49	0.60	0.07	0.53
70.94	0.08	0.04	0.05	73.54	0.60	0.07	0.54
70.99	0.11	0.04	0.07	73.59	0.61	0.07	0.54
71.04	0.13	0.04	0.10	73.64	0.62	0.07	0.55
71.09	0.16	0.04	0.12	73.69	0.62	0.07	0.55
71.14	0.18	0.04	0.15	73.74	0.63	0.07	0.56
71.19	0.20	0.04	0.16	73.79	0.63	0.07	0.56
71.24	0.22	0.04	0.18	73.84	0.64	0.07	0.57
71.29	0.24	0.04	0.20	73.89	0.64	0.07	0.57
71.34	0.26	0.04	0.21	73.94	0.65	0.07	0.58
71.39	0.27	0.04	0.23	73.99	<b>0.65</b>	<b>0.07</b>	<b>0.58</b>
71.44	0.28	0.04	0.24				
71.49	0.29	0.04	0.25				
71.54	0.30	0.04	0.26				
71.59	0.32	0.04	0.27				
71.64	0.33	0.04	0.28				
71.69	0.34	0.04	0.29				
71.74	0.35	0.05	0.30				
71.79	0.36	0.05	0.31				
71.84	0.37	0.05	0.32				
71.89	0.37	0.05	0.33				
71.94	0.38	0.05	0.34				
71.99	0.39	0.05	0.34				
72.04	0.40	0.05	0.35				
72.09	0.41	0.05	0.36				
72.14	0.42	0.05	0.37				
72.19	0.43	0.05	0.37				
72.24	0.43	0.05	0.38				
72.29	0.44	0.05	0.39				
72.34	0.45	0.05	0.40				
72.39	0.46	0.05	0.40				
72.44	0.46	0.05	0.41				
72.49	0.47	0.05	0.42				
72.54	0.48	0.06	0.42				
72.59	0.48	0.06	0.43				
72.64	0.49	0.06	0.44				
72.69	0.50	0.06	0.44				
72.74	0.51	0.06	0.45				
72.79	0.51	0.06	0.45				
72.84	0.52	0.06	0.46				
72.89	0.53	0.06	0.47				
72.94	0.53	0.06	0.47				
72.99	0.54	0.06	0.48				
73.04	0.54	0.06	0.48				

**WQV ELEVATION = 72.93****DISCHARGE @ 72.93  
= 0.47 C.F.S.**

## APPENDIX 8

### RIP RAP CALCULATIONS



## RIP RAP CALCULATIONS

35 Madbury Road  
Durham, NH

**Jones & Beach Engineers, Inc.**

P.O. Box 219  
Stratham, NH 03885  
6-Aug-25

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire*.  
Aprons are sized for the 25-Year storm event.

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### TAILWATER < HALF THE $D_o$

$$L_a = (1.8 \times Q) / D_o^{3/2} + (7 \times D_o)$$

$$W = L_a + (3 \times D_o) \text{ or defined channel width}$$

$$d_{50} = (0.02 \times Q^{4/3}) / (T_w \times D_o)$$

Culvert or Catch Basin (Sta. No.)	Tailwater (Feet) $T_w$	Discharge (C.F.S.) $Q$	Diameter of Pipe $D_o$	Length of Rip Rap $L_a$ (feet)	Width of Rip Rap $W$ (feet)	$d_{50}$ -Median Stone Rip Rap $d_{50}$ (feet)
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### TAILWATER > HALF THE $D_o$

