## **DRAINAGE ANALYSIS**

## **FOR**

## **RiverWoods Phase II**

Stone Quarry Drive Durham, NH

**Tax Map 209 Lot 33** 

July 23, 2025

Prepared For:

## The RiverWoods Durham

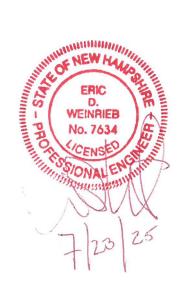
14 Stone Quarry Drive Durham, NH 03824

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# Section 1

# Narrative



## PROJECT DESCRIPTION

The RiverWoods Durham is proposing to construct a second phase on an undeveloped parcel adjacent to the existing RiverWoods continuing care retirement community campus in Durham, New Hampshire. The 22.5-acre property is identified as Assessor's Map 209, Lot 33 and is located in the Office Research District. The project site is primarily woodland with sections forested wetland. Access is from NH 108 via the existing Stone Quarry Drive.

The proposal includes two new age-restricted multi-family housing buildings, a community center and a maintenance garage together with associated accessways and parking areas, utilities and stormwater infrastructure. These measures will include four bioretention ponds and a section of porous pavement. Pretreatment will be provided by catch basins with deep sumps and grease hoods. This proposed stormwater management system will reduce peak flows and treat runoff from the site's impervious areas prior to leaving the site.

#### Site Soils

Michael Cuomo, NH soils scientist completed a site-specific soil survey (SSSS) for the project site. This survey indicates that the subject property can be broken into hydrologic soils groups (HSG) B, C and D. Test pits indicate that majority of the soils underlying the development area are comprised of clay. Information on soils in offsite areas was taken from a high intensity soil survey (HISS) done for the adjacent RiverWoods campus in 2018 and NRCS maps.

## Pre-Development (Existing Conditions)

Runoff generally flows through and off the site in a southerly direction to three points of analysis. POA #1 is an existing culvert under Stone Quarry Drive that captures flow from the western corner of the parcel. POA #2 is an offsite wetland to which the majority of the site and some offsite areas are directed. This offsite area was included as it represents the confluence of two wetland systems and an area affected by the relocation of Stone Quarry Drive. POA #3 is the southern property line where an existing stream captures the southeast portion of the lot. The sites hydrology is characterized by five existing subcatchments as delineated on the accompanying "Pre-Development Watershed Plan".

## Post-Development (Proposed Conditions)

The post-development conditions were analyzed at the same discharge points as the predevelopment conditions as delineated on the accompanying "Post-Development Watershed Plan". Modifications to the delineated areas and associated ground cover were made to subcatchments to account for the proposed improvements to the property. As shown on the attached Post-Development Watershed Plan, the site was divided into forty post-development subcatchment areas. Site topography, existing features, proposed site improvements, proposed grading, drainage and erosion control measures are shown on the accompanying plan set. Recommended erosion control measures are based upon the December 2008 edition of the "New Hampshire Stormwater Manual Volumes 1 through 3" prepared by NHDES and Comprehensive Environmental, Inc. as amended.

#### **CALCULATION METHODS**

The drainage study was completed using the USDA SCS TR-20 Method within the HydroCAD Stormwater Modeling System. Reservoir routing was performed with the Dynamic Storage Indication method with automated calculation of tailwater conditions. A Type III 24-hour rainfall distribution was utilized in analyzing the data for the 2, 10 and 25 year - 24-hour storm events using rainfall data provided by the Northeast Regional Climate Center (NRCC). As the project site lies within a Coastal and Great Bay Community identified by NHDES Alteration of Terrain, all rainfall amounts were increased by 15% to account for potential future increases in rainfall due to climate change. A time span of 0 to 48 hours was analyzed at 0.01-hour increments. Design infiltration rates used in the analysis were taken from the corresponding test pit logs. Pond summaries for the 100-year storm event are also included in the proposed analysis.

#### Disclaimer

Altus Engineering, Inc. notes that stormwater modeling is limited in its capacity to precisely predict peak rates of runoff and flood elevations. Results should not be considered to represent actual storm events due to the number of variables and assumptions involved in the modeling effort. Surface roughness coefficients (n), entrance loss coefficients (ke), velocity factors (kv) and times of concentration (Tc) are based on subjective field observations and engineering judgment using available data. For design purposes, curve numbers (Cn) describe the average conditions. However, curve numbers will vary from storm to storm depending on the antecedent runoff conditions (ARC) including saturation and frozen ground. Also, higher water elevations than predicted by modeling could occur if drainage channels, closed drain systems or culverts are not maintained and/or become blocked by debris before and/or during a storm event as this will impact flow capacity of the structures. Structures should be re-evaluated if future changes occur within relevant drainage areas in order to assess any required design modifications.

## Drainage Analysis

A complete summary of the drainage model is included in the appendix of this report. The following tables compare pre- and post-development peak rates and volumes at the Point of Analysis identified on the plans for the 1", 2, 10 and 25-year storm events:

Stormwater Modeling Summary
Peak Q (cfs) for Type III 24-Hour Storm Events

	1" Storm	2-Yr Storm	10-Yr Storm	25-Yr Storm
	(1.00 inch)	(3.61 inch)	(5.47 inch)	(6.93 inch)
POA #1 (West to CB)				
Pre	0.01	2.40	4.26	5.12
Post	0.01	2.02	3.74	4.75
Change	0.00	-0.38	-0.52	-0.37
POA #2 (South to Wetland)				
Pre	0.05	15.07	27.12	34.48
Post	0.10	13.31	23.08	30.05
Change	0.05	-1.76	-4.04	-4.43
POA #3 (South to Wetland)				
Pre	0.00	6.43	16.14	24.80
Post	0.04	5.85	15.75	24.24
Change	0.04	-0.58	-0.39	-0.56

As the above table demonstrates, the proposed peak rates of runoff at the points of analysis will match or be decreased from the existing conditions for all analyzed storm events with the exception of the 1" event where the increases have been determined to be insignificant due to the fact that they total no more than 0.05 cfs and because decreases are shown in all larger storms. A decrease in the 1" storm is also not a requirement of the Town of Durham.

The following table demonstrates the pre- and post- volumes of runoff. As shown in the attached calculations, the use of porous pavement allows the infiltration of the town's requisite groundwater recharge volume which exceeds that required by the NHDES.

## Stormwater Modeling Summary Volume V (af) for Type III 24-Hour Storm Events

	1" Storm	2-Yr Storm	10-Yr Storm	25-Yr Storm
	(1.00 inch)	(3.61 inch)	(5.47 inch)	(6.93 inch)
POA #1 (West to CB)				
Pre	0.004	0.215	0.448	0.650
Post	0.008	0.212	0.424	0.606
Change	0.004	-0.003	-0.024	-0.044
POA #2 (South to Wetland)				
Pre	0.038	2.198	4.597	6.679
Post	0.057	2.170	4.509	6.538
Change	0.019	-0.028	-0.088	-0.141
POA #3 (South to Wetland)				
Pre	0.001	0.691	1.589	2.399
Post	0.064	0.966	1.987	2.882
Change	0.063	0.275	0.398	0.483

## POLLUTANT REMOVAL

Based on the New Hampshire Stormwater Manual (Volume 2), the following pollutant removal rates would be expected from the implementation of the proposed stormwater BMPs:

<u>BMP</u>	<u>Pollutant</u>	Removal Efficiency
Deep Sump Ca	atch Basin -	
	Total Suspended Solids (TSS)	15%
	Total Nitrogen (TN)	5%
	Total Phosphorus (TP)	5%
Bioretention P	ond -	
	Total Suspended Solids (TSS)	90%
	Total Nitrogen (TN)	65%
	Total Phosphorus (TP)	65%
Porous Pavem	ent -	
	Total Suspended Solids (TSS)	90%
	Total Nitrogen (TN)	60%
	Total Phosphorus (TP)	65%

#### **CONCLUSION**

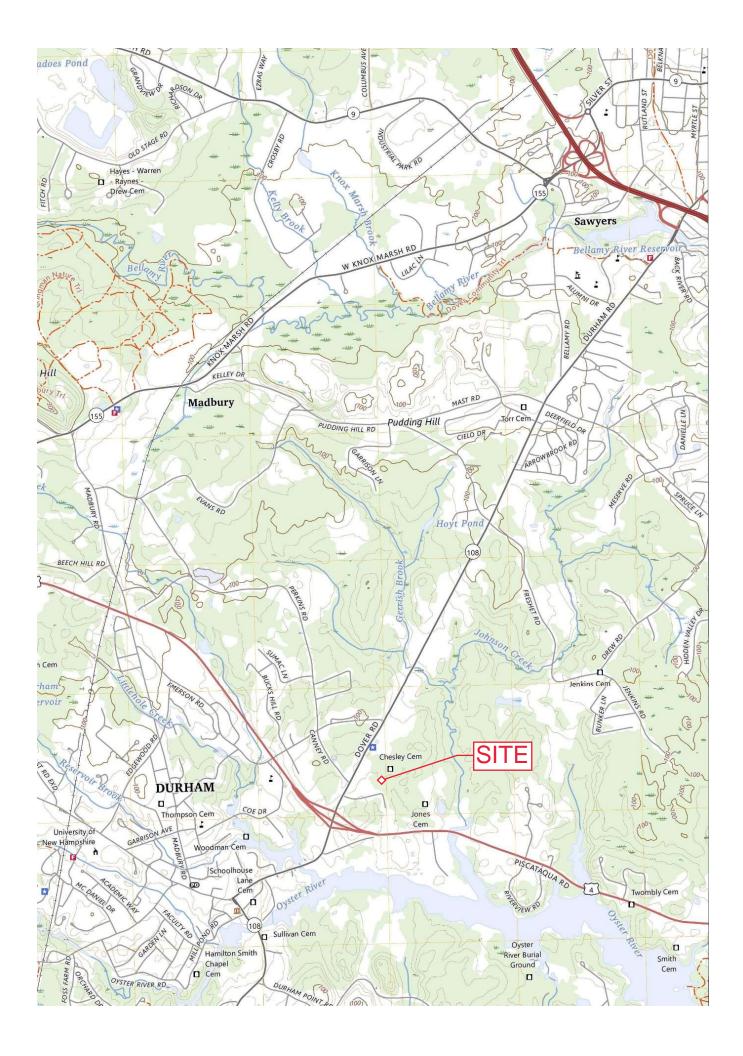
This proposed development of property located on Stone Quarry Drive in Durham, New Hampshire will have minimal adverse effect on abutting properties and infrastructure as a result of stormwater runoff or siltation. Post-construction peak rates of runoff from the site will be at or lower than the existing conditions for all analyzed storm events with the insignificant exceptions noted above. The new stormwater management system will also provide appropriate treatment to and infiltration of runoff from the proposed impervious surfaces. Appropriate steps will be taken to properly mitigate erosion and sedimentation through the use of temporary and permanent Best Management Practices for sediment and erosion control, including deep sump catch basins with grease hoods, bioretention ponds and porous pavement.

# Section 2

# Aerial Photo and USGS Map





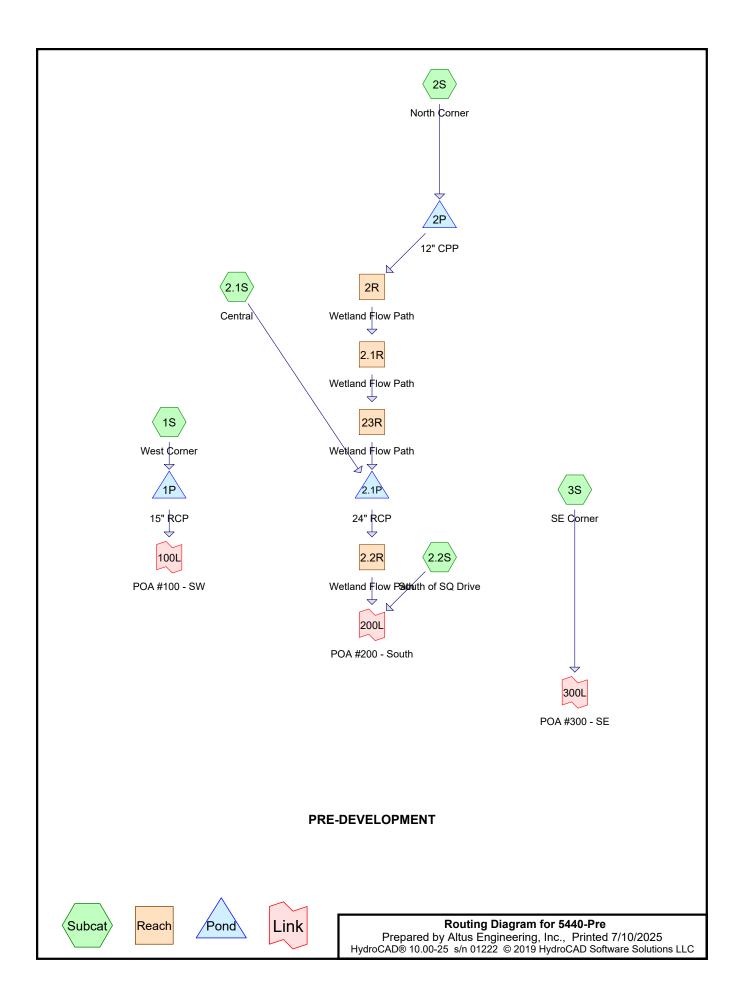


## Section 3

# **Drainage Calculations**

Pre-Development 2-Year, 24-Hour Summary 10-Year, 24-Hour Complete 25-Year, 24-Hour Summary





## 5440-Pre

Prepared by Altus Engineering, Inc.

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Corner Runoff Area = 85,332 sf 8.89% Impervious Runoff Depth = 0.02"

Flow Length=366' Tc=9.8 min CN=74 Runoff=0.01 cfs 0.004 af

Subcatchment 2.1S: Central Runoff Area=494,247 sf 8.83% Impervious Runoff Depth=0.02"

Flow Length=1,341' Tc=15.8 min CN=74 Runoff=0.04 cfs 0.022 af

Subcatchment 2.2S: South of SQ Drive Runoff Area=105,068 sf 10.77% Impervious Runoff Depth=0.05"

Flow Length=391' Tc=6.0 min CN=77 Runoff=0.03 cfs 0.010 af

Subcatchment 2S: North Corner Runoff Area = 284,221 sf 6.78% Impervious Runoff Depth = 0.01"

Tc=0.0 min CN=72 Runoff=0.01 cfs 0.007 af

Subcatchment 3S: SE Corner Runoff Area=373,920 sf 2.67% Impervious Runoff Depth=0.00"

Flow Length=1,149' Tc=15.9 min CN=68 Runoff=0.00 cfs 0.001 af

Reach 2.1R: Wetland Flow Path

Avg. Flow Depth=0.02' Max Vel=0.23 fps Inflow=0.01 cfs 0.007 af

n=0.040 L=344.0' S=0.0075'/' Capacity=54.59 cfs Outflow=0.01 cfs 0.007 af

Reach 2.2R: Wetland Flow Path

Avg. Flow Depth=0.03' Max Vel=0.74 fps Inflow=0.04 cfs 0.028 af

n=0.040 L=263.0' S=0.0502'/' Capacity=141.18 cfs Outflow=0.04 cfs 0.028 af

Reach 2R: Wetland Flow Path

Avg. Flow Depth=0.01' Max Vel=0.57 fps Inflow=0.01 cfs 0.007 af

n=0.040 L=151.0' S=0.0446'/' Capacity=133.09 cfs Outflow=0.01 cfs 0.007 af

Reach 23R: Wetland Flow Path Avg. Flow Depth=0.01' Max Vel=0.36 fps Inflow=0.01 cfs 0.007 af

n=0.040 L=131.0' S=0.0185 '/' Capacity=85.86 cfs Outflow=0.01 cfs 0.007 af

Pond 1P: 15" RCP Peak Elev=52.31' Storage=1 cf Inflow=0.01 cfs 0.004 af

15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=0.01 cfs 0.004 af

Pond 2.1P: 24" RCP Peak Elev=47.65' Storage=8 cf Inflow=0.04 cfs 0.028 af

24.0" Round Culvert n=0.012 L=78.0' S=0.0135 '/' Outflow=0.04 cfs 0.028 af

**Pond 2P: 12" CPP** Peak Elev=59.70' Storage=30 cf Inflow=0.01 cfs 0.007 af

Outflow=0.01 cfs 0.007 af

Link 100L: POA #100 - SW Inflow=0.01 cfs 0.004 af

Primary=0.01 cfs 0.004 af

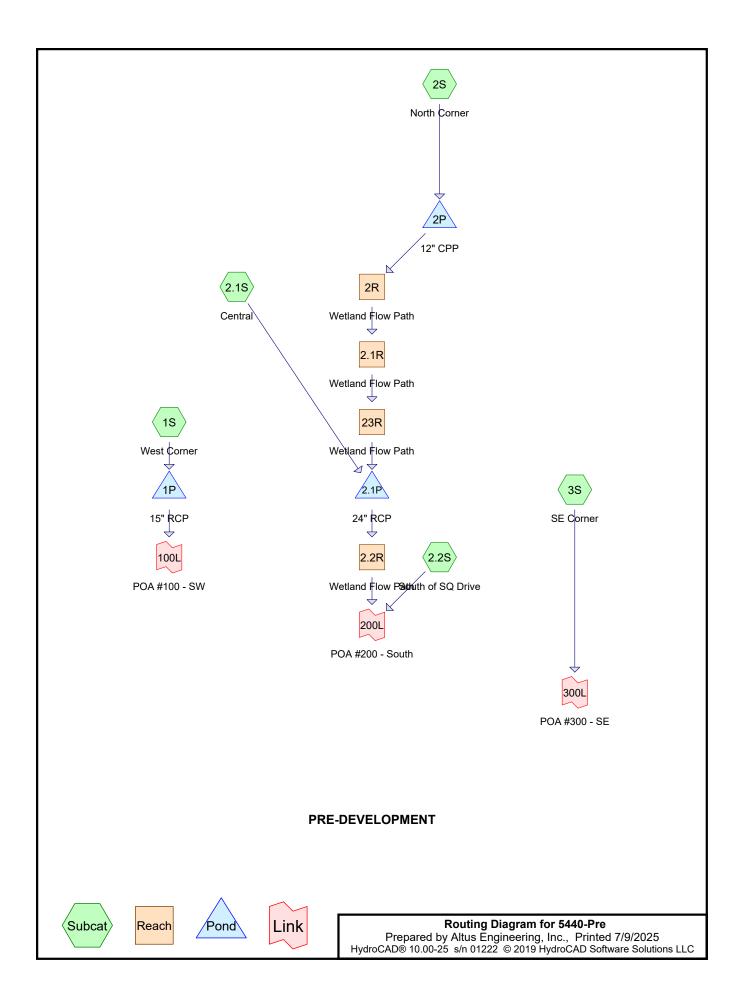
Link 200L: POA #200 - South Inflow=0.05 cfs 0.038 af

Primary=0.05 cfs 0.038 af

Link 300L: POA #300 - SE Inflow=0.00 cfs 0.001 af

Primary=0.00 cfs 0.001 af

Total Runoff Area = 30.826 ac Runoff Volume = 0.042 af Average Runoff Depth = 0.02" 93.16% Pervious = 28.718 ac 6.84% Impervious = 2.108 ac



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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Corner Runoff Area=85,332 sf 8.89% Impervious Runoff Depth=1.32"

Flow Length=366' Tc=9.8 min CN=74 Runoff=2.56 cfs 0.215 af

Subcatchment 2.1S: Central Runoff Area=494,247 sf 8.83% Impervious Runoff Depth=1.32"

Flow Length=1,341' Tc=15.8 min CN=74 Runoff=12.48 cfs 1.245 af

**Subcatchment 2.2S: South of SQ Drive** Runoff Area=105,068 sf 10.77% Impervious Runoff Depth=1.51"

Flow Length=391' Tc=6.0 min CN=77 Runoff=4.22 cfs 0.304 af

Subcatchment 2S: North Corner Runoff Area=284,221 sf 6.78% Impervious Runoff Depth=1.19"

Tc=0.0 min CN=72 Runoff=10.62 cfs 0.649 af

Subcatchment 3S: SE Corner Runoff Area=373,920 sf 2.67% Impervious Runoff Depth=0.97"

Flow Length=1,149' Tc=15.9 min CN=68 Runoff=6.43 cfs 0.691 af

Reach 2.1R: Wetland Flow Path

Avg. Flow Depth=0.45' Max Vel=1.48 fps Inflow=2.22 cfs 0.649 af

n=0.040 L=344.0' S=0.0075 '/' Capacity=54.59 cfs Outflow=2.22 cfs 0.649 af

Reach 2.2R: Wetland Flow Path Avg. Flow Depth=0.68' Max Vel=4.79 fps Inflow=13.20 cfs 1.894 af

n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=13.19 cfs 1.894 af

Reach 2R: Wetland Flow Path

Avg. Flow Depth=0.28' Max Vel=2.78 fps Inflow=2.23 cfs 0.649 af

n=0.040 L=151.0' S=0.0446 '/' Capacity=133.09 cfs Outflow=2.22 cfs 0.649 af

Reach 23R: Wetland Flow Path Avg. Flow Depth=0.35' Max Vel=2.04 fps Inflow=2.22 cfs 0.649 af

n=0.040 L=131.0' S=0.0185 '/' Capacity=85.86 cfs Outflow=2.22 cfs 0.649 af

Pond 1P: 15" RCP Peak Elev=53.20' Storage=137 cf Inflow=2.56 cfs 0.215 af

15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=2.40 cfs 0.215 af

Pond 2.1P: 24" RCP Peak Elev=49.33' Storage=2,463 cf Inflow=14.47 cfs 1.894 af

24.0" Round Culvert n=0.012 L=78.0' S=0.0135 '/' Outflow=13.20 cfs 1.894 af

Pond 2P: 12" CPP Peak Elev=60.71' Storage=8,446 cf Inflow=10.62 cfs 0.649 af

Outflow=2.23 cfs 0.649 af

Link 100L: POA #100 - SW Inflow=2.40 cfs 0.215 af

Primary=2.40 cfs 0.215 af

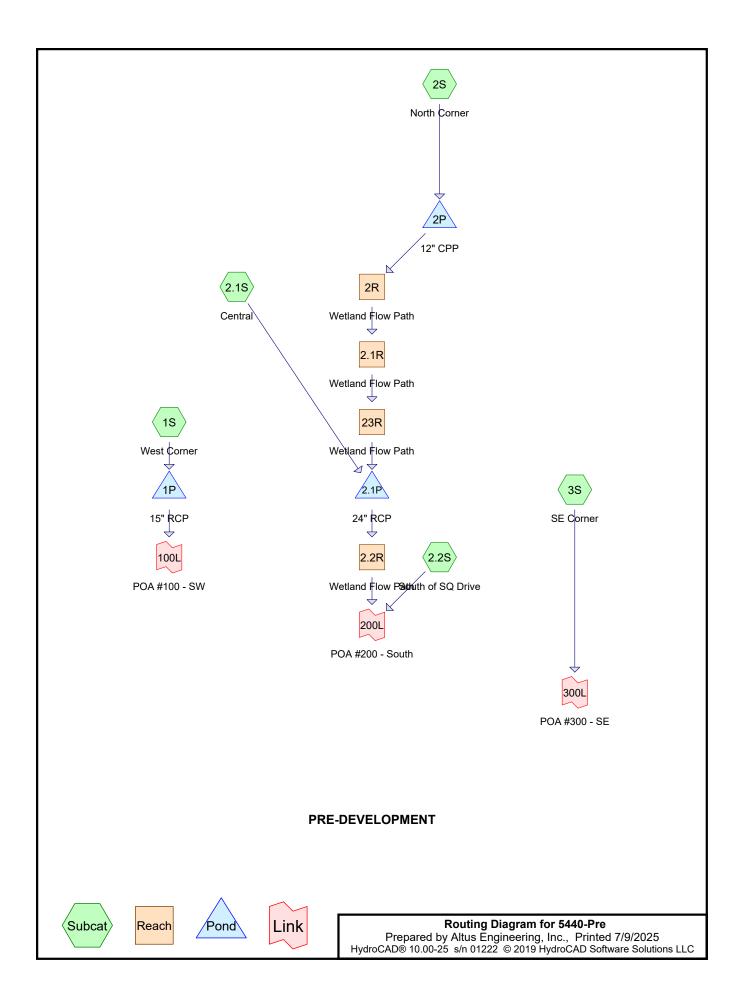
Link 200L: POA #200 - South Inflow=15.07 cfs 2.198 af

Primary=15.07 cfs 2.198 af

Link 300L: POA #300 - SE Inflow=6.43 cfs 0.691 af

Primary=6.43 cfs 0.691 af

Total Runoff Area = 30.826 ac Runoff Volume = 3.103 af Average Runoff Depth = 1.21" 93.16% Pervious = 28.718 ac 6.84% Impervious = 2.108 ac



## Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.039	61	>75% Grass cover, Good, HSG B (2.1S, 3S)
3.140	74	>75% Grass cover, Good, HSG C (1S, 2.1S, 2S, 3S)
0.087	80	>75% Grass cover, Good, HSG D (2.1S, 2S)
0.243	65	Brush, Good, HSG C (2.1S)
0.039	98	Paved parking, HSG B (2.1S, 3S)
1.406	98	Paved parking, HSG C (2.1S, 2.2S, 2S, 3S)
0.227	98	Paved parking, HSG D (2.1S, 2.2S, 2S)
0.174	98	Paved roads w/curbs & sewers, HSG C (1S)
0.261	98	Roofs, HSG C (2.1S, 2S)
2.232	55	Woods, Good, HSG B (1S, 2.1S, 2S, 3S)
19.669	70	Woods, Good, HSG C (1S, 2.1S, 2.2S, 2S, 3S)
3.308	77	Woods, Good, HSG D (2.1S, 2.2S, 2S)
30.826	72	TOTAL AREA

## Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
2.310	HSG B	1S, 2.1S, 2S, 3S
24.894	HSG C	1S, 2.1S, 2.2S, 2S, 3S
3.622	HSG D	2.1S, 2.2S, 2S
0.000	Other	
30.826		TOTAL AREA

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Corner Runoff Area=85,332 sf 8.89% Impervious Runoff Depth=2.74"

Flow Length=366' Tc=9.8 min CN=74 Runoff=5.53 cfs 0.448 af

Subcatchment 2.1S: Central Runoff Area=494,247 sf 8.83% Impervious Runoff Depth=2.74"

Flow Length=1,341' Tc=15.8 min CN=74 Runoff=26.96 cfs 2.595 af

Subcatchment 2.2S: South of SQ Drive Runoff Area=105,068 sf 10.77% Impervious Runoff Depth=3.02"

Flow Length=391' Tc=6.0 min CN=77 Runoff=8.55 cfs 0.607 af

Subcatchment 2S: North Corner Runoff Area=284,221 sf 6.78% Impervious Runoff Depth=2.57"

Tc=0.0 min CN=72 Runoff=23.92 cfs 1.395 af

Subcatchment 3S: SE Corner Runoff Area=373,920 sf 2.67% Impervious Runoff Depth=2.22"

Flow Length=1,149' Tc=15.9 min CN=68 Runoff=16.14 cfs 1.589 af

Reach 2.1R: Wetland Flow Path Avg. Flow Depth=1.19' Max Vel=2.53 fps Inflow=18.63 cfs 1.395 af

n=0.040 L=344.0' S=0.0075 '/' Capacity=54.59 cfs Outflow=16.73 cfs 1.395 af

Reach 2.2R: Wetland Flow Path Avg. Flow Depth=0.91' Max Vel=5.61 fps Inflow=24.09 cfs 3.990 af

n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=24.09 cfs 3.990 af

Reach 2R: Wetland Flow Path Avg. Flow Depth=0.83' Max Vel=5.02 fps Inflow=18.70 cfs 1.395 af

n=0.040 L=151.0' S=0.0446 '/' Capacity=133.09 cfs Outflow=18.63 cfs 1.395 af

Reach 23R: Wetland Flow Path Avg. Flow Depth=0.96' Max Vel=3.53 fps Inflow=16.73 cfs 1.395 af

n=0.040 L=131.0' S=0.0185'/' Capacity=85.86 cfs Outflow=16.62 cfs 1.395 af

Pond 1P: 15" RCP Peak Elev=53.65' Storage=1,011 cf Inflow=5.53 cfs 0.448 af

15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=4.26 cfs 0.448 af

Pond 2.1P: 24" RCP Peak Elev=51.11' Storage=18,912 cf Inflow=38.13 cfs 3.990 af

24.0" Round Culvert n=0.012 L=78.0' S=0.0135 '/' Outflow=24.09 cfs 3.990 af

Pond 2P: 12" CPP Peak Elev=60.93' Storage=11,719 cf Inflow=23.92 cfs 1.395 af

Outflow=18.70 cfs 1.395 af

Link 100L: POA #100 - SW Inflow=4.26 cfs 0.448 af

Primary=4.26 cfs 0.448 af

**Link 200L: POA #200 - South** Inflow=27.12 cfs 4.597 af

Primary=27.12 cfs 4.597 af

Link 300L: POA #300 - SE Inflow=16.14 cfs 1.589 af

Primary=16.14 cfs 1.589 af

Total Runoff Area = 30.826 ac Runoff Volume = 6.634 af Average Runoff Depth = 2.58" 93.16% Pervious = 28.718 ac 6.84% Impervious = 2.108 ac

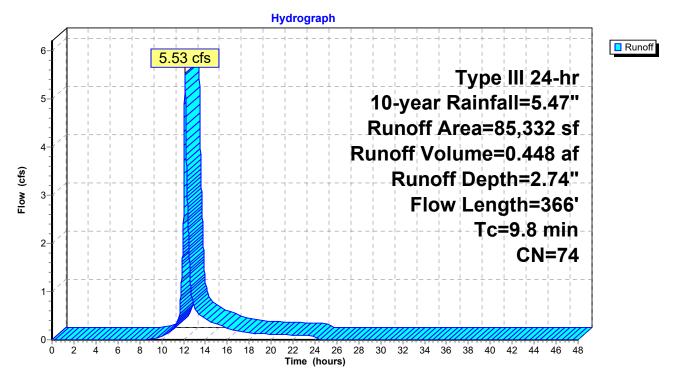
## **Summary for Subcatchment 1S: West Corner**

Runoff 5.53 cfs @ 12.14 hrs, Volume= 0.448 af, Depth= 2.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN [	Description				
		7,590	98 F	Paved roads w/curbs & sewers, HSG C				
		37,391	74 >	>75% Grass cover, Good, HSG C				
		40,320	70 \	Woods, Go	od, HSG C			
_		31	55 \	Woods, Good, HSG B				
		85,332	74 \	<b>Neighted A</b>	verage			
		77,742	(	91.11% Per	vious Area			
		7,590	8	3.89% Impe	ervious Area	a		
	_							
	Tc	Length	Slope	,	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	4.5	35	0.1071	0.13		Sheet Flow,		
						Woods: Light underbrush n= 0.400 P2= 3.61"		
	1.6	129	0.0388	1.38		Shallow Concentrated Flow,		
						Short Grass Pasture Kv= 7.0 fps		
	0.6	55	0.0909	1.51		Shallow Concentrated Flow,		
						Woodland Kv= 5.0 fps		
	3.1	147	0.0254	0.80		Shallow Concentrated Flow,		
_						Woodland Kv= 5.0 fps		
	9.8	366	Total					

## **Subcatchment 1S: West Corner**



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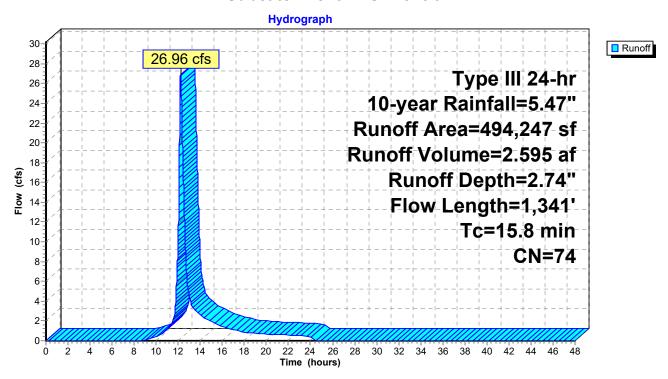
## **Summary for Subcatchment 2.1S: Central**

Runoff = 26.96 cfs @ 12.22 hrs, Volume= 2.595 af, Depth= 2.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN E	Description					
	4,537	98 F	Paved parking, HSG D					
	33,589			ing, HSG C				
	5,448		Roofs, HSG					
	49	98 F	Paved park	ing, HSG B				
	3,520				ood, HSG D			
	69,745			od, HSG D	·			
	10,593	65 E	Brush, Goo	d, HSG C				
	71,371	74 >	75% Gras	s cover, Go	ood, HSG C			
2	80,230	70 V	Voods, Go	od, HSG C				
	530	61 >	75% Gras	s cover, Go	ood, HSG B			
	14,635	55 V	Voods, Go	od, HSG B				
4	94,247	74 V	Veighted A	verage				
4	50,624			vious Area				
	43,623	8	3.83% Impe	ervious Area	a			
			•					
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
0.5	35	0.0200	1.18		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.61"			
4.7	255	0.0165	0.90		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
2.0	132	0.0501	1.12		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
0.4	67	0.0313	2.85		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
1.0	89	0.0465	1.51		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
4.3	289	0.0500	1.12		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
2.9	474	0.0106	2.72	13.61	Trap/Vee/Rect Channel Flow,			
					Bot.W=2.00' D=1.00' Z= 3.0 '/' Top.W=8.00'			
					n= 0.040 Winding stream, pools & shoals			
15.8	1,341	Total						

## **Subcatchment 2.1S: Central**



## **Summary for Subcatchment 2.2S: South of SQ Drive**

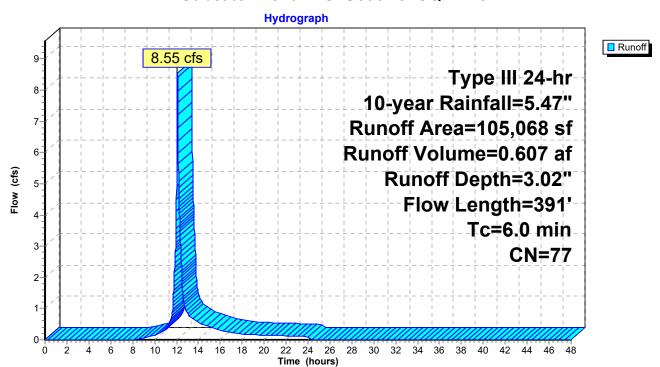
Runoff = 8.55 cfs @ 12.09 hrs, Volume= 0.607 af, Depth= 3.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Α	rea (sf)	CN [	Description		
		5,341	98 F	Paved park	ing, HSG D	
		5,978	98 F	Paved park	ing, HSG C	
		53,584	77 V	Voods, Go	od, HSG D	
		40,165 70 Woods, Good, HSG C				
	1	05,068	77 V	Veighted A	verage	
	93,749 89.23% Pervious Area			89.23% Per	vious Area	
	11,319 10.77% Impervious Area			0.77% Imp	pervious Are	ea
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.3	19	0.0200	1.05		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.61"
	1.4	118	0.0816	1.43		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.7	254	0.0502	5.93	29.63	Trap/Vee/Rect Channel Flow,
						Bot.W=2.00' D=1.00' Z= 3.0 '/' Top.W=8.00'
_						n= 0.040 Winding stream, pools & shoals
	0.4	204	T-4-1 1		::	T 0.0 min

2.4 391 Total, Increased to minimum Tc = 6.0 min

## Subcatchment 2.2S: South of SQ Drive



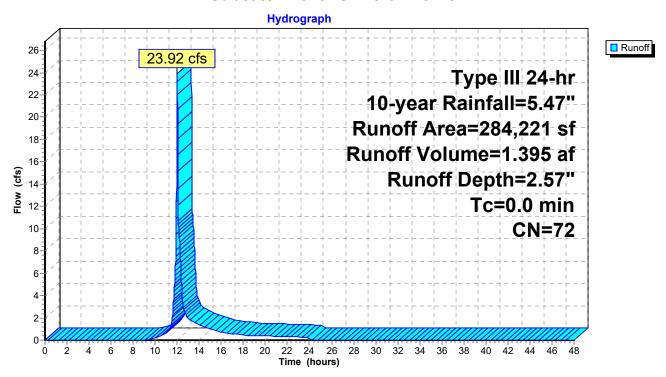
## **Summary for Subcatchment 2S: North Corner**

Runoff = 23.92 cfs @ 12.00 hrs, Volume= 1.395 af, Depth= 2.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

Area (sf)	CN	Description
27	98	Paved parking, HSG D
13,324	98	Paved parking, HSG C
5,932	98	Roofs, HSG C
254	80	>75% Grass cover, Good, HSG D
20,767	77	Woods, Good, HSG D
21,632	74	>75% Grass cover, Good, HSG C
199,815	70	Woods, Good, HSG C
22,470	55	Woods, Good, HSG B
284,221	72	Weighted Average
264,938		93.22% Pervious Area
19,283		6.78% Impervious Area

## **Subcatchment 2S: North Corner**



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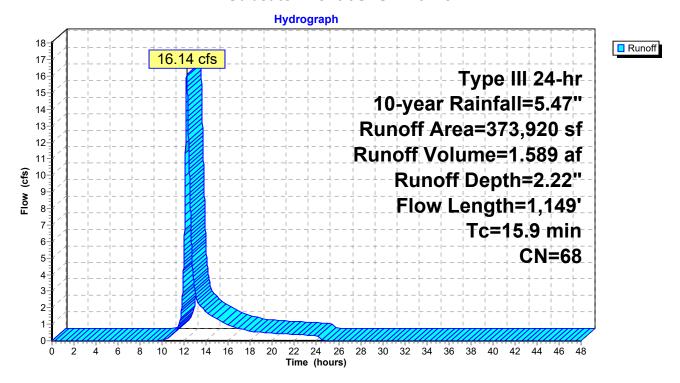
## **Summary for Subcatchment 3S: SE Corner**

Runoff = 16.14 cfs @ 12.23 hrs, Volume= 1.589 af, Depth= 2.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Area (sf)	CN [	Description		
	8,365	98 F	Paved park	ing, HSG C	
	1,632			ing, HSG B	
	6,383			s cover, Go	od, HSG C
	296,269	70 \	Noods, Go	od, HSG C	
	1,172			s cover, Go	od, HSG B
	60,099	55 \	Noods, Go	od, HSG B	
;	373,920		Veighted A		
;	363,923			vious Area	
	9,997	2	2.67% Impe	ervious Area	a e e e e e e e e e e e e e e e e e e e
_					
Tc		Slope		Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.5	90	0.1412	0.18		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.61"
4.7	331	0.0554	1.18		Shallow Concentrated Flow,
	004	0.0554	0.00	04.40	Woodland Kv= 5.0 fps
0.9	331	0.0554	6.22	31.12	Trap/Vee/Rect Channel Flow,
					Bot.W=2.00' D=1.00' Z= 3.0 '/' Top.W=8.00'
4.0	207	0.0400	0.00	05.00	n= 0.040 Winding stream, pools & shoals
1.8	397	0.0160	3.63	25.39	Trap/Vee/Rect Channel Flow,
					Bot.W=4.00' D=1.00' Z= 3.0 '/' Top.W=10.00'
	4 4 4 5	<del></del>			n= 0.040 Winding stream, pools & shoals
15.9	1,149	Total			

## **Subcatchment 3S: SE Corner**



## **Summary for Reach 2.1R: Wetland Flow Path**

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 18.63 cfs @ 12.05 hrs, Volume= 1.395 af

Outflow = 16.73 cfs @ 12.09 hrs, Volume= 1.395 af, Atten= 10%, Lag= 2.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.53 fps, Min. Travel Time= 2.3 min Avg. Velocity = 0.72 fps, Avg. Travel Time= 7.9 min

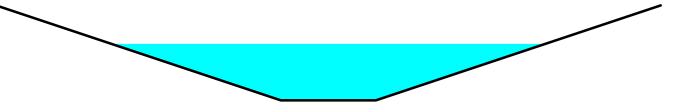
Peak Storage= 2,278 cf @ 12.09 hrs Average Depth at Peak Storage= 1.19' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 54.59 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

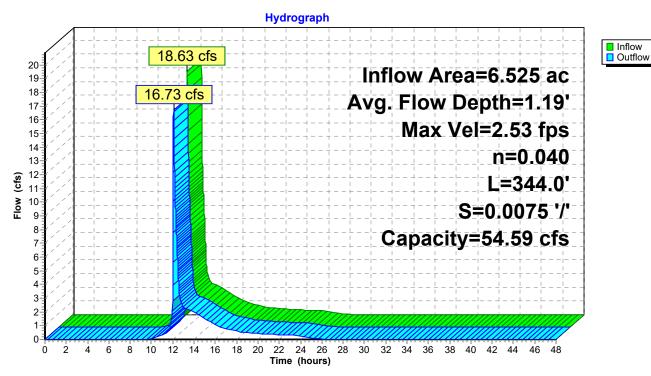
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 344.0' Slope= 0.0075 '/'

Inlet Invert= 52.58', Outlet Invert= 50.00'



## Reach 2.1R: Wetland Flow Path



## **Summary for Reach 2.2R: Wetland Flow Path**

Inflow Area = 17.871 ac, 8.08% Impervious, Inflow Depth = 2.68" for 10-year event

Inflow = 24.09 cfs @ 12.43 hrs, Volume= 3.990 af

Outflow = 24.09 cfs @ 12.44 hrs, Volume= 3.990 af, Atten= 0%, Lag= 0.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity = 5.61 fps, Min. Travel Time = 0.8 min Avg. Velocity = 1.93 fps, Avg. Travel Time = 2.3 min

Peak Storage= 1,129 cf @ 12.44 hrs Average Depth at Peak Storage= 0.91'

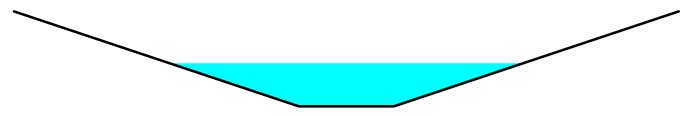
Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 141.18 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

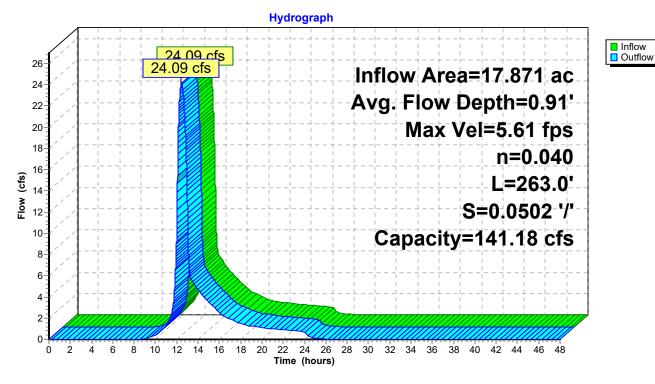
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 263.0' Slope= 0.0502 '/'

Inlet Invert= 46.52', Outlet Invert= 33.33'



Reach 2.2R: Wetland Flow Path



## Summary for Reach 2R: Wetland Flow Path

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 18.70 cfs @ 12.05 hrs, Volume= 1.395 af

Outflow = 18.63 cfs @ 12.05 hrs, Volume= 1.395 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 5.02 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.45 fps, Avg. Travel Time= 1.7 min

Peak Storage= 560 cf @ 12.05 hrs Average Depth at Peak Storage= 0.83'

Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 133.09 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

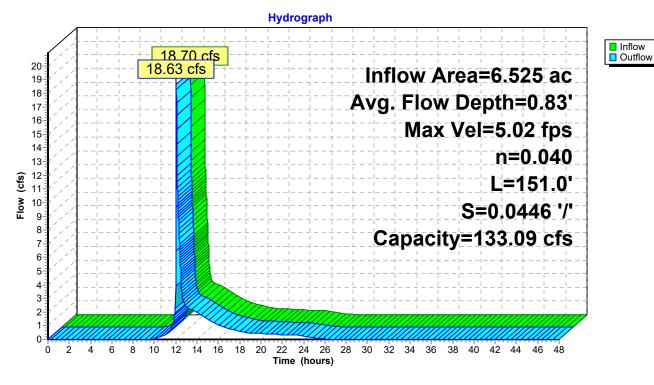
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 151.0' Slope= 0.0446 '/'

Inlet Invert= 59.31', Outlet Invert= 52.58'