$$L_a = (3.0 \times Q) / D_o^{3/2} + (7 \times D_o)$$

$$W = (0.4 \times L_a) + (3 \times D_o) \text{ or defined channel width}$$

$$d_{50} = (0.02 \times Q^{4/3}) / (T_w \times D_o)$$

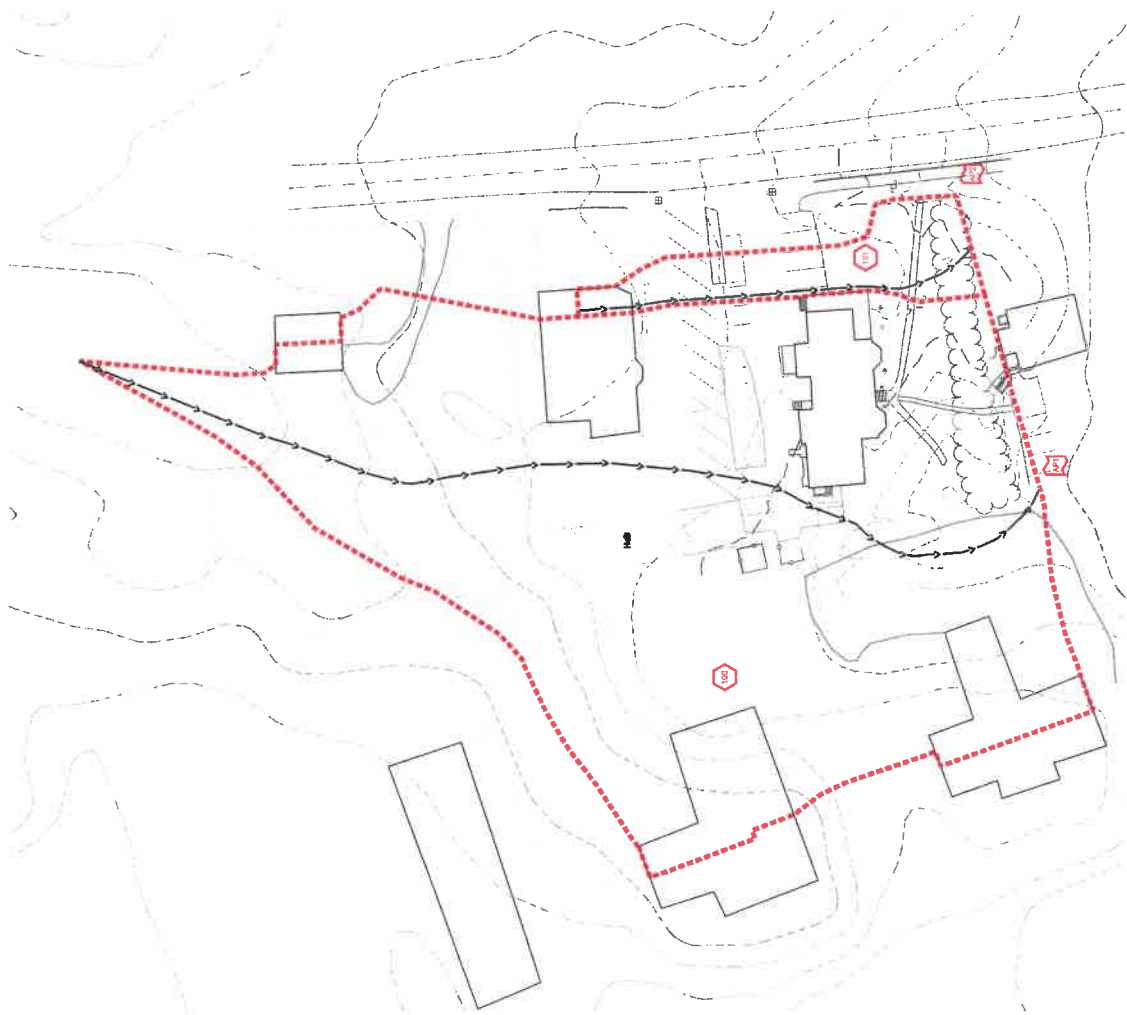
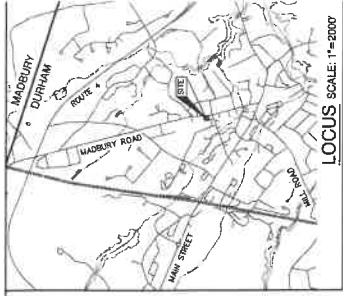
Culvert or Catch Basin (Sta. No.)	Tailwater (Feet) $T_w$	Discharge (C.F.S.) $Q$	Diameter of Pipe $D_o$	Length of Rip Rap $L_a$ (feet)	Width of Rip Rap $W$ (feet)	$d_{50}$ -Median Stone Rip Rap $d_{50}$ (feet)
4" HDPE	0.33	0.29	0.33	6.9	4	0.04

Table 7-24 -- Recommended Rip Rap Gradation Ranges			
d <sub>50</sub> Size =	0.25	Feet	3 Inches
% of Weight Smaller Than the Given d <sub>50</sub> Size	Size of Stone (Inches)		
	From	To	
100%	5	6	
85%	4	5	
50%	3	5	
15%	1	2	