## Reach 2R: Wetland Flow Path



## **Summary for Reach 23R: Wetland Flow Path**

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 16.73 cfs @ 12.09 hrs, Volume= 1.395 af

Outflow = 16.62 cfs @ 12.10 hrs, Volume= 1.395 af, Atten= 1%, Lag= 0.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.53 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.03 fps, Avg. Travel Time= 2.1 min

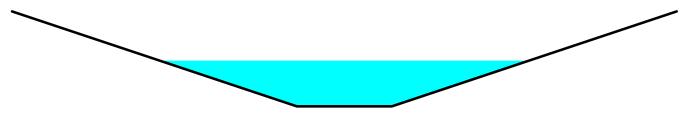
Peak Storage= 617 cf @ 12.10 hrs Average Depth at Peak Storage= 0.96' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 85.86 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

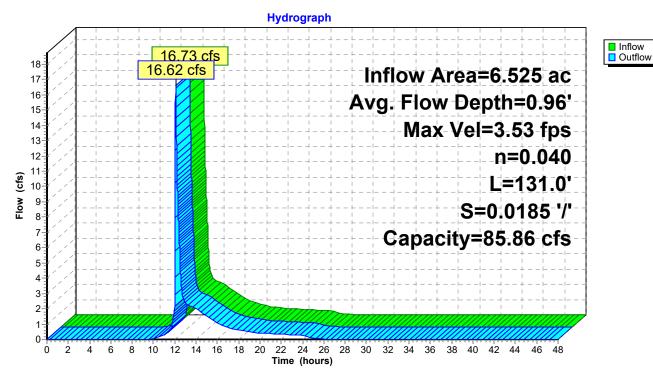
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 131.0' Slope= 0.0185 '/'

Inlet Invert= 50.00', Outlet Invert= 47.57'



## Reach 23R: Wetland Flow Path



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## **Summary for Pond 1P: 15" RCP**

Inflow Area = 1.959 ac, 8.89% Impervious, Inflow Depth = 2.74" for 10-year event

5.53 cfs @ 12.14 hrs, Volume= Inflow 0.448 af

4.26 cfs @ 12.23 hrs, Volume= Outflow = 0.448 af, Atten= 23%, Lag= 5.5 min

4.26 cfs @ 12.23 hrs, Volume= Primary 0.448 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 53.65' @ 12.23 hrs Surf.Area= 2,904 sf Storage= 1,011 cf

Plug-Flow detention time= 1.4 min calculated for 0.448 af (100% of inflow)

Center-of-Mass det. time= 1.3 min (837.9 - 836.6)

Volume	Invert	Avail.Storage	Storage Description
#1	52.26'	9,237 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

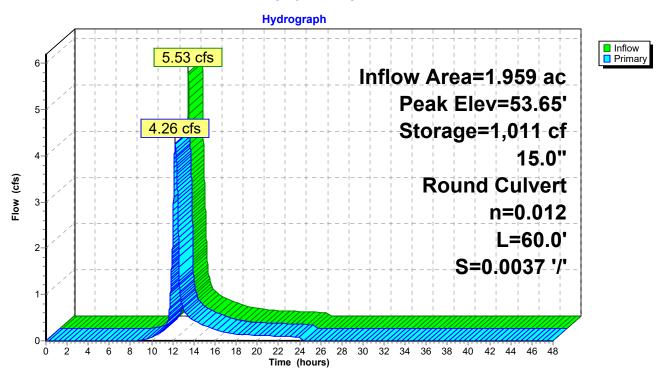
Elevation	Surt.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
52.26	10	0	0
53.00	85	35	35
54.00	4,401	2,243	2,278
55.00	9,516	6,959	9,237

Device	Routing	Invert	Outlet Devices
#1	Primary	52.26'	15.0" Round Culvert

L= 60.0' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 52.26' / 52.04' S= 0.0037 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=4.26 cfs @ 12.23 hrs HW=53.65' TW=0.00' (Dynamic Tailwater) 1=Culvert (Barrel Controls 4.26 cfs @ 3.89 fps)

Pond 1P: 15" RCP



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## Summary for Pond 2.1P: 24" RCP

Inflow Area = 17.871 ac, 8.08% Impervious, Inflow Depth = 2.68" for 10-year event

Inflow = 38.13 cfs @ 12.19 hrs, Volume= 3.990 af

Outflow = 24.09 cfs @ 12.43 hrs, Volume= 3.990 af, Atten= 37%, Lag= 14.6 min

Primary = 24.09 cfs @ 12.43 hrs, Volume= 3.990 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 51.11' @ 12.43 hrs Surf.Area= 16,584 sf Storage= 18,912 cf

Plug-Flow detention time= 4.8 min calculated for 3.990 af (100% of inflow) Center-of-Mass det. time= 4.7 min (861.2 - 856.5)

Volume	Invert	Avail.Storage	Storage Description
#1	47.57'	80,071 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

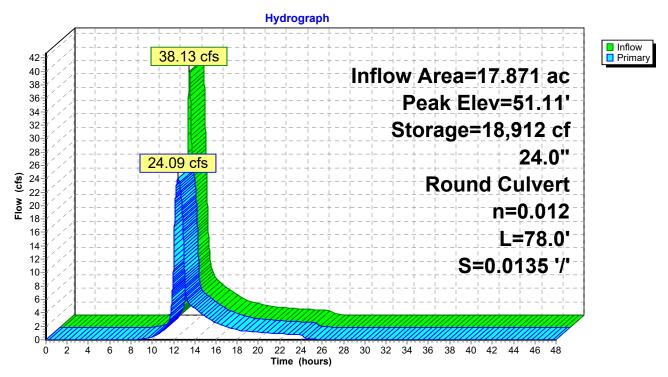
Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
47.57	100	0	0
48.00	164	57	57
49.00	2,506	1,335	1,392
50.00	7,196	4,851	6,243
51.00	14,807	11,002	17,244
52.00	31,534	23,171	40,415
53.00	47,779	39,657	80,071

Device	Routing	Invert	Outlet Devices
#1	Primary	47.57'	24.0" Round Culvert

L= 78.0' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 47.57' / 46.52' S= 0.0135 '/' Cc= 0.900 n= 0.012, Flow Area= 3.14 sf

Primary OutFlow Max=24.09 cfs @ 12.43 hrs HW=51.11' TW=47.43' (Dynamic Tailwater) 1=Culvert (Inlet Controls 24.09 cfs @ 7.67 fps)

Pond 2.1P: 24" RCP



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### Summary for Pond 2P: 12" CPP

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 23.92 cfs @ 12.00 hrs, Volume= 1.395 af

Outflow = 18.70 cfs @ 12.05 hrs, Volume= 1.395 af, Atten= 22%, Lag= 2.6 min

Primary = 18.70 cfs @ 12.05 hrs, Volume= 1.395 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 60.93' @ 12.05 hrs Surf.Area= 15,490 sf Storage= 11,719 cf

Plug-Flow detention time= 44.2 min calculated for 1.395 af (100% of inflow)

Center-of-Mass det. time= 44.1 min ( 876.6 - 832.4 )

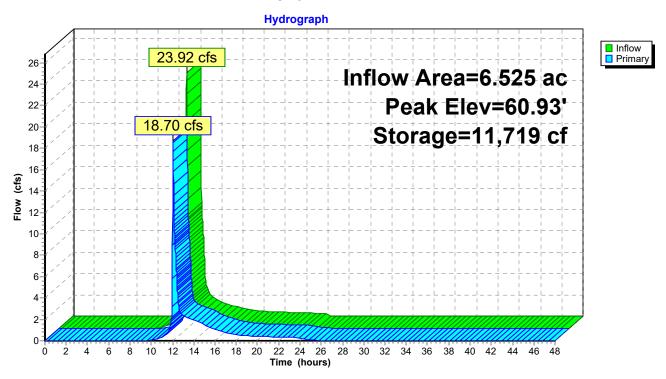
Volume	Inv	ert Avail.Sto	orage	Storage	e Description	
#1	59.	65' 35,7	'64 cf	Custon	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevation	on	Surf.Area	Inc	.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubi	c-feet)	(cubic-feet)	
59.6	65	100		0	0	
60.0	60.00 6,996			1,242	1,242	
61.0	61.00 16,111		•	11,554	12,795	
62.0	00	29,827	2	22,969	35,764	
Device	Routing	Invert	Outl	et Device	es	
#1	Primary	59.65'	12.0	" Round	d Culvert	
			L= 9	.0' CPP	, projecting, no h	neadwall, Ke= 0.900
			Inlet	/ Outlet	Invert= 59.65' / 5	9.31' S= 0.0378 '/' Cc= 0.900
			n= 0	.012, Flo	ow Area= 0.79 sf	
#2	Primary	60.75'		_		oad-Crested Rectangular Weir
						0.80 1.00 1.20 1.40 1.60 1.80 2.00
					.50 4.00 4.50 5	
						69 2.68 2.67 2.67 2.65 2.66 2.66
			2.68	2.72 2.	.73 2.76 2.79 2	.88 3.07 3.32

Primary OutFlow Max=18.66 cfs @ 12.05 hrs HW=60.93' TW=60.13' (Dynamic Tailwater)

1=Culvert (Inlet Controls 2.64 cfs @ 3.36 fps)

-2=Broad-Crested Rectangular Weir (Weir Controls 16.02 cfs @ 1.01 fps)

# Pond 2P: 12" CPP



# Summary for Link 100L: POA #100 - SW

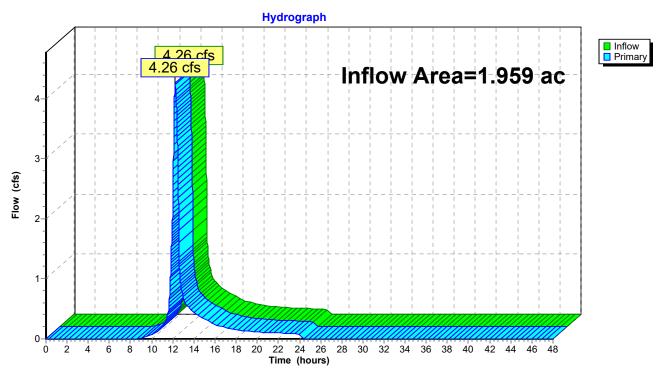
Inflow Area = 1.959 ac, 8.89% Impervious, Inflow Depth = 2.74" for 10-year event

Inflow = 4.26 cfs @ 12.23 hrs, Volume= 0.448 af

Primary = 4.26 cfs @ 12.23 hrs, Volume= 0.448 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Link 100L: POA #100 - SW



### Summary for Link 200L: POA #200 - South

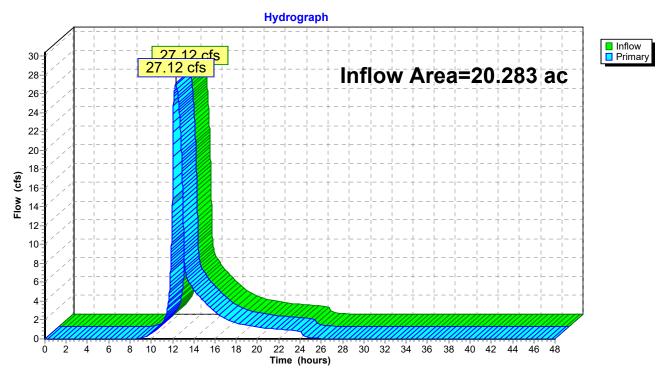
Inflow Area = 20.283 ac, 8.40% Impervious, Inflow Depth = 2.72" for 10-year event

Inflow = 27.12 cfs @ 12.34 hrs, Volume= 4.597 af

Primary = 27.12 cfs @ 12.34 hrs, Volume= 4.597 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Link 200L: POA #200 - South



# Summary for Link 300L: POA #300 - SE

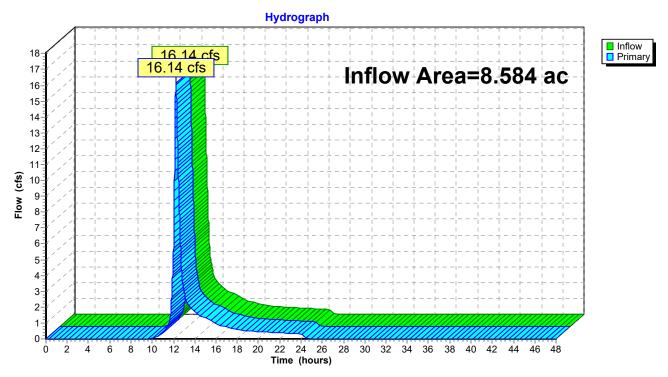
Inflow Area = 8.584 ac, 2.67% Impervious, Inflow Depth = 2.22" for 10-year event

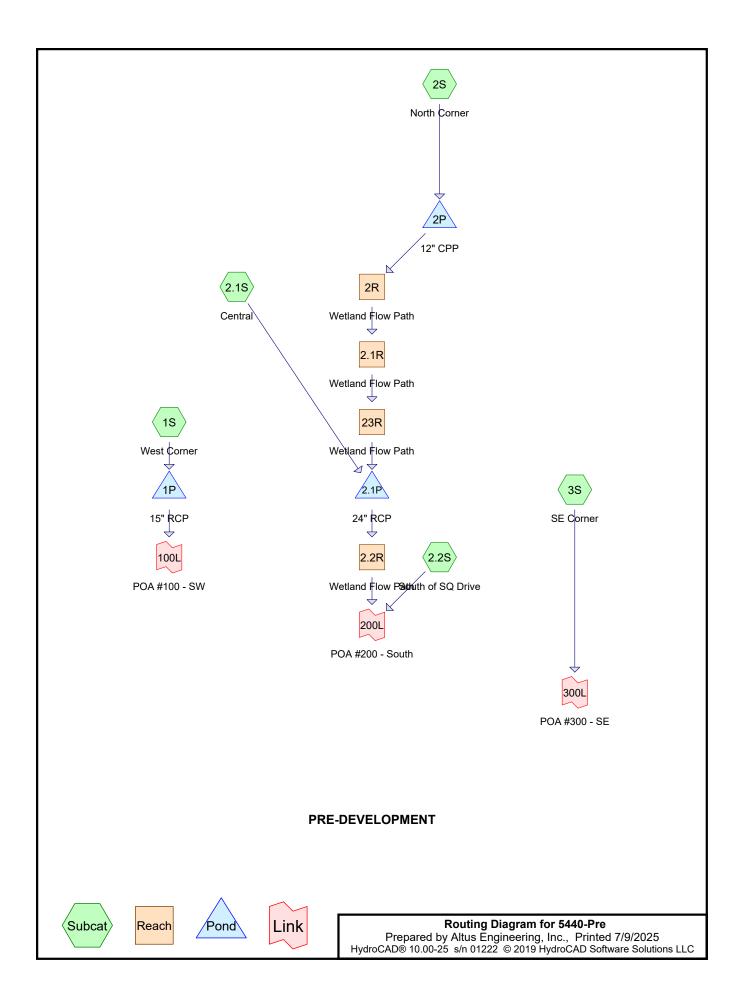
Inflow = 16.14 cfs @ 12.23 hrs, Volume= 1.589 af

Primary = 16.14 cfs @ 12.23 hrs, Volume= 1.589 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

#### Link 300L: POA #300 - SE





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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: West Corner Runoff Area=85,332 sf 8.89% Impervious Runoff Depth=3.98"

Flow Length=366' Tc=9.8 min CN=74 Runoff=8.04 cfs 0.650 af

Subcatchment 2.1S: Central Runoff Area=494,247 sf 8.83% Impervious Runoff Depth=3.98"

Flow Length=1,341' Tc=15.8 min CN=74 Runoff=39.25 cfs 3.764 af

**Subcatchment 2.2S: South of SQ Drive** Runoff Area=105,068 sf 10.77% Impervious Runoff Depth=4.30"

Flow Length=391' Tc=6.0 min CN=77 Runoff=12.13 cfs 0.865 af

Subcatchment 2S: North Corner Runoff Area = 284,221 sf 6.78% Impervious Runoff Depth = 3.77"

Tc=0.0 min CN=72 Runoff=35.33 cfs 2.050 af

Subcatchment 3S: SE Corner Runoff Area=373,920 sf 2.67% Impervious Runoff Depth=3.35"

Flow Length=1,149' Tc=15.9 min CN=68 Runoff=24.80 cfs 2.399 af

Reach 2.1R: Wetland Flow Path Avg. Flow Depth=1.53' Max Vel=2.91 fps Inflow=31.17 cfs 2.050 af

n=0.040 L=344.0' S=0.0075 '/' Capacity=54.59 cfs Outflow=29.25 cfs 2.050 af

Reach 2.2R: Wetland Flow Path Avg. Flow Depth=0.98' Max Vel=5.85 fps Inflow=28.17 cfs 5.814 af

n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=28.17 cfs 5.814 af

Reach 2R: Wetland Flow Path Avg. Flow Depth=1.05' Max Vel=5.74 fps Inflow=31.29 cfs 2.050 af

n=0.040 L=151.0' S=0.0446 '/' Capacity=133.09 cfs Outflow=31.17 cfs 2.050 af

Reach 23R: Wetland Flow Path Avg. Flow Depth=1.25' Max Vel=4.08 fps Inflow=29.25 cfs 2.050 af

n=0.040 L=131.0' S=0.0185'/' Capacity=85.86 cfs Outflow=29.14 cfs 2.050 af

Pond 1P: 15" RCP Peak Elev=54.02' Storage=2,363 cf Inflow=8.04 cfs 0.650 af

15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=5.12 cfs 0.650 af

Pond 2.1P: 24" RCP Peak Elev=52.04' Storage=41,604 cf Inflow=55.24 cfs 5.814 af

24.0" Round Culvert n=0.012 L=78.0' S=0.0135 '/' Outflow=28.17 cfs 5.814 af

Pond 2P: 12" CPP Peak Elev=61.01' Storage=13,034 cf Inflow=35.33 cfs 2.050 af

Outflow=31.29 cfs 2.050 af

Link 100L: POA #100 - SW Inflow=5.12 cfs 0.650 af

Primary=5.12 cfs 0.650 af

Link 200L: POA #200 - South Inflow=34.48 cfs 6.679 af

Primary=34.48 cfs 6.679 af

Link 300L: POA #300 - SE Inflow=24.80 cfs 2.399 af

Primary=24.80 cfs 2.399 af

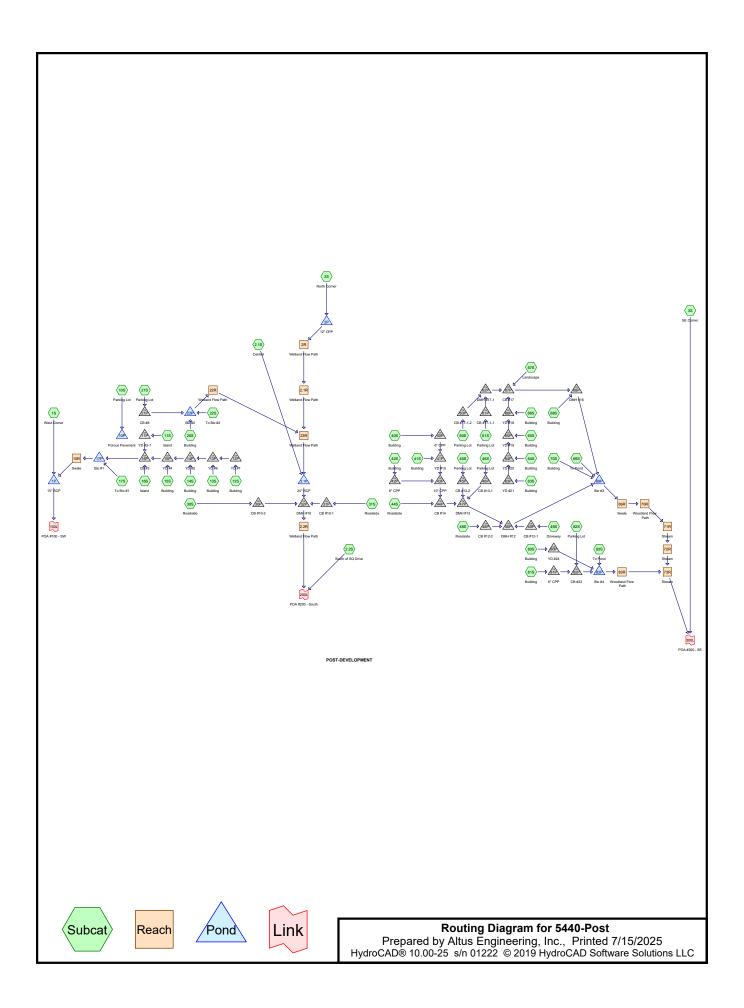
Total Runoff Area = 30.826 ac Runoff Volume = 9.728 af Average Runoff Depth = 3.79" 93.16% Pervious = 28.718 ac 6.84% Impervious = 2.108 ac

# Section 4

# **Drainage Calculations**

Post-Development
2-Year, 24-Hour Summary
10-Year, 24-Hour Complete
25-Year, 24-Hour Summary
100-Year, 24-Hour Pond Reports





Tc=6.0 min CN=74 Runoff=0.00 cfs 0.000 af

# 5440-Post

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=65,016 sf 9.83% Impervious Runoff Depth=0.03" Subcatchment 1S: West Corner Flow Length=366' Tc=9.8 min CN=75 Runoff=0.01 cfs 0.004 af Runoff Area=445,535 sf 8.04% Impervious Runoff Depth=0.02" Subcatchment 2.1S: Central Flow Length=1,341' Tc=15.8 min CN=73 Runoff=0.02 cfs 0.015 af Runoff Area=102,088 sf 10.13% Impervious Runoff Depth=0.05" Subcatchment 2.2S: South of SQ Drive Flow Length=391' Tc=6.0 min CN=77 Runoff=0.03 cfs 0.009 af Runoff Area=284,221 sf 6.78% Impervious Runoff Depth=0.01" Subcatchment 2S: North Corner Tc=0.0 min CN=72 Runoff=0.01 cfs 0.007 af Runoff Area=308,423 sf 2.18% Impervious Runoff Depth=0.00" Subcatchment 3S: SE Corner Flow Length=1,149' Tc=15.9 min CN=68 Runoff=0.00 cfs 0.000 af Runoff Area=10,178 sf 99.02% Impervious Runoff Depth>0.79" Subcatchment 10S: Parking Lot Tc=790.0 min CN=98 Runoff=0.01 cfs 0.015 af Runoff Area=588 sf 65.82% Impervious Runoff Depth=0.32" Subcatchment 11S: Island Tc=6.0 min CN=90 Runoff=0.00 cfs 0.000 af Runoff Area=1,878 sf 65.12% Impervious Runoff Depth=0.32" Subcatchment 12S: Building Tc=6.0 min CN=90 Runoff=0.02 cfs 0.001 af Runoff Area=1,349 sf 73.83% Impervious Runoff Depth=0.40" Subcatchment 13S: Building Tc=6.0 min CN=92 Runoff=0.01 cfs 0.001 af Runoff Area=1,022 sf 77.79% Impervious Runoff Depth=0.45" Subcatchment 14S: Building Tc=6.0 min CN=93 Runoff=0.01 cfs 0.001 af Runoff Area=1,377 sf 43.21% Impervious Runoff Depth=0.15" Subcatchment 15S: Building Tc=6.0 min CN=84 Runoff=0.00 cfs 0.000 af Runoff Area=928 sf 26.51% Impervious Runoff Depth=0.08" Subcatchment 16S: Island Tc=6.0 min CN=80 Runoff=0.00 cfs 0.000 af Subcatchment 17S: To Bio #1 Runoff Area=2,893 sf 0.28% Impervious Runoff Depth=0.02" Tc=6.0 min CN=74 Runoff=0.00 cfs 0.000 af Runoff Area=9,167 sf 100.00% Impervious Runoff Depth=0.79" Subcatchment 20S: Building Tc=6.0 min CN=98 Runoff=0.19 cfs 0.014 af Runoff Area=2,620 sf 100.00% Impervious Runoff Depth=0.79" **Subcatchment 21S: Parking Lot** Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af Subcatchment 22S: To Bio #2 Runoff Area=3,961 sf 0.00% Impervious Runoff Depth=0.02"

Subcatchment 30S: Roadside	Runoff Area=8,230 sf 53.10% Impervious Runoff Depth=0.22" Flow Length=204' Tc=6.0 min CN=87 Runoff=0.04 cfs 0.004 af
Subcatchment31S: Roadside	Runoff Area=7,135 sf 71.11% Impervious Runoff Depth=0.36" Flow Length=143' Tc=6.0 min CN=91 Runoff=0.07 cfs 0.005 af
Subcatchment40S: Building	Runoff Area=3,066 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment41S: Building	Runoff Area=2,120 sf 90.94% Impervious Runoff Depth=0.63" Tc=6.0 min CN=96 Runoff=0.04 cfs 0.003 af
Subcatchment42S: Building	Runoff Area=2,162 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.04 cfs 0.003 af
Subcatchment44S: Roadside	Runoff Area=4,663 sf 40.92% Impervious Runoff Depth=0.15" Tc=6.0 min CN=84 Runoff=0.01 cfs 0.001 af
Subcatchment45S: Parking Lot	Runoff Area=3,851 sf 71.88% Impervious Runoff Depth=0.36" Tc=6.0 min CN=91 Runoff=0.04 cfs 0.003 af
Subcatchment46S: Parking Lot	Runoff Area=4,489 sf 73.25% Impervious Runoff Depth=0.40" Tc=6.0 min CN=92 Runoff=0.05 cfs 0.003 af
Subcatchment48S: Roadside	Runoff Area=3,415 sf 55.67% Impervious Runoff Depth=0.25" Tc=6.0 min CN=88 Runoff=0.02 cfs 0.002 af
Subcatchment49S: Driveway	Runoff Area=3,652 sf 83.90% Impervious Runoff Depth=0.45" Tc=6.0 min CN=93 Runoff=0.04 cfs 0.003 af
Subcatchment 60S: Parking Lot	Runoff Area=9,169 sf 78.19% Impervious Runoff Depth=0.45" Flow Length=116' Tc=6.0 min CN=93 Runoff=0.11 cfs 0.008 af
Subcatchment 61S: Parking Lot	Runoff Area=7,068 sf 91.98% Impervious Runoff Depth=0.63" Flow Length=111' Tc=6.0 min CN=96 Runoff=0.12 cfs 0.009 af
Subcatchment 63S: Building	Runoff Area=1,459 sf 65.52% Impervious Runoff Depth=0.32" Tc=6.0 min CN=90 Runoff=0.01 cfs 0.001 af
Subcatchment 64S: Building	Runoff Area=1,506 sf 81.27% Impervious Runoff Depth=0.50" Tc=6.0 min CN=94 Runoff=0.02 cfs 0.001 af
Subcatchment 65S: Building	Runoff Area=982 sf 80.86% Impervious Runoff Depth=0.45" Tc=6.0 min CN=93 Runoff=0.01 cfs 0.001 af
Subcatchment 66S: Building	Runoff Area=1,478 sf 44.79% Impervious Runoff Depth=0.11" Tc=6.0 min CN=82 Runoff=0.00 cfs 0.000 af
Subcatchment 67S: Landscape	Runoff Area=1,511 sf 10.32% Impervious Runoff Depth=0.00" Tc=6.0 min CN=64 Runoff=0.00 cfs 0.000 af
Subcatchment 68S: Building	Runoff Area=1,370 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.002 af

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 Subcatchment 69S: To Pond
 Runoff Area=12,794 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=69 Runoff=0.00 cfs 0.000 af

 Subcatchment 70S: Building
 Runoff Area=6,905 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.010 af

 Subcatchment 80S: Building
 Runoff Area=1,982 sf 84.56% Impervious Runoff Depth=0.50" Tc=6.0 min CN=94 Runoff=0.03 cfs 0.002 af

 Subcatchment 81S: Building
 Runoff Area=1,200 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.02 cfs 0.002 af

Subcatchment 82S: Parking Lot

Runoff Area=8,819 sf 89.53% Impervious Runoff Depth=0.56"

Flow Length=214' Tc=6.0 min CN=95 Runoff=0.13 cfs 0.010 af

Subcatchment83S: To Pond

Runoff Area=2,507 sf 0.00% Impervious Runoff Depth=0.02"

Tc=6.0 min CN=74 Runoff=0.00 cfs 0.000 af

**Reach 2.1R: Wetland Flow Path**Avg. Flow Depth=0.02' Max Vel=0.23 fps Inflow=0.01 cfs 0.007 af n=0.040 L=344.0' S=0.0075 '/' Capacity=54.59 cfs Outflow=0.01 cfs 0.007 af

**Reach 2.2R: Wetland Flow Path**Avg. Flow Depth=0.05' Max Vel=1.04 fps Inflow=0.11 cfs 0.047 af n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=0.10 cfs 0.047 af

**Reach 2R: Wetland Flow Path**Avg. Flow Depth=0.01' Max Vel=0.57 fps Inflow=0.01 cfs 0.007 af n=0.040 L=151.0' S=0.0446 '/' Capacity=133.09 cfs Outflow=0.01 cfs 0.007 af

Reach 10R: Swale

Avg. Flow Depth=0.01' Max Vel=0.14 fps Inflow=0.00 cfs 0.004 af n=0.035 L=44.0' S=0.0050'/ Capacity=16.22 cfs Outflow=0.00 cfs 0.004 af

**Reach 22R: Wetland Flow Path**Avg. Flow Depth=0.00' Max Vel=0.42 fps Inflow=0.01 cfs 0.018 af n=0.040 L=211.0' S=0.0245 '/' Capacity=392.58 cfs Outflow=0.01 cfs 0.018 af

**Reach 23R: Wetland Flow Path**Avg. Flow Depth=0.02' Max Vel=0.43 fps Inflow=0.02 cfs 0.024 af n=0.040 L=131.0' S=0.0185 '/' Capacity=85.86 cfs Outflow=0.02 cfs 0.024 af

**Reach 69R: Swale**Avg. Flow Depth=0.03' Max Vel=0.25 fps Inflow=0.03 cfs 0.050 af n=0.069 L=17.0' S=0.0147 '/' Capacity=14.11 cfs Outflow=0.03 cfs 0.050 af

**Reach 70R: Woodland Flow Path**Avg. Flow Depth=0.02' Max Vel=0.12 fps Inflow=0.03 cfs 0.050 af n=0.400 L=57.0' S=0.1404 '/' Capacity=21.20 cfs Outflow=0.03 cfs 0.050 af

Reach 71R: Stream

Avg. Flow Depth=0.02' Max Vel=0.67 fps Inflow=0.03 cfs 0.050 af n=0.040 L=80.0' S=0.0554 '/' Capacity=31.12 cfs Outflow=0.03 cfs 0.050 af

**Reach 72R: Stream**Avg. Flow Depth=0.02' Max Vel=0.35 fps Inflow=0.03 cfs 0.050 af n=0.040 L=88.0' S=0.0160 '/' Capacity=25.40 cfs Outflow=0.03 cfs 0.050 af

Reach 73R: Stream Avg. Flow Depth=0.03' Max Vel=0.41 fps Inflow=0.04 cfs 0.064 af

n=0.040 L=309.0' S=0.0160'/' Capacity=25.38 cfs Outflow=0.04 cfs 0.063 af

Reach 83R: Woodland Flow P	ath Avg. Flow Depth=0.02' Max Vel=0.08 fps Inflow=0.01 cfs 0.013 af n=0.400 L=122.0' S=0.0950 '/' Capacity=17.44 cfs Outflow=0.01 cfs 0.013 af
Pond 1P: 15" RCP	Peak Elev=52.32' Storage=1 cf Inflow=0.01 cfs 0.008 af 15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=0.01 cfs 0.008 af
Pond 2.1P: 24" RCP	Peak Elev=47.65' Storage=9 cf Inflow=0.04 cfs 0.039 af 24.0" Round Culvert n=0.012 L=17.0' S=0.0135 '/' Outflow=0.04 cfs 0.039 af
Pond 2P: 12" CPP	Peak Elev=59.70' Storage=30 cf Inflow=0.01 cfs 0.007 af Outflow=0.01 cfs 0.007 af
Pond 10P: Porous Pavement	Peak Elev=0.00' Storage=5 cf Inflow=0.01 cfs 0.015 af Outflow=0.01 cfs 0.015 af
Pond 11P: YD #3-1	Peak Elev=57.21' Inflow=0.00 cfs 0.000 af 6.0" Round Culvert n=0.012 L=36.0' S=0.0050 '/' Outflow=0.00 cfs 0.000 af
Pond 12P: YD #7	Peak Elev=57.84' Inflow=0.02 cfs 0.001 af 8.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=0.02 cfs 0.001 af
Pond 13P: YD #6	Peak Elev=57.43' Inflow=0.03 cfs 0.002 af 10.0" Round Culvert n=0.012 L=29.0' S=0.0052 '/' Outflow=0.03 cfs 0.002 af
Pond 14P: YD #5	Peak Elev=57.20' Inflow=0.04 cfs 0.003 af 10.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=0.04 cfs 0.003 af
Pond 15P: YD #4	Peak Elev=56.93' Inflow=0.05 cfs 0.003 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.05 cfs 0.003 af
Pond 16P: CB #3	Peak Elev=56.61' Inflow=0.05 cfs 0.004 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0049 '/' Outflow=0.05 cfs 0.004 af
Pond 17P: Bio #1	Peak Elev=56.42' Storage=126 cf Inflow=0.05 cfs 0.004 af Outflow=0.00 cfs 0.004 af
Pond 21P: CB #8	Peak Elev=58.16' Inflow=0.05 cfs 0.004 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0050 '/' Outflow=0.05 cfs 0.004 af
Pond 22P: Bio #2	Peak Elev=58.16' Storage=546 cf Inflow=0.24 cfs 0.018 af Outflow=0.01 cfs 0.018 af
Pond 30P: CB #10-2	Peak Elev=52.75' Inflow=0.04 cfs 0.004 af 12.0" Round Culvert n=0.012 L=78.0' S=0.0397 '/' Outflow=0.04 cfs 0.004 af
Pond 31P: CB #10-1	Peak Elev=49.73' Inflow=0.07 cfs 0.005 af 12.0" Round Culvert n=0.012 L=2.0' S=0.0250 '/' Outflow=0.07 cfs 0.005 af
Pond 32P: DMH #10	Peak Elev=47.42' Inflow=0.11 cfs 0.047 af 24.0" Round Culvert n=0.012 L=57.0' S=0.0135 '/' Outflow=0.11 cfs 0.047 af
Pond 40P: 6" CPP	Peak Elev=53.73' Inflow=0.06 cfs 0.005 af 6.0" Round Culvert n=0.012 L=174.0' S=0.0150 '/' Outflow=0.06 cfs 0.005 af

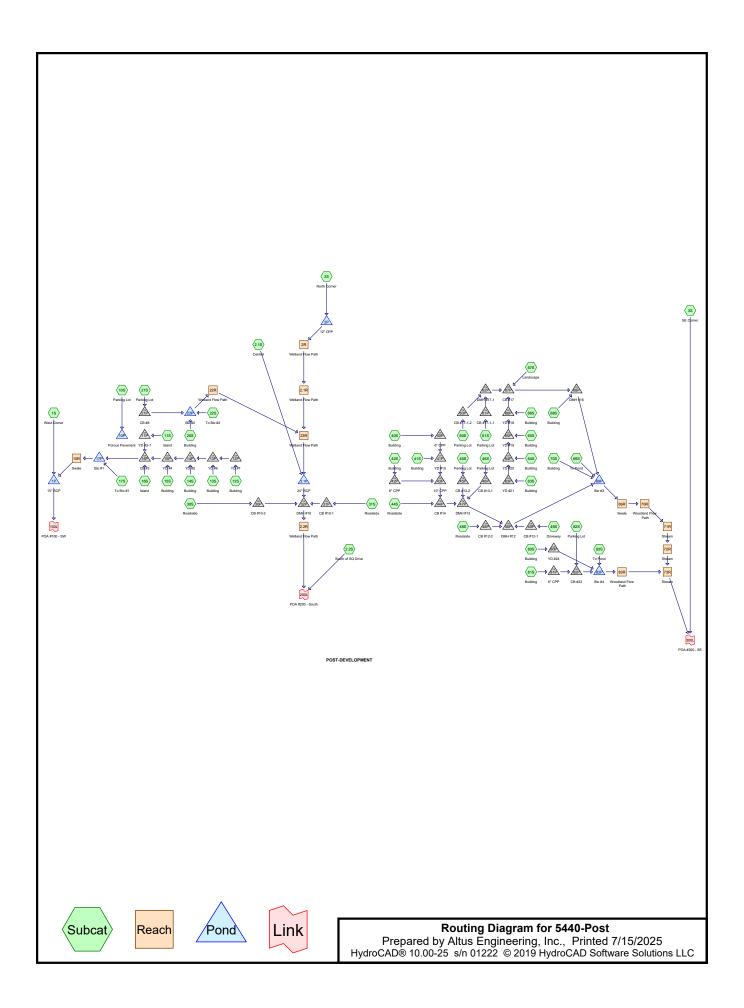
Pond 41P: YD #15	Peak Elev=50.97' Inflow=0.10 cfs 0.007 af 8.0" Round Culvert n=0.012 L=47.0' S=0.0149 '/' Outflow=0.10 cfs 0.007 af
Pond 42P: 6" CPP	Peak Elev=52.93' Inflow=0.04 cfs 0.003 af 6.0" Round Culvert n=0.012 L=150.0' S=0.0175 '/' Outflow=0.04 cfs 0.003 af
Pond 43P: 10" CPP	Peak Elev=50.31' Inflow=0.14 cfs 0.010 af 8.0" Round Culvert n=0.012 L=33.0' S=0.0148 '/' Outflow=0.14 cfs 0.010 af
Pond 44P: CB #14	Peak Elev=49.49' Inflow=0.15 cfs 0.012 af 12.0" Round Culvert n=0.012 L=31.0' S=0.0048 '/' Outflow=0.15 cfs 0.012 af
Pond 45P: CB #13-2	Peak Elev=49.74' Inflow=0.04 cfs 0.003 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0245 '/' Outflow=0.04 cfs 0.003 af
Pond 46P: CB #13-1	Peak Elev=49.60' Inflow=0.05 cfs 0.003 af 12.0" Round Culvert n=0.012 L=12.0' S=0.0325 '/' Outflow=0.05 cfs 0.003 af
Pond 47P: DMH #13	Peak Elev=49.28' Inflow=0.24 cfs 0.018 af 12.0" Round Culvert n=0.012 L=67.0' S=0.0051 '/' Outflow=0.24 cfs 0.018 af
Pond 48P: CB #12-2	Peak Elev=48.79' Inflow=0.02 cfs 0.002 af 12.0" Round Culvert n=0.012 L=6.0' S=0.0050 '/' Outflow=0.02 cfs 0.002 af
Pond 49P: CB #12-1	Peak Elev=49.02' Inflow=0.04 cfs 0.003 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.04 cfs 0.003 af
Pond 50P: DMH #12	Peak Elev=48.79' Inflow=0.30 cfs 0.023 af 15.0" Round Culvert n=0.012 L=106.0' S=0.0040 '/' Outflow=0.30 cfs 0.023 af
Pond 60P: CB #17-1-2	Peak Elev=50.60' Inflow=0.11 cfs 0.008 af 12.0" Round Culvert n=0.012 L=21.0' S=0.0052 '/' Outflow=0.11 cfs 0.008 af
Pond 61P: CB #17-1-1	Peak Elev=50.57' Inflow=0.12 cfs 0.009 af 12.0" Round Culvert n=0.012 L=3.0' S=0.0367 '/' Outflow=0.12 cfs 0.009 af
Pond 62P: DMH #17-1	Peak Elev=50.46' Inflow=0.23 cfs 0.016 af 12.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=0.23 cfs 0.016 af
Pond 63P: YD #21	Peak Elev=51.76' Inflow=0.01 cfs 0.001 af 12.0" Round Culvert n=0.012 L=49.0' S=0.0049 '/' Outflow=0.01 cfs 0.001 af
Pond 64P: YD #20	Peak Elev=51.39' Inflow=0.03 cfs 0.002 af 10.0" Round Culvert n=0.012 L=35.0' S=0.0049 '/' Outflow=0.03 cfs 0.002 af
Pond 65P: YD #19	Peak Elev=51.13' Inflow=0.04 cfs 0.003 af 10.0" Round Culvert n=0.012 L=42.0' S=0.0050 '/' Outflow=0.04 cfs 0.003 af
Pond 66P: YD #18	Peak Elev=50.72' Inflow=0.05 cfs 0.004 af 12.0" Round Culvert n=0.012 L=11.0' S=0.0509 '/' Outflow=0.05 cfs 0.004 af

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Pond 67P: CB #17	Peak Elev=50.25' Inflow=0.28 cfs 0.020 af 12.0" Round Culvert n=0.012 L=74.0' S=0.0050 '/' Outflow=0.28 cfs 0.020 af
Pond 68P: DMH #16	Peak Elev=49.76' Inflow=0.30 cfs 0.022 af 12.0" Round Culvert n=0.012 L=90.0' S=0.0110 '/' Outflow=0.30 cfs 0.022 af
Pond 69P: Bio #3	Peak Elev=48.79' Storage=1,679 cf Inflow=0.75 cfs 0.055 af Outflow=0.03 cfs 0.050 af
Pond 80P: YD #24	Peak Elev=48.44' Inflow=0.03 cfs 0.002 af 6.0" Round Culvert n=0.012 L=100.0' S=0.0285 '/' Outflow=0.03 cfs 0.002 af
Pond 81P: 6" CPP	Peak Elev=48.14' Inflow=0.02 cfs 0.002 af 6.0" Round Culvert n=0.012 L=85.0' S=0.0200 '/' Outflow=0.02 cfs 0.002 af
Pond 82P: CB #23	Peak Elev=46.25' Inflow=0.16 cfs 0.011 af 12.0" Round Culvert n=0.012 L=18.0' S=0.0194 '/' Outflow=0.16 cfs 0.011 af
Pond 83P: Bio #4	Peak Elev=46.25' Storage=339 cf Inflow=0.19 cfs 0.013 af Outflow=0.01 cfs 0.013 af
Link 100L: POA #100 - SW	Inflow=0.01 cfs 0.008 af Primary=0.01 cfs 0.008 af
Link 200L: POA #200 - South	Inflow=0.10 cfs 0.057 af Primary=0.10 cfs 0.057 af
Link 300L: POA #300 - SE	Inflow=0.04 cfs 0.064 af Primary=0.04 cfs 0.064 af

Total Runoff Area = 30.826 ac Runoff Volume = 0.149 af Average Runoff Depth = 0.06" 87.29% Pervious = 26.907 ac 12.71% Impervious = 3.919 ac



Tc=6.0 min CN=74 Runoff=0.14 cfs 0.010 af

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=65,016 sf 9.83% Impervious Runoff Depth=1.38" Subcatchment 1S: West Corner Flow Length=366' Tc=9.8 min CN=75 Runoff=2.06 cfs 0.172 af Runoff Area=445,535 sf 8.04% Impervious Runoff Depth=1.25" Subcatchment 2.1S: Central Flow Length=1,341' Tc=15.8 min CN=73 Runoff=10.62 cfs 1.069 af Runoff Area=102,088 sf 10.13% Impervious Runoff Depth=1.51" Subcatchment 2.2S: South of SQ Drive Flow Length=391' Tc=6.0 min CN=77 Runoff=4.10 cfs 0.295 af Runoff Area=284,221 sf 6.78% Impervious Runoff Depth=1.19" Subcatchment 2S: North Corner Tc=0.0 min CN=72 Runoff=10.62 cfs 0.649 af Runoff Area=308,423 sf 2.18% Impervious Runoff Depth=0.97" Subcatchment 3S: SE Corner Flow Length=1,149' Tc=15.9 min CN=68 Runoff=5.30 cfs 0.570 af Runoff Area=10,178 sf 99.02% Impervious Runoff Depth>3.36" Subcatchment 10S: Parking Lot Tc=790.0 min CN=98 Runoff=0.06 cfs 0.065 af Runoff Area=588 sf 65.82% Impervious Runoff Depth=2.55" Subcatchment 11S: Island Tc=6.0 min CN=90 Runoff=0.04 cfs 0.003 af Runoff Area=1,878 sf 65.12% Impervious Runoff Depth=2.55" Subcatchment 12S: Building Tc=6.0 min CN=90 Runoff=0.13 cfs 0.009 af Runoff Area=1,349 sf 73.83% Impervious Runoff Depth=2.74" Subcatchment 13S: Building Tc=6.0 min CN=92 Runoff=0.10 cfs 0.007 af Runoff Area=1,022 sf 77.79% Impervious Runoff Depth=2.84" Subcatchment 14S: Building Tc=6.0 min CN=93 Runoff=0.08 cfs 0.006 af Runoff Area=1,377 sf 43.21% Impervious Runoff Depth=2.03" Subcatchment 15S: Building Tc=6.0 min CN=84 Runoff=0.08 cfs 0.005 af Runoff Area=928 sf 26.51% Impervious Runoff Depth=1.72" Subcatchment 16S: Island Tc=6.0 min CN=80 Runoff=0.04 cfs 0.003 af Subcatchment 17S: To Bio #1 Runoff Area=2,893 sf 0.28% Impervious Runoff Depth=1.32" Tc=6.0 min CN=74 Runoff=0.10 cfs 0.007 af Runoff Area=9,167 sf 100.00% Impervious Runoff Depth=3.38" Subcatchment 20S: Building Tc=6.0 min CN=98 Runoff=0.74 cfs 0.059 af Runoff Area=2,620 sf 100.00% Impervious Runoff Depth=3.38" **Subcatchment 21S: Parking Lot** Tc=6.0 min CN=98 Runoff=0.21 cfs 0.017 af Subcatchment 22S: To Bio #2 Runoff Area=3,961 sf 0.00% Impervious Runoff Depth=1.32"