Table 7-24 -- Recommended Rip Rap Gradation Ranges			
d <sub>50</sub> Size =	0.5	Feet	6 Inches
% of Weight Smaller Than the Given d <sub>50</sub> Size	Size of Stone (Inches)		
	From	To	
100%	9	12	
85%	8	11	
50%	6	9	
15%	2	3	

APPENDIX 10

WATERSHED PLANS



- LEGEND**
- SUBCATCHMENT BOUNDARY
  - SUBCATCHMENT
  - REACH
  - POND
  - TC PATH

**SOIL LEGEND**

SYMBOL	NAME	USE
H-6B	HOLLIS-CHARLTON FINE SANDY LOAMS	D



PROJECT PART  
1.0000000000000000  
1.0000000000000000  
1.0000000000000000

APPLICATION  
1.0000000000000000  
1.0000000000000000  
1.0000000000000000

TOTAL LOT AREA  
1.0000000000000000  
1.0000000000000000  
1.0000000000000000

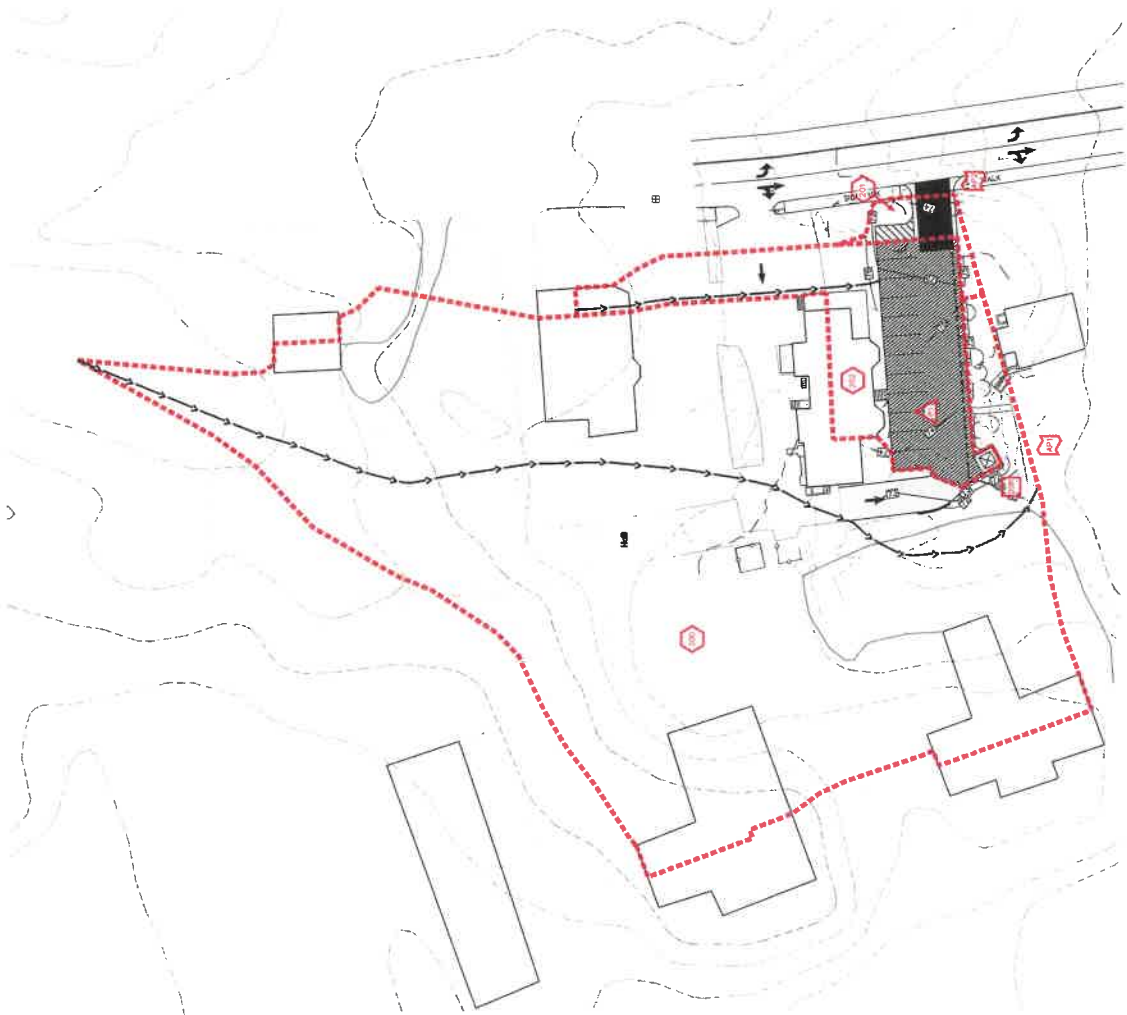
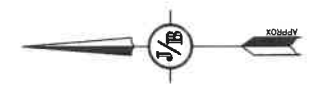
DRAWN  
W  
SHEET  
1 OF 1  
DATE  
10/10/2018