Subcatchment 30S: Roadside	Runoff Area=8,230 sf 53.10% Impervious Runoff Depth=2.28" Flow Length=204' Tc=6.0 min CN=87 Runoff=0.50 cfs 0.036 af
Subcatchment31S: Roadside	Runoff Area=7,135 sf 71.11% Impervious Runoff Depth=2.65" Flow Length=143' Tc=6.0 min CN=91 Runoff=0.50 cfs 0.036 af
Subcatchment40S: Building	Runoff Area=3,066 sf 100.00% Impervious Runoff Depth=3.38" Tc=6.0 min CN=98 Runoff=0.25 cfs 0.020 af
Subcatchment41S: Building	Runoff Area=2,120 sf 90.94% Impervious Runoff Depth=3.15" Tc=6.0 min CN=96 Runoff=0.17 cfs 0.013 af
Subcatchment42S: Building	Runoff Area=2,162 sf 100.00% Impervious Runoff Depth=3.38" Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af
Subcatchment44S: Roadside	Runoff Area=4,663 sf 40.92% Impervious Runoff Depth=2.03" Tc=6.0 min CN=84 Runoff=0.26 cfs 0.018 af
Subcatchment45S: Parking Lot	Runoff Area=3,851 sf 71.88% Impervious Runoff Depth=2.65" Tc=6.0 min CN=91 Runoff=0.27 cfs 0.019 af
Subcatchment46S: Parking Lot	Runoff Area=4,489 sf 73.25% Impervious Runoff Depth=2.74" Tc=6.0 min CN=92 Runoff=0.32 cfs 0.024 af
Subcatchment48S: Roadside	Runoff Area=3,415 sf 55.67% Impervious Runoff Depth=2.37" Tc=6.0 min CN=88 Runoff=0.22 cfs 0.015 af
Subcatchment49S: Driveway	Runoff Area=3,652 sf 83.90% Impervious Runoff Depth=2.84" Tc=6.0 min CN=93 Runoff=0.27 cfs 0.020 af
Subcatchment 60S: Parking Lot	Runoff Area=9,169 sf 78.19% Impervious Runoff Depth=2.84" Flow Length=116' Tc=6.0 min CN=93 Runoff=0.67 cfs 0.050 af
Subcatchment 61S: Parking Lot	Runoff Area=7,068 sf 91.98% Impervious Runoff Depth=3.15" Flow Length=111' Tc=6.0 min CN=96 Runoff=0.55 cfs 0.043 af
Subcatchment 63S: Building	Runoff Area=1,459 sf 65.52% Impervious Runoff Depth=2.55" Tc=6.0 min CN=90 Runoff=0.10 cfs 0.007 af
Subcatchment 64S: Building	Runoff Area=1,506 sf 81.27% Impervious Runoff Depth=2.94" Tc=6.0 min CN=94 Runoff=0.11 cfs 0.008 af
Subcatchment65S: Building	Runoff Area=982 sf 80.86% Impervious Runoff Depth=2.84" Tc=6.0 min CN=93 Runoff=0.07 cfs 0.005 af
Subcatchment 66S: Building	Runoff Area=1,478 sf 44.79% Impervious Runoff Depth=1.87" Tc=6.0 min CN=82 Runoff=0.07 cfs 0.005 af
Subcatchment 67S: Landscape	Runoff Area=1,511 sf 10.32% Impervious Runoff Depth=0.76" Tc=6.0 min CN=64 Runoff=0.03 cfs 0.002 af
Subcatchment 68S: Building	Runoff Area=1,370 sf 100.00% Impervious Runoff Depth=3.38" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af

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Runoff Area=12,794 sf 0.00% Impervious Runoff Depth=1.02" Subcatchment 69S: To Pond

Tc=6.0 min CN=69 Runoff=0.32 cfs 0.025 af

Subcatchment 70S: Building Runoff Area=6,905 sf 100.00% Impervious Runoff Depth=3.38"

Tc=6.0 min CN=98 Runoff=0.56 cfs 0.045 af

Runoff Area=1,982 sf 84.56% Impervious Runoff Depth=2.94" Subcatchment 80S: Building

Tc=6.0 min CN=94 Runoff=0.15 cfs 0.011 af

Subcatchment81S: Building Runoff Area=1,200 sf 100.00% Impervious Runoff Depth=3.38"

Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af

Runoff Area=8,819 sf 89.53% Impervious Runoff Depth=3.05" Subcatchment 82S: Parking Lot

Flow Length=214' Tc=6.0 min CN=95 Runoff=0.68 cfs 0.051 af

Runoff Area=2,507 sf 0.00% Impervious Runoff Depth=1.32" Subcatchment 83S: To Pond

Tc=6.0 min CN=74 Runoff=0.09 cfs 0.006 af

Avg. Flow Depth=0.45' Max Vel=1.48 fps Inflow=2.22 cfs 0.649 af Reach 2.1R: Wetland Flow Path

n=0.040 L=344.0' S=0.0075 '/' Capacity=54.59 cfs Outflow=2.22 cfs 0.649 af

Avg. Flow Depth=0.64' Max Vel=4.62 fps Inflow=11.57 cfs 1.875 af Reach 2.2R: Wetland Flow Path

n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=11.56 cfs 1.875 af

Avg. Flow Depth=0.28' Max Vel=2.78 fps Inflow=2.23 cfs 0.649 af Reach 2R: Wetland Flow Path

n=0.040 L=151.0' S=0.0446'/' Capacity=133.09 cfs Outflow=2.22 cfs 0.649 af

Avg. Flow Depth=0.05' Max Vel=0.38 fps Inflow=0.07 cfs 0.040 af Reach 10R: Swale

n=0.035 L=44.0' S=0.0050 '/' Capacity=16.22 cfs Outflow=0.07 cfs 0.040 af

Reach 22R: Wetland Flow Path Avg. Flow Depth=0.04' Max Vel=0.67 fps Inflow=0.29 cfs 0.085 af

n=0.040 L=211.0' S=0.0245'/' Capacity=392.58 cfs Outflow=0.29 cfs 0.085 af

Avg. Flow Depth=0.38' Max Vel=2.11 fps Inflow=2.51 cfs 0.734 af Reach 23R: Wetland Flow Path

n=0.040 L=131.0' S=0.0185 '/' Capacity=85.86 cfs Outflow=2.50 cfs 0.734 af

Avg. Flow Depth=0.23' Max Vel=0.88 fps Inflow=0.93 cfs 0.321 af Reach 69R: Swale

n=0.069 L=17.0' S=0.0147'/' Capacity=14.11 cfs Outflow=0.93 cfs 0.321 af

Avg. Flow Depth=0.19' Max Vel=0.41 fps Inflow=0.93 cfs 0.321 af Reach 70R: Woodland Flow Path

n=0.400 L=57.0' S=0.1404 '/' Capacity=21.20 cfs Outflow=0.93 cfs 0.321 af

Reach 71R: Stream Avg. Flow Depth=0.16' Max Vel=2.29 fps Inflow=0.93 cfs 0.321 af

n=0.040 L=80.0' S=0.0554 '/' Capacity=31.12 cfs Outflow=0.93 cfs 0.321 af

Reach 72R: Stream Avg. Flow Depth=0.16' Max Vel=1.29 fps Inflow=0.93 cfs 0.321 af

n=0.040 L=88.0' S=0.0160 '/' Capacity=25.40 cfs Outflow=0.93 cfs 0.320 af

Avg. Flow Depth=0.19' Max Vel=1.43 fps Inflow=1.25 cfs 0.397 af Reach 73R: Stream

n=0.040 L=309.0' S=0.0160 '/' Capacity=25.38 cfs Outflow=1.24 cfs 0.396 af

6.0" Round Culvert n=0.012 L=174.0' S=0.0150 '/' Outflow=0.25 cfs 0.020 af

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Reach 83R: Woodland Flow I	Path Avg. Flow Depth=0.11' Max Vel=0.25 fps Inflow=0.33 cfs 0.076 af n=0.400 L=122.0' S=0.0950 '/' Capacity=17.44 cfs Outflow=0.32 cfs 0.076 af
Pond 1P: 15" RCP	Peak Elev=53.11' Storage=69 cf Inflow=2.08 cfs 0.212 af 15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=2.02 cfs 0.212 af
Pond 2.1P: 24" RCP	Peak Elev=49.46' Storage=3,036 cf Inflow=12.85 cfs 1.803 af 24.0" Round Culvert n=0.012 L=17.0' S=0.0135 '/' Outflow=11.20 cfs 1.803 af
Pond 2P: 12" CPP	Peak Elev=60.71' Storage=8,446 cf Inflow=10.62 cfs 0.649 af Outflow=2.23 cfs 0.649 af
Pond 10P: Porous Pavement	Peak Elev=0.52' Storage=573 cf Inflow=0.06 cfs 0.065 af Outflow=0.03 cfs 0.065 af
Pond 11P: YD #3-1	Peak Elev=57.49' Inflow=0.04 cfs 0.003 af 6.0" Round Culvert n=0.012 L=36.0' S=0.0050 '/' Outflow=0.04 cfs 0.003 af
Pond 12P: YD #7	Peak Elev=57.99' Inflow=0.13 cfs 0.009 af 8.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=0.13 cfs 0.009 af
Pond 13P: YD #6	Peak Elev=57.62' Inflow=0.22 cfs 0.016 af 10.0" Round Culvert n=0.012 L=29.0' S=0.0052 '/' Outflow=0.22 cfs 0.016 af
Pond 14P: YD #5	Peak Elev=57.49' Inflow=0.30 cfs 0.022 af 10.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=0.30 cfs 0.022 af
Pond 15P: YD #4	Peak Elev=57.49' Inflow=0.37 cfs 0.027 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.37 cfs 0.027 af
Pond 16P: CB #3	Peak Elev=57.49' Inflow=0.46 cfs 0.033 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0049 '/' Outflow=0.46 cfs 0.033 af
Pond 17P: Bio #1	Peak Elev=57.49' Storage=933 cf Inflow=0.56 cfs 0.040 af Outflow=0.07 cfs 0.040 af
Pond 21P: CB #8	Peak Elev=59.00' Inflow=0.21 cfs 0.017 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0050 '/' Outflow=0.21 cfs 0.017 af
Pond 22P: Bio #2	Peak Elev=59.00' Storage=1,829 cf Inflow=1.09 cfs 0.086 af Outflow=0.29 cfs 0.085 af
Pond 30P: CB #10-2	Peak Elev=53.00' Inflow=0.50 cfs 0.036 af 12.0" Round Culvert n=0.012 L=78.0' S=0.0397 '/' Outflow=0.50 cfs 0.036 af
Pond 31P: CB #10-1	Peak Elev=50.00' Inflow=0.50 cfs 0.036 af 12.0" Round Culvert n=0.012 L=2.0' S=0.0250 '/' Outflow=0.50 cfs 0.036 af
Pond 32P: DMH #10	Peak Elev=48.89' Inflow=11.57 cfs 1.875 af 24.0" Round Culvert n=0.012 L=57.0' S=0.0135 '/' Outflow=11.57 cfs 1.875 af
Pond 40P: 6" CPP	Peak Elev=53.89' Inflow=0.25 cfs 0.020 af

Peak Elev=51.17' Inflow=0.41 cfs 0.033 af Pond 41P: YD #15 8.0" Round Culvert n=0.012 L=47.0' S=0.0149 '/' Outflow=0.41 cfs 0.033 af Peak Elev=53.07' Inflow=0.17 cfs 0.014 af Pond 42P: 6" CPP 6.0" Round Culvert n=0.012 L=150.0' S=0.0175 '/' Outflow=0.17 cfs 0.014 af Peak Elev=50.85' Inflow=0.59 cfs 0.047 af Pond 43P: 10" CPP 8.0" Round Culvert n=0.012 L=33.0' S=0.0148 '/' Outflow=0.59 cfs 0.047 af Peak Elev=50.85' Inflow=0.84 cfs 0.065 af Pond 44P: CB #14 12.0" Round Culvert n=0.012 L=31.0' S=0.0048 '/' Outflow=0.84 cfs 0.065 af Peak Elev=50.85' Inflow=0.27 cfs 0.019 af Pond 45P: CB #13-2 12.0" Round Culvert n=0.012 L=22.0' S=0.0245 '/' Outflow=0.27 cfs 0.019 af Peak Elev=50.85' Inflow=0.32 cfs 0.024 af Pond 46P: CB #13-1 12.0" Round Culvert n=0.012 L=12.0' S=0.0325 '/' Outflow=0.32 cfs 0.024 af Peak Elev=50.85' Inflow=1.43 cfs 0.108 af Pond 47P: DMH #13 12.0" Round Culvert n=0.012 L=67.0' S=0.0051 '/' Outflow=1.43 cfs 0.108 af Peak Elev=50.84' Inflow=0.22 cfs 0.015 af Pond 48P: CB #12-2 12.0" Round Culvert n=0.012 L=6.0' S=0.0050 '/' Outflow=0.22 cfs 0.015 af Peak Elev=50.84' Inflow=0.27 cfs 0.020 af Pond 49P: CB #12-1 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.27 cfs 0.020 af Peak Elev=50.84' Inflow=1.92 cfs 0.143 af Pond 50P: DMH #12 15.0" Round Culvert n=0.012 L=106.0' S=0.0040 '/' Outflow=1.92 cfs 0.143 af Peak Elev=51.11' Inflow=0.67 cfs 0.050 af Pond 60P: CB #17-1-2 12.0" Round Culvert n=0.012 L=21.0' S=0.0052 '/' Outflow=0.67 cfs 0.050 af Peak Elev=51.08' Inflow=0.55 cfs 0.043 af Pond 61P: CB #17-1-1 12.0" Round Culvert n=0.012 L=3.0' S=0.0367 '/' Outflow=0.55 cfs 0.043 af Pond 62P: DMH #17-1 Peak Elev=51.04' Inflow=1.23 cfs 0.092 af 12.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=1.23 cfs 0.092 af Peak Elev=51.88' Inflow=0.10 cfs 0.007 af Pond 63P: YD #21 12.0" Round Culvert n=0.012 L=49.0' S=0.0049 '/' Outflow=0.10 cfs 0.007 af Peak Elev=51.56' Inflow=0.21 cfs 0.016 af Pond 64P: YD #20 10.0" Round Culvert n=0.012 L=35.0' S=0.0049 '/' Outflow=0.21 cfs 0.016 af Pond 65P: YD #19 Peak Elev=51.32' Inflow=0.28 cfs 0.021 af 10.0" Round Culvert n=0.012 L=42.0' S=0.0050 '/' Outflow=0.28 cfs 0.021 af Pond 66P: YD #18 Peak Elev=50.99' Inflow=0.36 cfs 0.026 af 12.0" Round Culvert n=0.012 L=11.0' S=0.0509 '/' Outflow=0.36 cfs 0.026 af

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Type III 24-hr 2-year Rainfall=3.61"

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Pond 67P: CB #17	Peak Elev=50.88'	Inflow=1.61 cfs 0.121 af
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12.0" Round Culvert n=0.012 L=74.0' S=0.0050 '/' Outflow=1.61 cfs 0.121 af

Pond 68P: DMH #16 Peak Elev=50.85' Inflow=1.72 cfs 0.130 af

12.0" Round Culvert n=0.012 L=90.0' S=0.0110 '/' Outflow=1.72 cfs 0.130 af

Pond 69P: Bio #3 Peak Elev=50.83' Storage=7,720 cf Inflow=4.51 cfs 0.342 af

Outflow=0.93 cfs 0.321 af

Pond 80P: YD #24 Peak Elev=48.58' Inflow=0.15 cfs 0.011 af

6.0" Round Culvert n=0.012 L=100.0' S=0.0285 '/' Outflow=0.15 cfs 0.011 af

Pond 81P: 6" CPP Peak Elev=48.24' Inflow=0.10 cfs 0.008 af

6.0" Round Culvert n=0.012 L=85.0' S=0.0200 '/' Outflow=0.10 cfs 0.008 af

Pond 82P: CB #23 Peak Elev=47.67' Inflow=0.78 cfs 0.059 af

12.0" Round Culvert n=0.012 L=18.0' S=0.0194 '/' Outflow=0.78 cfs 0.059 af

Pond 83P: Bio #4 Peak Elev=47.67' Storage=1,453 cf Inflow=1.01 cfs 0.077 af

Outflow=0.33 cfs 0.076 af

Link 100L: POA #100 - SW Inflow=2.02 cfs 0.212 af

Primary=2.02 cfs 0.212 af

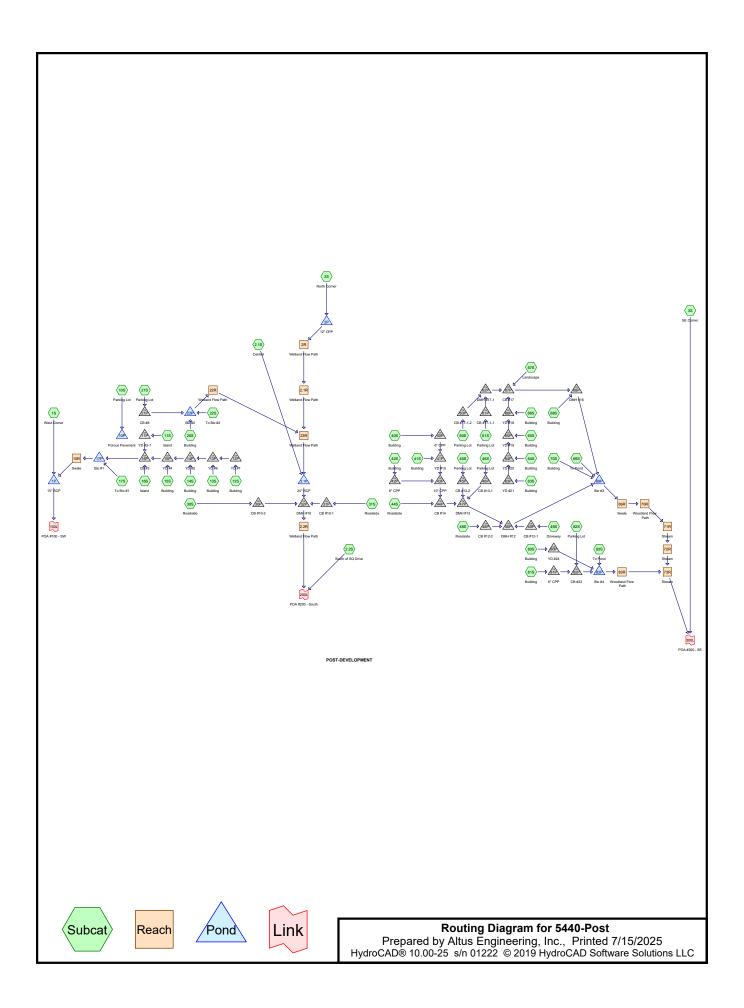
Link 200L: POA #200 - South Inflow=13.31 cfs 2.170 af

Primary=13.31 cfs 2.170 af

Link 300L: POA #300 - SE Inflow=5.85 cfs 0.966 af

Primary=5.85 cfs 0.966 af

Total Runoff Area = 30.826 ac Runoff Volume = 3.438 af Average Runoff Depth = 1.34" 87.29% Pervious = 26.907 ac 12.71% Impervious = 3.919 ac



# Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
(acies)		
0.229	61	>75% Grass cover, Good, HSG B (2.1S, 3S, 48S, 49S, 61S, 66S, 67S, 69S, 82S)
3.987	74	>75% Grass cover, Good, HSG C (1S, 2.1S, 2.2S, 2S, 3S, 10S, 11S, 12S, 13S,
		14S, 15S, 16S, 17S, 22S, 30S, 31S, 41S, 44S, 45S, 46S, 48S, 49S, 60S, 61S, 63S,
		64S, 65S, 66S, 69S, 80S, 82S, 83S)
0.107	80	>75% Grass cover, Good, HSG D (2.1S, 2.2S, 2S, 48S, 49S)
0.203	65	Brush, Good, HSG C (2.1S)
0.117	98	Paved parking, HSG B (2.1S, 3S, 49S, 61S, 67S, 82S)
2.047	98	Paved parking, HSG C (2.1S, 2.2S, 2S, 3S, 30S, 31S, 44S, 45S, 46S, 48S, 49S,
		60S, 61S, 66S, 80S, 82S)
0.241	98	Paved parking, HSG D (2.1S, 2.2S, 2S, 3S, 48S, 49S)
0.442	98	Paved roads w/curbs & sewers, HSG C (1S, 10S, 11S, 12S, 15S, 16S, 17S, 21S)
0.035	98	Roofs, HSG B (66S, 68S, 70S)
1.037	98	Roofs, HSG C (2.1S, 2S, 11S, 12S, 13S, 14S, 15S, 20S, 21S, 40S, 41S, 42S, 48S,
		63S, 64S, 65S, 66S, 68S, 70S, 80S, 81S)
1.930	55	Woods, Good, HSG B (1S, 2.1S, 2S, 3S, 67S)
17.179	70	Woods, Good, HSG C (1S, 2.1S, 2.2S, 2S, 3S, 60S)
3.274	77	Woods, Good, HSG D (2.1S, 2.2S, 2S)
30.826	74	TOTAL AREA