Plan Name: EXISTING WATERSHED PLAN  
Project: 35 MADBURY ROAD DURHAM, NH  
Owner of Record: DWS 35, LLC 288 CALEF HIGHWAY, LEE, NH 03861

J/B Jones & Beach Engineers, Inc.  
Civil Engineering Services  
85 Portsmouth Ave  
PO Box 219  
Durham, NH 03825  
E-MAIL: JBE@JONESANDBEACH.COM  
603-772-4746

REV.	DATE	BY	REVISION
1	08/06/20	NLE	REVISED PER SITE MODIFICATION
0	07/06/20	NLE	ISSUED FOR REVIEW

Design: NLE Draft: NLE Date: 08/06/2018  
Checked: PSL Scale: AS SHOWN Project: No. 25078  
Drawing Name: 25078-WATERSHED.dwg  
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE).  
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.



- LEGEND**
- SUBCATCHMENT BOUNDARY (Red dashed line)
  - SUBCATCHMENT (Red dashed line with 'X' symbol)
  - REACH (Black line with arrows)
  - POND (Red triangle symbol)
  - TC PATH (Black line with arrows)



PROJECT PART  
TOWN OF DURHAM  
TAX MAP 106, LOT 10

APPLICATION  
DWS 35, LLC  
280 CALEF HIGHWAY  
LEE, NH 03861

TOTAL LOT AREA  
±18,000 SQ. FT.  
±0.42 ACRES

DRAWN  
W  
SHEET  
JES PROVED

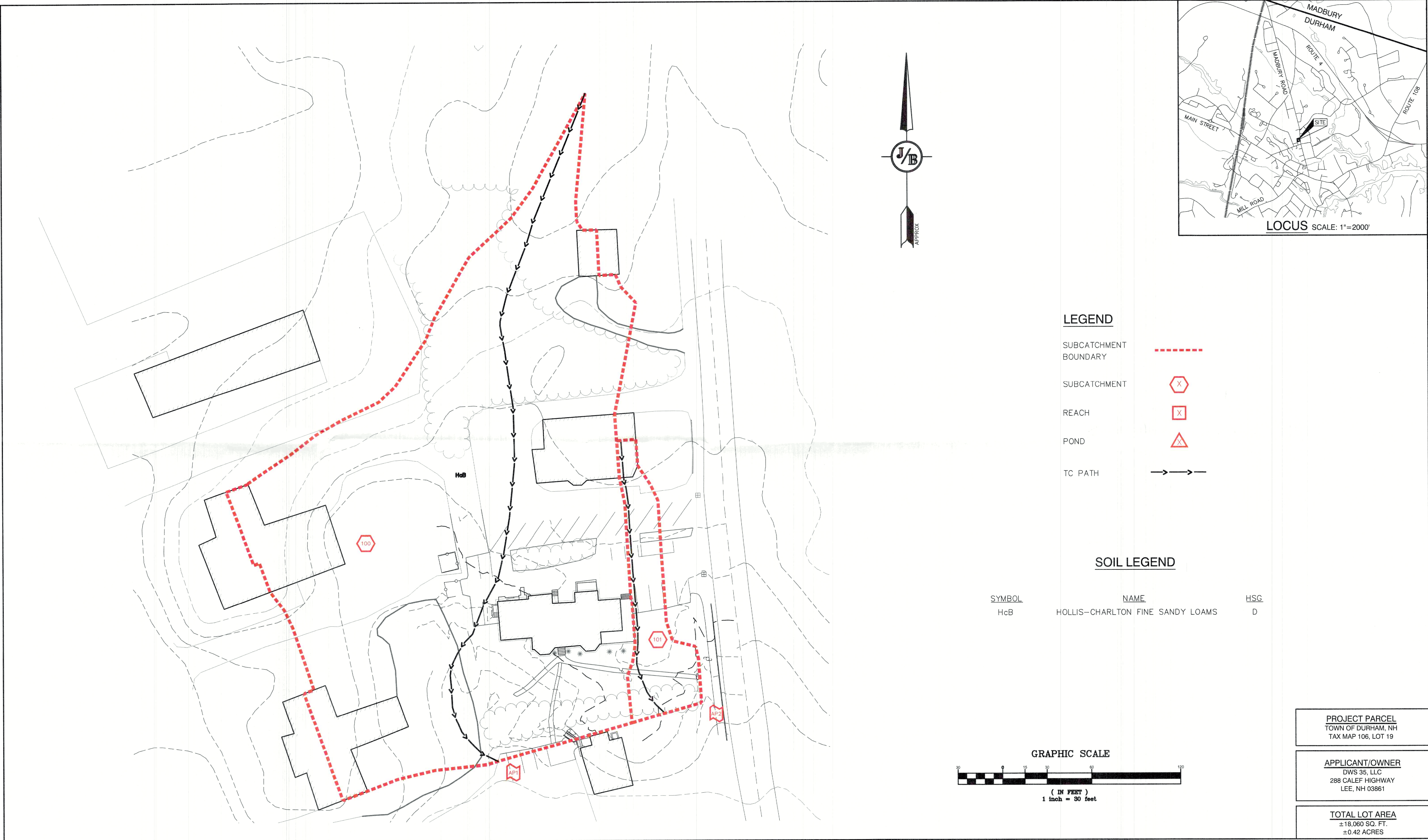
Plan Name: **PROPOSED WATERSHED PLAN**  
Project: **35 MADBURY ROAD  
DURHAM, NH**  
Owner of Record: **DWS 35, LLC  
280 CALEF HIGHWAY, LEE, NH 03861**