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# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
2.310	HSG B	1S, 2.1S, 2S, 3S, 48S, 49S, 61S, 66S, 67S, 68S, 69S, 70S, 82S
24.894	HSG C	1S, 2.1S, 2.2S, 2S, 3S, 10S, 11S, 12S, 13S, 14S, 15S, 16S, 17S, 20S, 21S, 22S,
		30S, 31S, 40S, 41S, 42S, 44S, 45S, 46S, 48S, 49S, 60S, 61S, 63S, 64S, 65S,
		66S, 68S, 69S, 70S, 80S, 81S, 82S, 83S
3.622	HSG D	2.1S, 2.2S, 2S, 3S, 48S, 49S
0.000	Other	
30.826		TOTAL AREA

Runoff Area=3,961 sf 0.00% Impervious Runoff Depth=2.74"

Tc=6.0 min CN=74 Runoff=0.29 cfs 0.021 af

Subcatchment 22S: To Bio #2

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=65,016 sf 9.83% Impervious Runoff Depth=2.84" Subcatchment 1S: West Corner Flow Length=366' Tc=9.8 min CN=75 Runoff=4.36 cfs 0.353 af Runoff Area=445,535 sf 8.04% Impervious Runoff Depth=2.65" Subcatchment 2.1S: Central Flow Length=1,341' Tc=15.8 min CN=73 Runoff=23.46 cfs 2.263 af Runoff Area=102,088 sf 10.13% Impervious Runoff Depth=3.02" Subcatchment 2.2S: South of SQ Drive Flow Length=391' Tc=6.0 min CN=77 Runoff=8.31 cfs 0.590 af Runoff Area=284,221 sf 6.78% Impervious Runoff Depth=2.57" Subcatchment 2S: North Corner Tc=0.0 min CN=72 Runoff=23.92 cfs 1.395 af Runoff Area=308,423 sf 2.18% Impervious Runoff Depth=2.22" Subcatchment 3S: SE Corner Flow Length=1,149' Tc=15.9 min CN=68 Runoff=13.31 cfs 1.310 af Runoff Area=10,178 sf 99.02% Impervious Runoff Depth>5.20" Subcatchment 10S: Parking Lot Tc=790.0 min CN=98 Runoff=0.09 cfs 0.101 af Runoff Area=588 sf 65.82% Impervious Runoff Depth=4.33" Subcatchment 11S: Island Tc=6.0 min CN=90 Runoff=0.07 cfs 0.005 af Runoff Area=1,878 sf 65.12% Impervious Runoff Depth=4.33" Subcatchment 12S: Building Tc=6.0 min CN=90 Runoff=0.21 cfs 0.016 af Runoff Area=1,349 sf 73.83% Impervious Runoff Depth=4.55" Subcatchment 13S: Building Tc=6.0 min CN=92 Runoff=0.16 cfs 0.012 af Runoff Area=1,022 sf 77.79% Impervious Runoff Depth=4.66" Subcatchment 14S: Building Tc=6.0 min CN=93 Runoff=0.12 cfs 0.009 af Runoff Area=1,377 sf 43.21% Impervious Runoff Depth=3.70" Subcatchment 15S: Building Tc=6.0 min CN=84 Runoff=0.14 cfs 0.010 af Runoff Area=928 sf 26.51% Impervious Runoff Depth=3.31" Subcatchment 16S: Island Tc=6.0 min CN=80 Runoff=0.08 cfs 0.006 af Subcatchment 17S: To Bio #1 Runoff Area=2,893 sf 0.28% Impervious Runoff Depth=2.74" Tc=6.0 min CN=74 Runoff=0.21 cfs 0.015 af Runoff Area=9,167 sf 100.00% Impervious Runoff Depth=5.23" Subcatchment 20S: Building Tc=6.0 min CN=98 Runoff=1.13 cfs 0.092 af Runoff Area=2,620 sf 100.00% Impervious Runoff Depth=5.23" **Subcatchment 21S: Parking Lot** Tc=6.0 min CN=98 Runoff=0.32 cfs 0.026 af

Subcatchment30S: Roadside	Runoff Area=8,230 sf 53.10% Impervious Runoff Depth=4.01" Flow Length=204' Tc=6.0 min CN=87 Runoff=0.87 cfs 0.063 af
Subcatchment31S: Roadside	Runoff Area=7,135 sf 71.11% Impervious Runoff Depth=4.44" Flow Length=143' Tc=6.0 min CN=91 Runoff=0.81 cfs 0.061 af
Subcatchment 40S: Building	Runoff Area=3,066 sf 100.00% Impervious Runoff Depth=5.23" Tc=6.0 min CN=98 Runoff=0.38 cfs 0.031 af
Subcatchment41S: Building	Runoff Area=2,120 sf 90.94% Impervious Runoff Depth=5.00" Tc=6.0 min CN=96 Runoff=0.26 cfs 0.020 af
Subcatchment 42S: Building	Runoff Area=2,162 sf 100.00% Impervious Runoff Depth=5.23" Tc=6.0 min CN=98 Runoff=0.27 cfs 0.022 af
Subcatchment44S: Roadside	Runoff Area=4,663 sf 40.92% Impervious Runoff Depth=3.70" Tc=6.0 min CN=84 Runoff=0.46 cfs 0.033 af
Subcatchment 45S: Parking Lot	Runoff Area=3,851 sf 71.88% Impervious Runoff Depth=4.44" Tc=6.0 min CN=91 Runoff=0.44 cfs 0.033 af
Subcatchment 46S: Parking Lot	Runoff Area=4,489 sf 73.25% Impervious Runoff Depth=4.55" Tc=6.0 min CN=92 Runoff=0.52 cfs 0.039 af
Subcatchment48S: Roadside	Runoff Area=3,415 sf 55.67% Impervious Runoff Depth=4.12" Tc=6.0 min CN=88 Runoff=0.37 cfs 0.027 af
Subcatchment 49S: Driveway	Runoff Area=3,652 sf 83.90% Impervious Runoff Depth=4.66" Tc=6.0 min CN=93 Runoff=0.43 cfs 0.033 af
Subcatchment 60S: Parking Lot	Runoff Area=9,169 sf 78.19% Impervious Runoff Depth=4.66" Flow Length=116' Tc=6.0 min CN=93 Runoff=1.07 cfs 0.082 af
Subcatchment 61S: Parking Lot	Runoff Area=7,068 sf 91.98% Impervious Runoff Depth=5.00" Flow Length=111' Tc=6.0 min CN=96 Runoff=0.86 cfs 0.068 af
Subcatchment 63S: Building	Runoff Area=1,459 sf 65.52% Impervious Runoff Depth=4.33" Tc=6.0 min CN=90 Runoff=0.16 cfs 0.012 af
Subcatchment 64S: Building	Runoff Area=1,506 sf 81.27% Impervious Runoff Depth=4.77" Tc=6.0 min CN=94 Runoff=0.18 cfs 0.014 af
Subcatchment 65S: Building	Runoff Area=982 sf 80.86% Impervious Runoff Depth=4.66" Tc=6.0 min CN=93 Runoff=0.12 cfs 0.009 af
Subcatchment 66S: Building	Runoff Area=1,478 sf 44.79% Impervious Runoff Depth=3.50" Tc=6.0 min CN=82 Runoff=0.14 cfs 0.010 af
Subcatchment 67S: Landscape	Runoff Area=1,511 sf 10.32% Impervious Runoff Depth=1.89" Tc=6.0 min CN=64 Runoff=0.07 cfs 0.005 af
Subcatchment 68S: Building	Runoff Area=1,370 sf 100.00% Impervious Runoff Depth=5.23" Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af

Subcatchment 69S: To Pond Runoff Area=12,794 sf 0.00% Impervious Runoff Depth=2.31"

Tc=6.0 min CN=69 Runoff=0.78 cfs 0.056 af

Subcatchment 70S: Building Runoff Area=6,905 sf 100.00% Impervious Runoff Depth=5.23"

Tc=6.0 min CN=98 Runoff=0.85 cfs 0.069 af

Subcatchment 80S: Building Runoff Area=1,982 sf 84.56% Impervious Runoff Depth=4.77"

Tc=6.0 min CN=94 Runoff=0.24 cfs 0.018 af

Subcatchment 81S: Building Runoff Area=1,200 sf 100.00% Impervious Runoff Depth=5.23"

Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af

Subcatchment 82S: Parking Lot Runoff Area=8,819 sf 89.53% Impervious Runoff Depth=4.89"

Flow Length=214' Tc=6.0 min CN=95 Runoff=1.06 cfs 0.082 af

Subcatchment 83S: To Pond Runoff Area=2,507 sf 0.00% Impervious Runoff Depth=2.74"

Tc=6.0 min CN=74 Runoff=0.18 cfs 0.013 af

**Reach 2.1R: Wetland Flow Path**Avg. Flow Depth=1.19' Max Vel=2.53 fps Inflow=18.63 cfs 1.395 af n=0.040 L=344.0' S=0.0075 '/' Capacity=54.59 cfs Outflow=16.73 cfs 1.395 af

Reach 2.2R: Wetland Flow Path Avg. Flow Depth=0.81' Max Vel=5.27 fps Inflow=19.20 cfs 3.919 af

n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=18.90 cfs 3.919 af

Reach 2R: Wetland Flow Path Avg. Flow Depth=0.83' Max Vel=5.02 fps Inflow=18.70 cfs 1.395 af

n=0.040 L=151.0' S=0.0446 '/' Capacity=133.09 cfs Outflow=18.63 cfs 1.395 af

Reach 10R: Swale Avg. Flow Depth=0.11' Max Vel=0.64 fps Inflow=0.30 cfs 0.072 af

 $n = 0.035 \quad L = 44.0' \quad S = 0.0050 \; \text{'/'} \quad Capacity = 16.22 \; cfs \quad Outflow = 0.30 \; cfs \; \; 0.072 \; af$ 

Reach 22R: Wetland Flow Path Avg. Flow Depth=0.05' Max Vel=0.80 fps Inflow=0.44 cfs 0.137 af

n=0.040 L=211.0' S=0.0245 '/' Capacity=392.58 cfs Outflow=0.44 cfs 0.137 af

Reach 23R: Wetland Flow Path Avg. Flow Depth=0.97' Max Vel=3.54 fps Inflow=17.02 cfs 1.532 af

n=0.040 L=131.0' S=0.0185'/' Capacity=85.86 cfs Outflow=16.92 cfs 1.532 af

Reach 69R: Swale Avg. Flow Depth=0.39' Max Vel=1.21 fps Inflow=2.47 cfs 0.552 af

n=0.069 L=17.0' S=0.0147'/' Capacity=14.11 cfs Outflow=2.47 cfs 0.552 af

Reach 70R: Woodland Flow Path

Avg. Flow Depth=0.33' Max Vel=0.57 fps Inflow=2.47 cfs 0.552 af

 $n = 0.400 \quad L = 57.0' \quad S = 0.1404 \; \text{$'$} \quad Capacity = 21.20 \; cfs \quad Outflow = 2.47 \; cfs \quad 0.552 \; af$ 

Reach 71R: Stream Avg. Flow Depth=0.28' Max Vel=3.10 fps Inflow=2.47 cfs 0.552 af

n=0.040 L=80.0' S=0.0554 '/' Capacity=31.12 cfs Outflow=2.47 cfs 0.552 af

Reach 72R: Stream Avg. Flow Depth=0.28' Max Vel=1.80 fps Inflow=2.47 cfs 0.552 af

n=0.040 L=88.0' S=0.0160 '/' Capacity=25.40 cfs Outflow=2.47 cfs 0.552 af

Reach 73R: Stream Avg. Flow Depth=0.31' Max Vel=1.91 fps Inflow=2.96 cfs 0.677 af

n=0.040 L=309.0' S=0.0160'/' Capacity=25.38 cfs Outflow=2.95 cfs 0.676 af

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Reach 83R: Woodland Flow I	Path Avg. Flow Depth=0.15' Max Vel=0.29 fps Inflow=0.50 cfs 0.125 af n=0.400 L=122.0' S=0.0950 '/' Capacity=17.44 cfs Outflow=0.49 cfs 0.125 af
Pond 1P: 15" RCP	Peak Elev=53.52' Storage=659 cf Inflow=4.57 cfs 0.424 af 15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=3.74 cfs 0.424 af
Pond 2.1P: 24" RCP	Peak Elev=51.35' Storage=23,483 cf Inflow=35.08 cfs 3.795 af 24.0" Round Culvert n=0.012 L=17.0' S=0.0135 '/' Outflow=18.86 cfs 3.795 af
Pond 2P: 12" CPP	Peak Elev=60.93' Storage=11,719 cf Inflow=23.92 cfs 1.395 af Outflow=18.70 cfs 1.395 af
Pond 10P: Porous Pavement	Peak Elev=1.48' Storage=1,631 cf Inflow=0.09 cfs 0.101 af Outflow=0.04 cfs 0.097 af
Pond 11P: YD #3-1	Peak Elev=57.89' Inflow=0.07 cfs 0.005 af 6.0" Round Culvert n=0.012 L=36.0' S=0.0050 '/' Outflow=0.07 cfs 0.005 af
Pond 12P: YD #7	Peak Elev=58.07' Inflow=0.21 cfs 0.016 af 8.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=0.21 cfs 0.016 af
Pond 13P: YD #6	Peak Elev=57.90' Inflow=0.37 cfs 0.027 af 10.0" Round Culvert n=0.012 L=29.0' S=0.0052 '/' Outflow=0.37 cfs 0.027 af
Pond 14P: YD #5	Peak Elev=57.90' Inflow=0.49 cfs 0.036 af 10.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=0.49 cfs 0.036 af
Pond 15P: YD #4	Peak Elev=57.89' Inflow=0.62 cfs 0.046 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.62 cfs 0.046 af
Pond 16P: CB #3	Peak Elev=57.89' Inflow=0.77 cfs 0.057 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0049 '/' Outflow=0.77 cfs 0.057 af
Pond 17P: Bio #1	Peak Elev=57.89' Storage=1,368 cf Inflow=0.98 cfs 0.072 af Outflow=0.30 cfs 0.072 af
Pond 21P: CB #8	Peak Elev=59.46' Inflow=0.32 cfs 0.026 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0050 '/' Outflow=0.32 cfs 0.026 af
Pond 22P: Bio #2	Peak Elev=59.46' Storage=2,733 cf Inflow=1.74 cfs 0.139 af Outflow=0.44 cfs 0.137 af
Pond 30P: CB #10-2	Peak Elev=53.13' Inflow=0.87 cfs 0.063 af 12.0" Round Culvert n=0.012 L=78.0' S=0.0397 '/' Outflow=0.87 cfs 0.063 af
Pond 31P: CB #10-1	Peak Elev=50.14' Inflow=0.81 cfs 0.061 af 12.0" Round Culvert n=0.012 L=2.0' S=0.0250 '/' Outflow=0.81 cfs 0.061 af
Pond 32P: DMH #10	Peak Elev=49.90' Inflow=19.20 cfs 3.919 af 24.0" Round Culvert n=0.012 L=57.0' S=0.0135 '/' Outflow=19.20 cfs 3.919 af
Pond 40P: 6" CPP	Peak Elev=53.99' Inflow=0.38 cfs 0.031 af 6.0" Round Culvert n=0.012 L=174.0' S=0.0150 '/' Outflow=0.38 cfs 0.031 af

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Pond 41P: YD #15	Peak Elev=52.44' Inflow=0.63 cfs 0.051 af 8.0" Round Culvert n=0.012 L=47.0' S=0.0149 '/' Outflow=0.63 cfs 0.051 af
Pond 42P: 6" CPP	Peak Elev=53.17' Inflow=0.27 cfs 0.022 af 6.0" Round Culvert n=0.012 L=150.0' S=0.0175 '/' Outflow=0.27 cfs 0.022 af
Pond 43P: 10" CPP	Peak Elev=52.29' Inflow=0.90 cfs 0.073 af 8.0" Round Culvert n=0.012 L=33.0' S=0.0148 '/' Outflow=0.90 cfs 0.073 af
Pond 44P: CB #14	Peak Elev=52.04' Inflow=1.36 cfs 0.106 af 12.0" Round Culvert n=0.012 L=31.0' S=0.0048 '/' Outflow=1.36 cfs 0.106 af
Pond 45P: CB #13-2	Peak Elev=51.94' Inflow=0.44 cfs 0.033 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0245 '/' Outflow=0.44 cfs 0.033 af
Pond 46P: CB #13-1	Peak Elev=51.95' Inflow=0.52 cfs 0.039 af 12.0" Round Culvert n=0.012 L=12.0' S=0.0325 '/' Outflow=0.52 cfs 0.039 af
Pond 47P: DMH #13	Peak Elev=51.93' Inflow=2.32 cfs 0.177 af 12.0" Round Culvert n=0.012 L=67.0' S=0.0051 '/' Outflow=2.32 cfs 0.177 af
Pond 48P: CB #12-2	Peak Elev=51.71' Inflow=0.37 cfs 0.027 af 12.0" Round Culvert n=0.012 L=6.0' S=0.0050 '/' Outflow=0.37 cfs 0.027 af
Pond 49P: CB #12-1	Peak Elev=51.71' Inflow=0.43 cfs 0.033 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.43 cfs 0.033 af
Pond 50P: DMH #12	Peak Elev=51.71' Inflow=3.11 cfs 0.237 af 15.0" Round Culvert n=0.012 L=106.0' S=0.0040 '/' Outflow=3.11 cfs 0.237 af
Pond 60P: CB #17-1-2	Peak Elev=52.75' Inflow=1.07 cfs 0.082 af 12.0" Round Culvert n=0.012 L=21.0' S=0.0052 '/' Outflow=1.07 cfs 0.082 af
Pond 61P: CB #17-1-1	Peak Elev=52.73' Inflow=0.86 cfs 0.068 af 12.0" Round Culvert n=0.012 L=3.0' S=0.0367 '/' Outflow=0.86 cfs 0.068 af
Pond 62P: DMH #17-1	Peak Elev=52.68' Inflow=1.93 cfs 0.149 af 12.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=1.93 cfs 0.149 af
Pond 63P: YD #21	Peak Elev=52.51' Inflow=0.16 cfs 0.012 af 12.0" Round Culvert n=0.012 L=49.0' S=0.0049 '/' Outflow=0.16 cfs 0.012 af
Pond 64P: YD #20	Peak Elev=52.51' Inflow=0.34 cfs 0.026 af 10.0" Round Culvert n=0.012 L=35.0' S=0.0049 '/' Outflow=0.34 cfs 0.026 af
Pond 65P: YD #19	Peak Elev=52.50' Inflow=0.46 cfs 0.035 af 10.0" Round Culvert n=0.012 L=42.0' S=0.0050 '/' Outflow=0.46 cfs 0.035 af
Pond 66P: YD #18	Peak Elev=52.47' Inflow=0.60 cfs 0.044 af 12.0" Round Culvert n=0.012 L=11.0' S=0.0509 '/' Outflow=0.60 cfs 0.044 af

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Pond 83P: Bio #4

Link 100L: POA #100 - SW

Type III 24-hr 10-year Rainfall=5.47"

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Pond 67P: CB #17	Peak Elev=52.45'	Inflow=2.60 cfs 0.199 af
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12.0" Round Culvert n=0.012 L=74.0' S=0.0050 '/' Outflow=2.60 cfs 0.199 af

Pond 68P: DMH #16 Peak Elev=51.92' Inflow=2.77 cfs 0.213 af

12.0" Round Culvert n=0.012 L=90.0' S=0.0110 '/' Outflow=2.77 cfs 0.213 af

Pond 69P: Bio #3 Peak Elev=51.67' Storage=11,205 cf Inflow=7.51 cfs 0.575 af

Outflow=2.47 cfs 0.552 af

Pond 80P: YD #24 Peak Elev=48.68' Inflow=0.24 cfs 0.018 af

6.0" Round Culvert n=0.012 L=100.0' S=0.0285 '/' Outflow=0.24 cfs 0.018 af

Pond 81P: 6" CPP Peak Elev=48.35' Inflow=0.15 cfs 0.012 af

6.0" Round Culvert n=0.012 L=85.0' S=0.0200 '/' Outflow=0.15 cfs 0.012 af

Pond 82P: CB #23 Peak Elev=48.31' Inflow=1.21 cfs 0.094 af 12.0" Round Culvert n=0.012 L=18.0' S=0.0194 '/' Outflow=1.21 cfs 0.094 af

12.0 TROUTE GUIVOIT II 0.012 E 10.0 0 0.0101 / Oddiow 1.21 010 0.001 al

Peak Elev=48.30' Storage=2,203 cf Inflow=1.63 cfs 0.126 af Outflow=0.50 cfs 0.125 af

Inflow=3.74 cfs 0.424 af Primary=3.74 cfs 0.424 af

Link 200L: POA #200 - South Inflow=23.08 cfs 4.509 af

Primary=23.08 cfs 4.509 af

Link 300L: POA #300 - SE Inflow=15.75 cfs 1.987 af

Primary=15.75 cfs 1.987 af

Total Runoff Area = 30.826 ac Runoff Volume = 7.048 af Average Runoff Depth = 2.74" 87.29% Pervious = 26.907 ac 12.71% Impervious = 3.919 ac Prepared by Altus Engineering, Inc.

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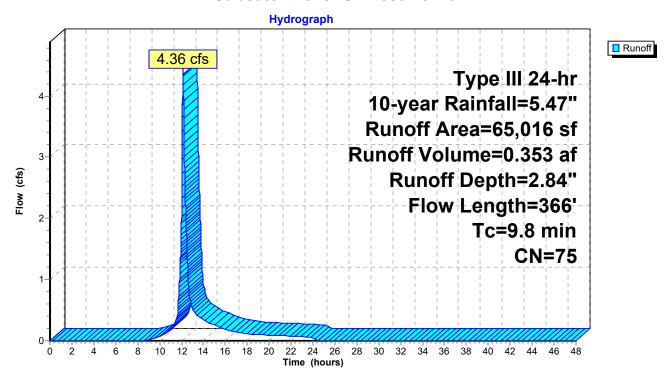
# **Summary for Subcatchment 1S: West Corner**

Runoff = 4.36 cfs @ 12.14 hrs, Volume= 0.353 af, Depth= 2.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN I	Description				
		6,392	98	Paved roads w/curbs & sewers, HSG C				
		35,003	74	>75% Grass cover, Good, HSG C				
		23,590	70	Woods, Good, HSG C				
		31	55	Noods, Go	od, HSG B			
		65,016	75 \	Neighted A				
		58,624	,	90.17% Per	vious Area			
		6,392	9	9.83% Impe	ervious Area	a		
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	4.5	35	0.1071	0.13		Sheet Flow,		
	4.5	35	0.1071	0.13		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.61"		
	4.5 1.6	35 129	0.1071 0.0388					
	1.6					Woods: Light underbrush n= 0.400 P2= 3.61"		
				1.38		Woods: Light underbrush n= 0.400 P2= 3.61"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps  Shallow Concentrated Flow,		
	1.6 0.6	129 55	0.0388	1.38 1.51		Woods: Light underbrush n= 0.400 P2= 3.61" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps		
	1.6	129	0.0388	1.38 1.51		Woods: Light underbrush n= 0.400 P2= 3.61"  Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps  Shallow Concentrated Flow, Woodland Kv= 5.0 fps  Shallow Concentrated Flow,		
_	1.6 0.6	129 55	0.0388	1.38 1.51		Woods: Light underbrush n= 0.400 P2= 3.61" <b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps <b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps		

#### **Subcatchment 1S: West Corner**



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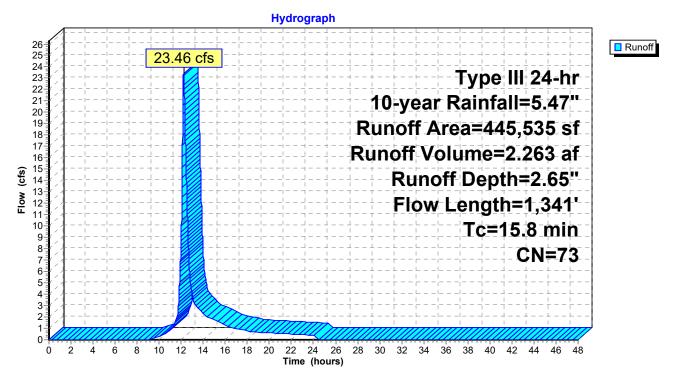
# **Summary for Subcatchment 2.1S: Central**

Runoff = 23.46 cfs @ 12.22 hrs, Volume= 2.263 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN E	Description				
	4,537	98 F	98 Paved parking, HSG D				
	25,778		1 0/				
	5,448		$\mathbf{I}$				
	49		Paved parking, HSG B				
	3,520						
	69,745		Woods, Good, HSG D				
	8,823		Brush, Goo				
	65,131				od, HSG C		
	49,553			od, HSG C			
_	530		•	s cover, Go	od. HSG B		
	12,421			od, HSG B			
4	45,535	73 V	Veighted A	verage			
4	09,723			vious Area			
	35,812	8	3.04% Impe	ervious Area	a		
			·				
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
0.5	35	0.0200	1.18		Sheet Flow,		
					Smooth surfaces n= 0.011 P2= 3.61"		
4.7	255	0.0165	0.90		Shallow Concentrated Flow,		
					Short Grass Pasture Kv= 7.0 fps		
2.0	132	0.0501	1.12		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
0.4	67	0.0313	2.85		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
1.0	89	0.0465	1.51		Shallow Concentrated Flow,		
					Short Grass Pasture Kv= 7.0 fps		
4.3	289	0.0500	1.12		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
2.9	474	0.0106	2.72	13.61	Trap/Vee/Rect Channel Flow,		
					Bot.W=2.00' D=1.00' Z= 3.0 '/' Top.W=8.00'		
					n= 0.040 Winding stream, pools & shoals		
15.8	1,341	Total	·				

#### **Subcatchment 2.1S: Central**



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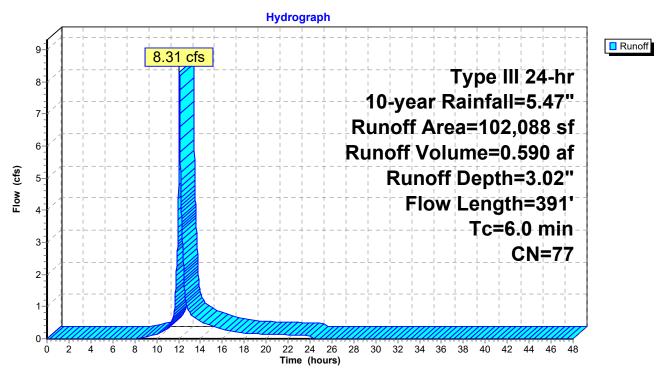
### **Summary for Subcatchment 2.2S: South of SQ Drive**

Runoff = 8.31 cfs @ 12.09 hrs, Volume= 0.590 af, Depth= 3.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN E	<b>Description</b>				
	4,776	98 F	Paved parking, HSG D				
	5,561		Paved parking, HSG C				
	639	80 >	>75% Grass cover, Good, HSG D				
	52,111	77 V	Voods, Go	od, HSG D			
	1,323			,	ood, HSG C		
	37,678	70 V	Voods, Go	od, HSG C			
1	02,088		Veighted A				
	91,751	8	9.87% Per	vious Area			
	10,337	1	0.13% Imp	pervious Ar	ea		
_		01			B		
Tc	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
0.3	19	0.0200	1.05		Sheet Flow,		
					Smooth surfaces n= 0.011 P2= 3.61"		
1.4	118	0.0816	1.43		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
0.7	254	0.0502	5.93	29.63	Trap/Vee/Rect Channel Flow,		
					Bot.W=2.00' D=1.00' Z= 3.0 '/' Top.W=8.00'		
					n= 0.040 Winding stream, pools & shoals		
2.4	391	Total, I	ncreased t	o minimum	Tc = 6.0 min		

## Subcatchment 2.2S: South of SQ Drive



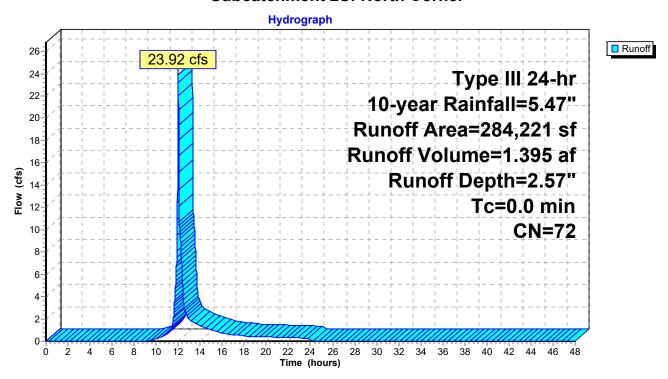
## **Summary for Subcatchment 2S: North Corner**

Runoff = 23.92 cfs @ 12.00 hrs, Volume= 1.395 af, Depth= 2.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

Area (sf)	CN	Description				
27	98	Paved parking, HSG D				
13,324	98	Paved parking, HSG C				
5,932	98	Roofs, HSG C				
254	80	>75% Grass cover, Good, HSG D				
20,767	77	Woods, Good, HSG D				
21,632	74	>75% Grass cover, Good, HSG C				
199,815	70	Woods, Good, HSG C				
22,470	55	Woods, Good, HSG B				
284,221	72	Weighted Average				
264,938		93.22% Pervious Area				
19,283		6.78% Impervious Area				

#### **Subcatchment 2S: North Corner**



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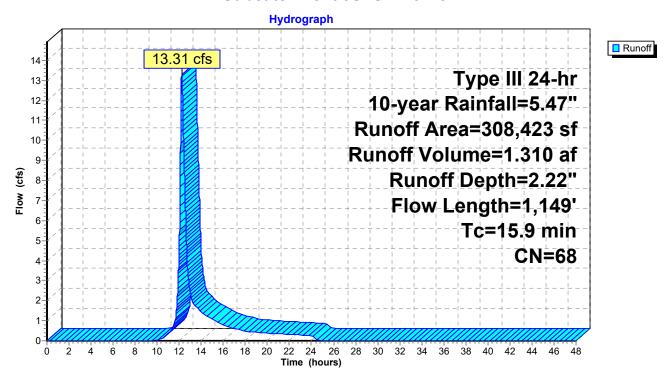
## **Summary for Subcatchment 3S: SE Corner**

Runoff = 13.31 cfs @ 12.23 hrs, Volume= 1.310 af, Depth= 2.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN [	Description		
•	223	98 F	Paved park	ing, HSG D	)
	5,324			ing, HSG C	
	1,176	98 F	Paved park	ing, HSG B	
	14,143	74 >	•75% Gras	s cover, Go	ood, HSG C
2	237,181	70 \	Voods, Go	od, HSG C	
	1,422				ood, HSG B
	48,954	55 \	Voods, Go	od, HSG B	
3	808,423		Veighted A		
3	301,700	-	-	vious Area	
	6,723	2	2.18% Impe	ervious Area	a
_					
Tc	Length	Slope		Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.5	90	0.1412	0.18		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.61"
4.7	331	0.0554	1.18		Shallow Concentrated Flow,
	201	0.0554	0.00	04.40	Woodland Kv= 5.0 fps
0.9	331	0.0554	6.22	31.12	•
					Bot.W=2.00' D=1.00' Z= 3.0 '/' Top.W=8.00'
4.0	207	0.0400	0.00	05.00	n= 0.040 Winding stream, pools & shoals
1.8	397	0.0160	3.63	25.39	•
					Bot.W=4.00' D=1.00' Z= 3.0 '/' Top.W=10.00'
					n= 0.040 Winding stream, pools & shoals
15.9	1,149	Total			

#### **Subcatchment 3S: SE Corner**



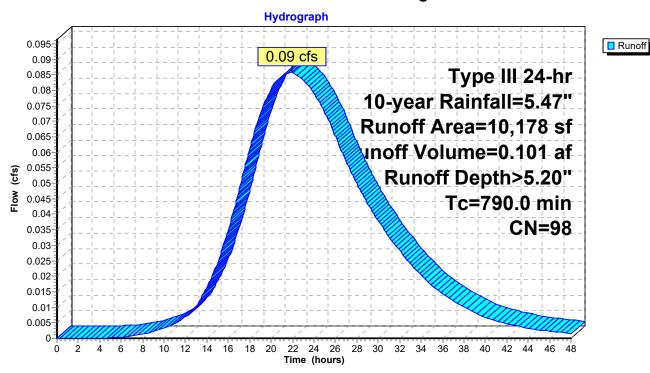
## **Summary for Subcatchment 10S: Parking Lot**

Runoff = 0.09 cfs @ 21.94 hrs, Volume= 0.101 af, Depth> 5.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

Α	rea (sf)	CN	Description							
	10,078	98	Paved roads w/curbs & sewers, HSG C							
	100	74	>75% Gras	>75% Grass cover, Good, HSG C						
	10,178	98	Weighted A	Veighted Average						
	100		0.98% Pervious Area							
	10,078		99.02% Imp	pervious Ar	ea					
Tc	Length (feet)		,	Capacity (cfs)	Description					
'90.0	(1001)	(1010	(1000)	(010)	Direct Entry,					
	Tc (min)	100 10,178 100 10,078 Tc Length (min) (feet)	10,078 98 100 74 10,178 98 100 10,078 Tc Length Slope (min) (feet) (ft/ft)	10,078 98 Paved road 100 74 >75% Gras 10,178 98 Weighted A 100 0.98% Perv 10,078 99.02% Imp  Tc Length Slope Velocity (min) (feet) (ft/ft) (ft/sec)	10,078         98         Paved roads w/curbs & 100         74         >75% Grass cover, Go           10,178         98         Weighted Average 0.98% Pervious Area 10,078         99.02% Impervious Ar           Tc         Length (flower of the control of the contr					

#### **Subcatchment 10S: Parking Lot**



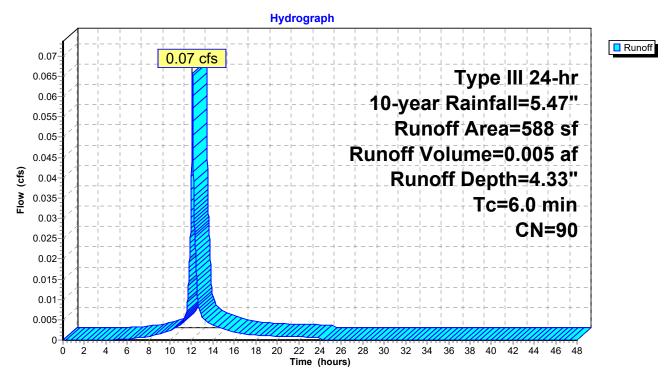
## **Summary for Subcatchment 11S: Island**

Runoff = 0.07 cfs @ 12.08 hrs, Volume= 0.005 af, Depth= 4.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description								
	321	98	Roofs, HSG	Roofs, HSG C							
	66	98	Paved road	s w/curbs &	& sewers, HSG C						
	201	74	>75% Gras	s cover, Go	ood, HSG C						
	588	90	Weighted A	Veighted Average							
	201		34.18% Per	vious Area	a						
	387		65.82% Imp	pervious Ar	rea						
Tc	Length	Slope	Velocity	Capacity	Description						
	-		,		Description						
<u>(min)</u>	(feet)	(ft/ft	(ft/sec)	(cfs)							
6.0					Direct Entry,						

#### **Subcatchment 11S: Island**



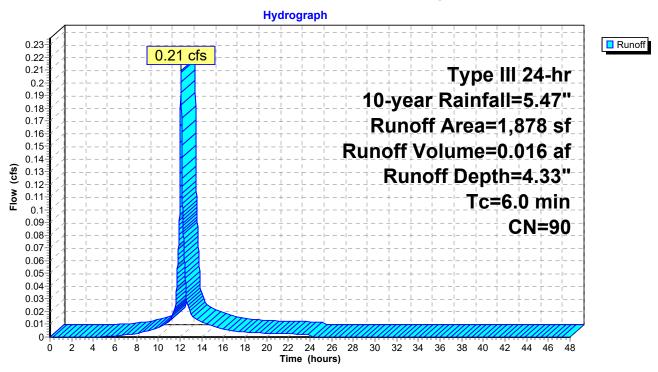
## **Summary for Subcatchment 12S: Building**

Runoff = 0.21 cfs @ 12.08 hrs, Volume= 0.016 af, Depth= 4.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description									
	1,171	98	Roofs, HSG C									
	52	98	Paved road	Paved roads w/curbs & sewers, HSG C								
	655	74	>75% Gras	>75% Grass cover, Good, HSG C								
	1,878	90	Weighted Average									
	655		34.88% Per	vious Area	a							
	1,223		65.12% lmp	ervious Ar	rea							
Tc	Length	Slope	Velocity	Capacity	Description							
(min)	(feet)	(ft/ft)	t) (ft/sec) (cfs)									
6.0					Direct Entry							

# Subcatchment 12S: Building



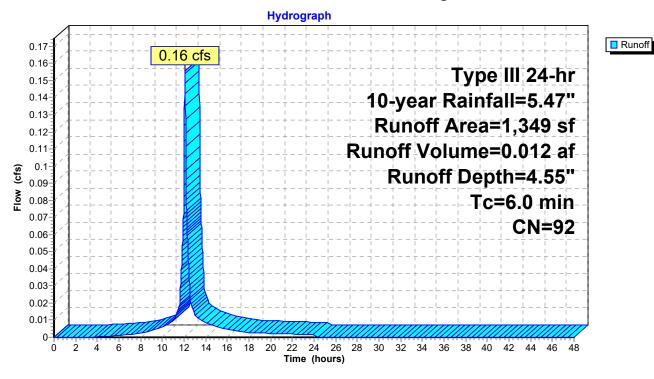
#### **Summary for Subcatchment 13S: Building**

Runoff = 0.16 cfs @ 12.08 hrs, Volume= 0.012 af, Depth= 4.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description							
_		996	98	Roofs, HSG C							
_		353	74	>75% Gras	>75% Grass cover, Good, HSG C						
		1,349	92	Weighted A	Veighted Average						
		353		26.17% Per	rvious Area						
		996		73.83% Imp	pervious Ar	ea					
	То	Longth	Clan	. Valacity	Conneity	Description					
	Tc	Length	Slope	,	Capacity	Description					
	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
_	6.0					Direct Entry					

## **Subcatchment 13S: Building**



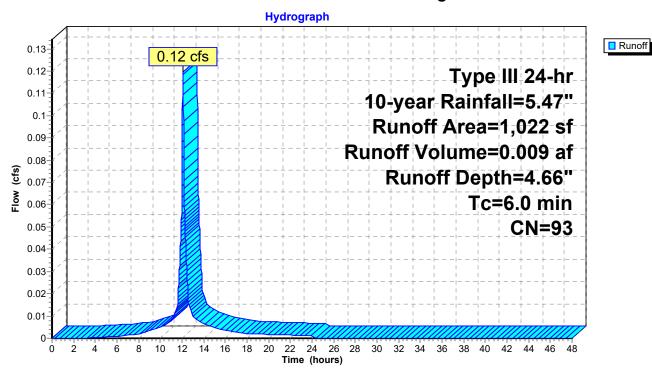
# **Summary for Subcatchment 14S: Building**

Runoff = 0.12 cfs @ 12.08 hrs, Volume= 0.009 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	795	98	Roofs, HSG C							
	227	74	>75% Gras	>75% Grass cover, Good, HSG C						
	1,022	93	Weighted A	Veighted Average						
	227		22.21% Per	22.21% Pervious Area						
	795		77.79% Imp	ervious Are	rea					
Tc	Length	Slope	,	Capacity	·					
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
6.0			Direct Entry,							

#### **Subcatchment 14S: Building**



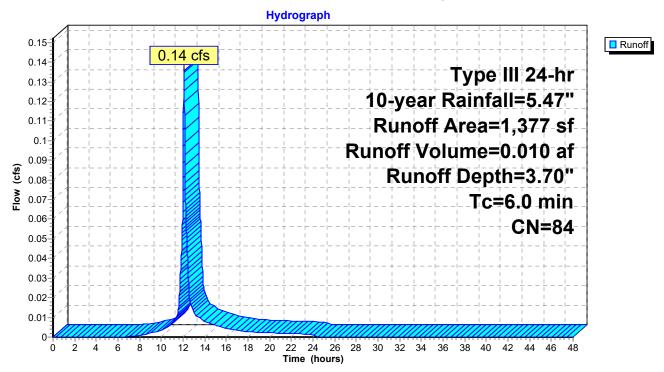
## **Summary for Subcatchment 15S: Building**

Runoff = 0.14 cfs @ 12.09 hrs, Volume= 0.010 af, Depth= 3.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description								
	484	98	Roofs, HSG C								
	111	98	Paved road	s w/curbs &	& sewers, HSG C						
	782	74	>75% Gras	s cover, Go	ood, HSG C						
	1,377	84	Weighted A	Weighted Average							
	782		56.79% Per	vious Area	a						
	595		43.21% Imp	ervious Ar	rea						
_		-									
Tc	Length	Slope	,	Capacity	Description						
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)							
6.0					Direct Entry.						

# Subcatchment 15S: Building



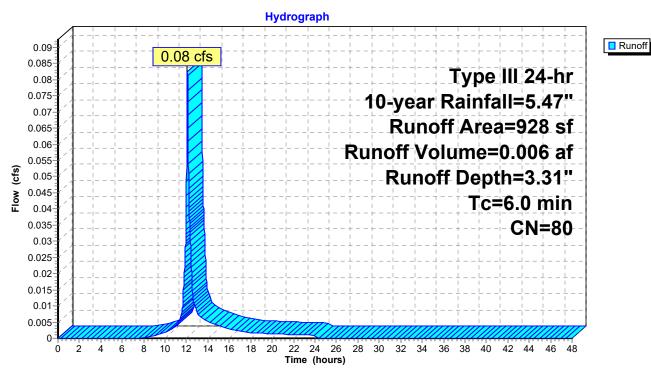
## **Summary for Subcatchment 16S: Island**

Runoff = 0.08 cfs @ 12.09 hrs, Volume= 0.006 af, Depth= 3.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description								
	246	98	Paved road	Paved roads w/curbs & sewers, HSG C							
	682	74	>75% Grass cover, Good, HSG C								
	928	80	Weighted A	/eighted Average							
	682		73.49% Pervious Area								
	246		26.51% Imp	ervious Are	rea						
Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	•						
	(ieet)	(11/11	(11/560)	(015)							
6.0					Direct Entry,						

#### **Subcatchment 16S: Island**



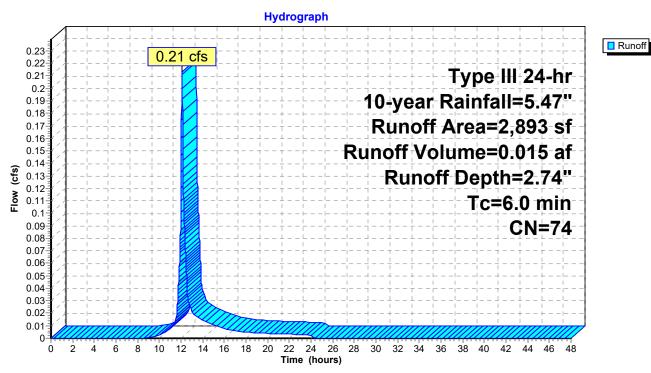
## Summary for Subcatchment 17S: To Bio #1

Runoff = 0.21 cfs @ 12.09 hrs, Volume= 0.015 af, Depth= 2.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Α	rea (sf)	CN	Description	Description								
		8	98	Paved road	Paved roads w/curbs & sewers, HSG C								
		2,885	74	>75% Gras	75% Grass cover, Good, HSG C								
		2,893	74	Weighted A	Veighted Average								
		2,885		99.72% Per	vious Area	a							
		8		0.28% Impe	ervious Area	ea							
	То	Longth	Clan	. Valacity	Consoitu	Description							
	Tc	Length	Slope	,	Capacity	·							
(n	nin)	(feet)	(ft/ft	) (ft/sec) (cfs)									
<u>-</u>	6.0					Direct Entry							

## Subcatchment 17S: To Bio #1



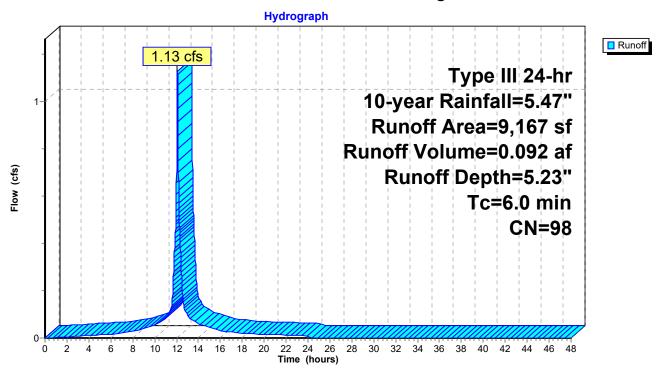
## **Summary for Subcatchment 20S: Building**