Designed and Produced in NH  
**J/B Jones & Beach Engineers, Inc.**  
Civil Engineering Services  
85 Portsmouth Ave.  
PO Box 219  
Durham, NH 03826  
603-772-4749  
E-MAIL: JBE@JONESANDBEACH.COM

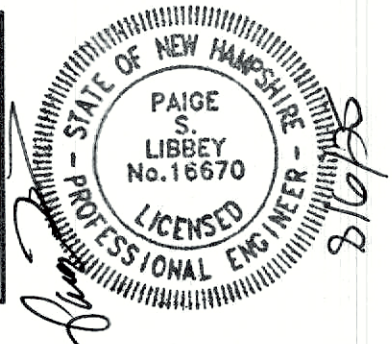
REV.	DATE	REVISION	BY
1	06/04/25	REVISED PER SITE MODIFICATION	N/L
0	07/02/25	ISSUED FOR REVIEW	N/L

Design: TLL | Draft: N/L | Date: 06/24/2025  
Checked: FSL | Scale: AS SHOWN | Project No: 25073  
Drawing Name: 25073-WATERSHED.dwg  
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN  
CONSENT OF THE ENGINEER. ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE  
AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.





Design: NJL	Draft: NJL	Date: 06/25/2025
Checked: PSL	Scale: AS SHOWN	Project No.: 25073
Drawing Name: 25073-WATERSHED.dwg		
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REV.	DATE	REVISION	BY
1	08/06/25	REVISED PER SITE MODIFICATION	NJL
0	07/02/25	ISSUED FOR REVIEW	NJL

**J/B**  
85 Portsmouth Ave.  
PO Box 219  
Stratham, NH 03885

Designed and Produced in NH

**Jones & Beach Engineers, Inc.**

Civil Engineering Services

603-772-4746  
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	<b>EXISTING WATERSHED PLAN</b>
Project:	<b>35 MADBURY ROAD DURHAM, NH</b>
Owner of Record:	<b>DWS 35, LLC 288 CALEF HIGHWAY, LEE, NH 03861</b>

DRAWING No.

**W1**

SHEET 1 OF 2  
JBE PROJECT NO. 25073

PROJECT PARCEL  
TOWN OF DURHAM, NH  
TAX MAP 106, LOT 19

APPLICANT/OWNER  
DWS 35, LLC  
288 CALEF HIGHWAY  
LEE, NH 03861

TOTAL LOT AREA  
±18,060 SQ. FT.  
±0.42 ACRES