Runoff = 1.13 cfs @ 12.08 hrs, Volume= 0.092 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	rea (sf)	CN I	Description						
	9,167	98 F	Roofs, HSG C						
	9,167	•	100.00% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				

#### **Subcatchment 20S: Building**



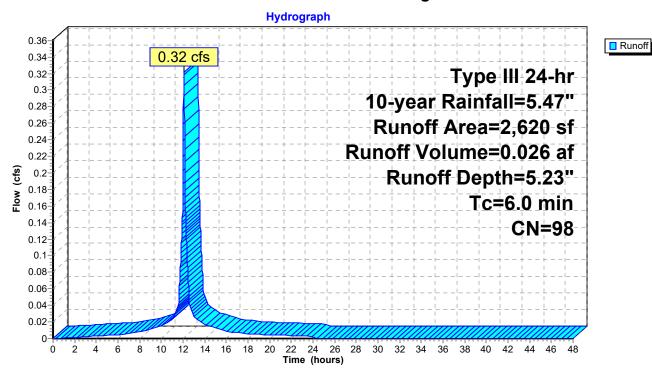
# **Summary for Subcatchment 21S: Parking Lot**

Runoff = 0.32 cfs @ 12.08 hrs, Volume= 0.026 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description	Description								
		331	98	Roofs, HSG	Roofs, HSG C								
		2,289	98	Paved road	Paved roads w/curbs & sewers, HSG C								
		2,620	98		Veighted Average								
		2,620		100.00% Im	npervious A	ırea							
	Тс	Length	Slope	e Velocity	Capacity	Description							
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)								
	6.0					Direct Entry,							

## **Subcatchment 21S: Parking Lot**



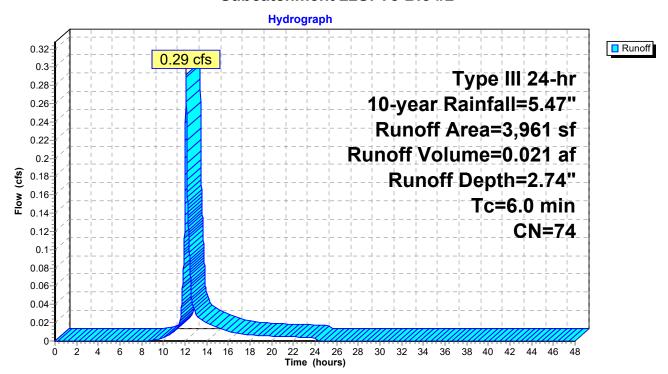
## Summary for Subcatchment 22S: To Bio #2

Runoff = 0.29 cfs @ 12.09 hrs, Volume= 0.021 af, Depth= 2.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	rea (sf)	CN E	Description						
	3,961	74 >	75% Grass cover, Good, HSG C						
	3,961	1	100.00% Pervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•				
6.0					Direct Entry,				

#### Subcatchment 22S: To Bio #2



## **Summary for Subcatchment 30S: Roadside**

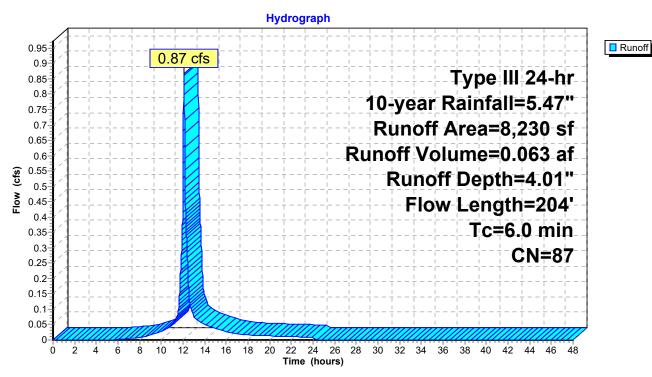
Runoff 0.87 cfs @ 12.09 hrs, Volume= 0.063 af, Depth= 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	rea (sf)	CN D	Description						
	4,370	98 P	aved park	ing, HSG C	;				
	3,860	74 >	>75% Grass cover, Good, HSG C						
	8,230	87 V	Veighted A	verage					
	3,860	4	46.90% Pervious Area						
	4,370	5	3.10% Imp	pervious Are	ea				
_									
Tc	Length	Slope	Velocity	Capacity	Description				
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)					
0.3	19	0.0200	1.05		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.61"				
2.9	185	0.0235	1.07		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
3.2	204	Total, I	Total, Increased to minimum Tc = 6.0 min						

Total, Increased to minimum Tc = 6.0 min

#### Subcatchment 30S: Roadside



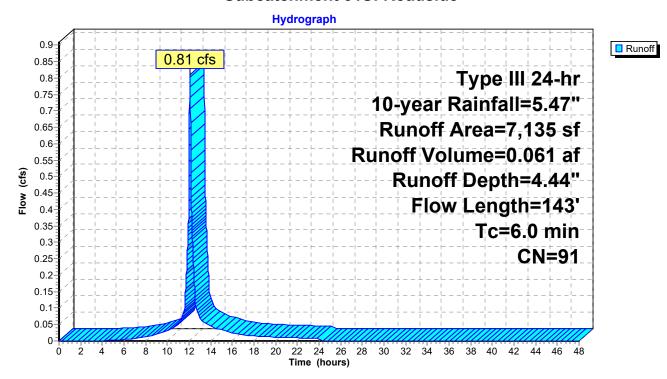
## **Summary for Subcatchment 31S: Roadside**

Runoff = 0.81 cfs @ 12.08 hrs, Volume= 0.061 af, Depth= 4.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Α	rea (sf)	CN Description							
		5,074	98 F	aved park	ing, HSG C					
		2,061	74 >	>75% Grass cover, Good, HSG C						
		7,135	91 V	Veighted A	verage					
		2,061	2	28.89% Pervious Area						
		5,074	7	1.11% Imp	ervious Are	ea				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.3	17	0.0200	1.03		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.61"				
	3.0	126	0.0100	0.70		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	3.3	143	Total, I	ncreased t	o minimum	Tc = 6.0 min				

#### Subcatchment 31S: Roadside



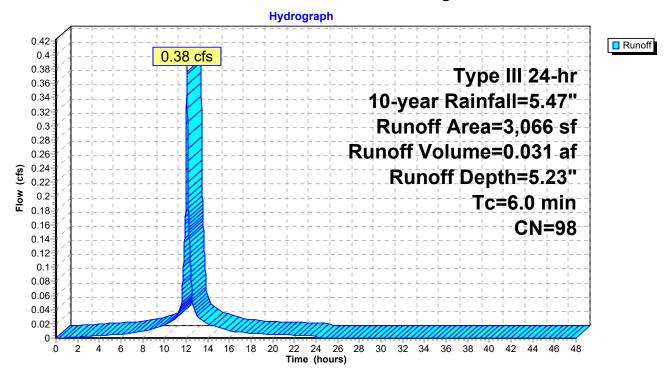
## **Summary for Subcatchment 40S: Building**

Runoff = 0.38 cfs @ 12.08 hrs, Volume= 0.031 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN I	Description						
	3,066	98 F	Roofs, HSG C						
	3,066		100.00% Impervious Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				

#### **Subcatchment 40S: Building**



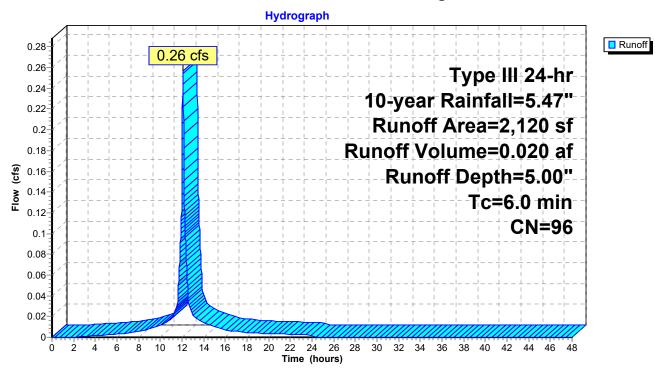
# **Summary for Subcatchment 41S: Building**

Runoff = 0.26 cfs @ 12.08 hrs, Volume= 0.020 af, Depth= 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Area (sf)	CN	Description						
	1,928	98	Roofs, HSG C						
	192	74	>75% Grass cover, Good, HSG C						
	2,120	96	Weighted Average						
	192		9.06% Pervious Area						
	1,928		90.94% lmp	pervious Ar	ea				
_									
To	9	Slope	,	Capacity	Description				
(min	) (feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0	)				Direct Entry				

## **Subcatchment 41S: Building**



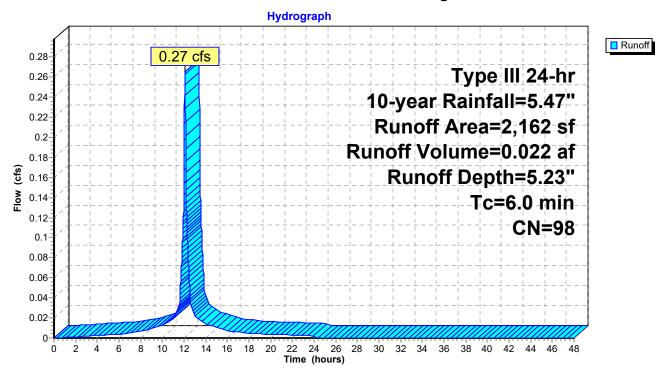
# **Summary for Subcatchment 42S: Building**

Runoff = 0.27 cfs @ 12.08 hrs, Volume= 0.022 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Area (sf)	CN I	Description						
	2,162	98 F	Roofs, HSG C						
	2,162		100.00% Impervious Area						
Tc	9	•	,		Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0					Direct Entry,				

#### **Subcatchment 42S: Building**



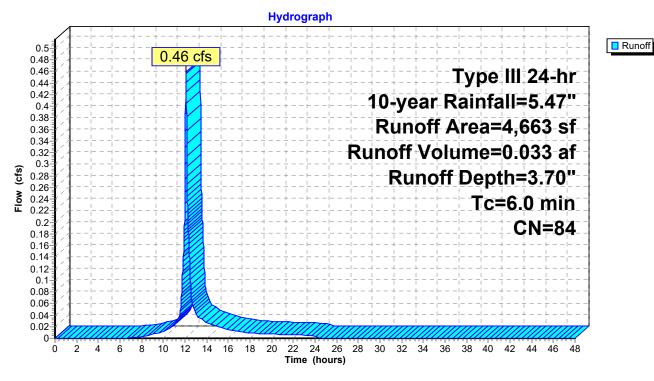
## **Summary for Subcatchment 44S: Roadside**

Runoff = 0.46 cfs @ 12.09 hrs, Volume= 0.033 af, Depth= 3.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description							
		1,908	98	Paved parking, HSG C							
_		2,755	74	>75% Grass cover, Good, HSG C							
		4,663	84	Weighted Average							
		2,755		59.08% Pervious Area							
		1,908		40.92% Imp	pervious Ar	ea					
	_										
	Tc	Length	Slope	,	Capacity	Description					
_	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)			_			
	6.0					Direct Entry					

#### **Subcatchment 44S: Roadside**



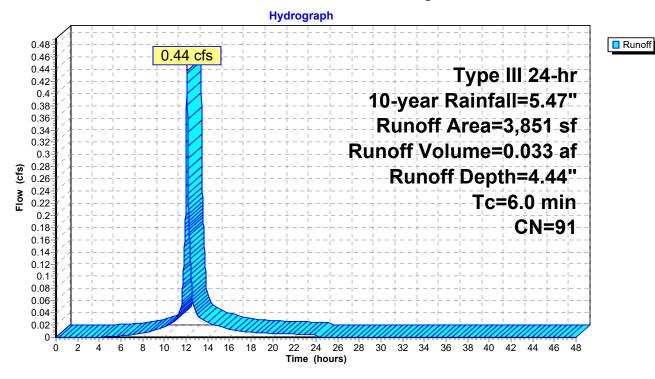
## **Summary for Subcatchment 45S: Parking Lot**

Runoff = 0.44 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 4.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	2,768	98	Paved parking, HSG C							
	1,083	74	>75% Grass cover, Good, HSG C							
	3,851	91	Weighted Average							
	1,083		28.12% Pervious Area							
	2,768		71.88% Impervious Area							
Tc (min)	Length (feet)	Slope (ft/ft	,	Capacity (cfs)	•					
6.0	, ,	•	, ,	, ,	Direct Entry,					

## **Subcatchment 45S: Parking Lot**



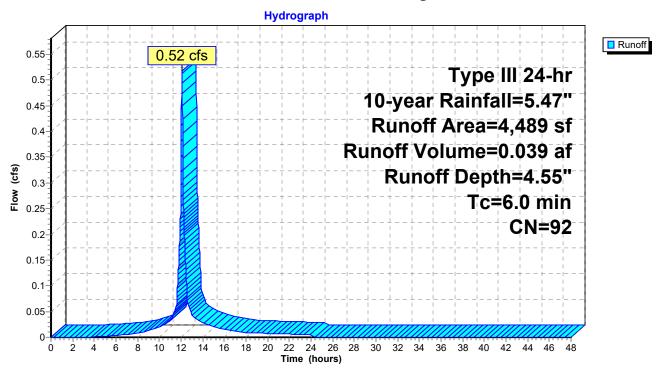
# **Summary for Subcatchment 46S: Parking Lot**

Runoff = 0.52 cfs @ 12.08 hrs, Volume= 0.039 af, Depth= 4.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	rea (sf)	CN	Description							
	3,288	98	Paved parking, HSG C							
	1,201	74	>75% Grass cover, Good, HSG C							
	4,489	92	Weighted Average							
	1,201		26.75% Pervious Area							
	3,288		73.25% Impervious Area							
_										
Tc	Length	Slope	,	Capacity	Description					
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)						
6.0			·	·	Direct Entry	·				

## **Subcatchment 46S: Parking Lot**



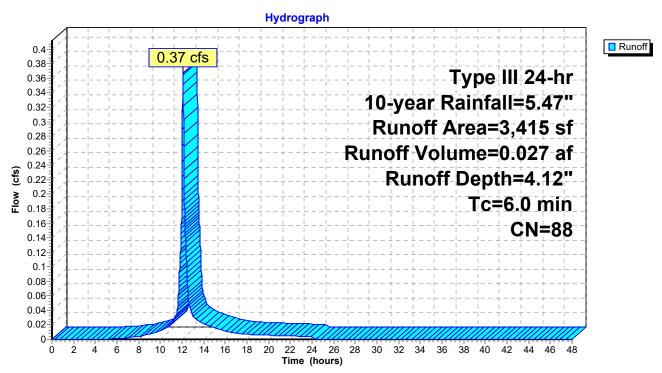
## **Summary for Subcatchment 48S: Roadside**

Runoff = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af, Depth= 4.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	245	98	Paved parking, HSG D							
	1,051	98	Paved parki	ng, HSG C	•					
	605	98	Roofs, HSG	Č						
	229	80	>75% Grass cover, Good, HSG D							
	1,268	74	>75% Grass	>75% Grass cover, Good, HSG C						
	17	61	>75% Grass cover, Good, HSG B							
	3,415	88	Weighted Average							
	1,514		44.33% Per	vious Area						
	1,901		55.67% Imp	ervious Are	ea					
Тс	Length	Slop	e Velocity	Capacity	Description					
(min)	(feet)	(ft/fi	(ft/sec)	(cfs)						
6.0					Direct Entry,					

#### **Subcatchment 48S: Roadside**



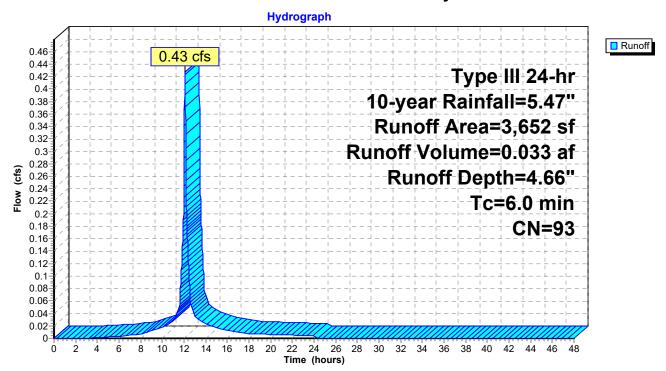
## **Summary for Subcatchment 49S: Driveway**

Runoff = 0.43 cfs @ 12.08 hrs, Volume= 0.033 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	700	98	Paved parking, HSG D							
	1,047	98	Paved park	ng, HSG C	,					
	1,317	98	Paved park	ng, HSG B	}					
	4	80	>75% Grass cover, Good, HSG D							
	174	74	>75% Grass	>75% Grass cover, Good, HSG C						
	410	61	>75% Grass cover, Good, HSG B							
	3,652	93	Weighted Average							
	588		16.10% Per	vious Area						
	3,064		83.90% Imp	ervious Ar	ea					
Tc	Length	Slope	e Velocity	Capacity	Description					
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
6.0					Direct Entry,					

## **Subcatchment 49S: Driveway**



## **Summary for Subcatchment 60S: Parking Lot**

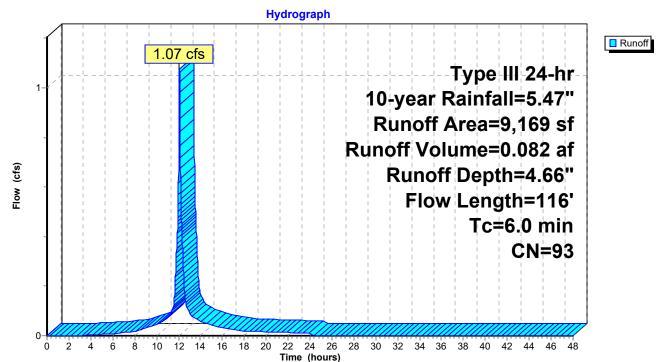
Runoff = 1.07 cfs @ 12.08 hrs, Volume= 0.082 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN [	Description							
	7,169	98 F	Paved parking, HSG C							
	1,516	74 >	75% Grass cover, Good, HSG C							
	484	70 V	Voods, Go	Voods, Good, HSG C						
•	9,169	93 V	/eighted Average							
	2,000			1.81% Pervious Area						
	7,169	7	78.19% Impervious Area							
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·					
0.4	24	0.0200	1.10		Sheet Flow,					
					Smooth surfaces n= 0.011 P2= 3.61"					
8.0	92	0.0100	2.03		Shallow Concentrated Flow,					
					Paved Kv= 20.3 fps					
	440	<b>-</b>								

1.2 116 Total, Increased to minimum Tc = 6.0 min

# **Subcatchment 60S: Parking Lot**



## **Summary for Subcatchment 61S: Parking Lot**

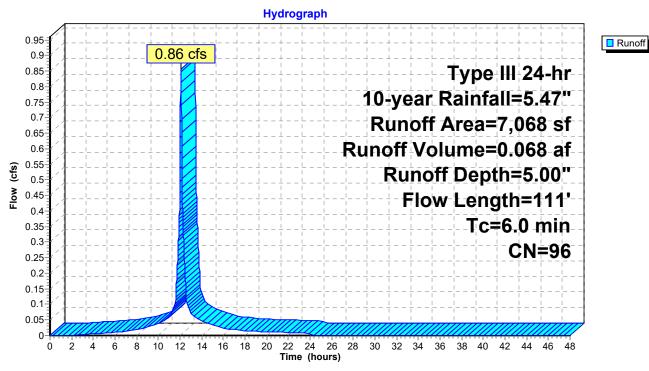
Runoff = 0.86 cfs @ 12.08 hrs, Volume= 0.068 af, Depth= 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Area (sf)	CN [	Description							
	4,574	98 F	Paved parking, HSG C							
	1,927	98 F	Paved park	ing, HSG B						
	335	74 >	75% Gras	s cover, Go	ood, HSG C					
	232	61 >	75% Gras	s cover, Go	ood, HSG B					
	7,068	96 V	Veighted A	verage						
	567	8	3.02% Perv	ious Area						
	6,501	ç	1.98% Imp	pervious Are	ea					
			_							
T	c Length	Slope	Velocity	Capacity	Description					
(min	) (feet)	(ft/ft)	(ft/sec)	(cfs)	·					
0.4	4 24	0.0200	1.10		Sheet Flow,					
					Smooth surfaces n= 0.011 P2= 3.61"					
0.	7 87	0.0100	2.03		Shallow Concentrated Flow,					
					Paved Kv= 20.3 fps					
	1 111	Total	personed t	a minimum	To = 6.0 min					

1.1 Total, Increased to minimum Tc = 6.0 min

# **Subcatchment 61S: Parking Lot**



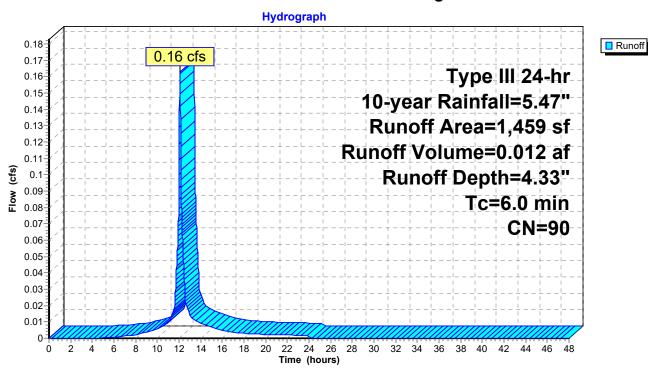
## **Summary for Subcatchment 63S: Building**

Runoff = 0.16 cfs @ 12.08 hrs, Volume= 0.012 af, Depth= 4.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	956	98	Roofs, HSG C							
	503	74	>75% Grass cover, Good, HSG C							
	1,459	90	Weighted A	Weighted Average						
	503		34.48% Per	vious Area	a					
	956		65.52% Imp	ervious Are	rea					
Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft	t) (ft/sec) (cfs)							
6.0					Direct Entry,					

#### **Subcatchment 63S: Building**



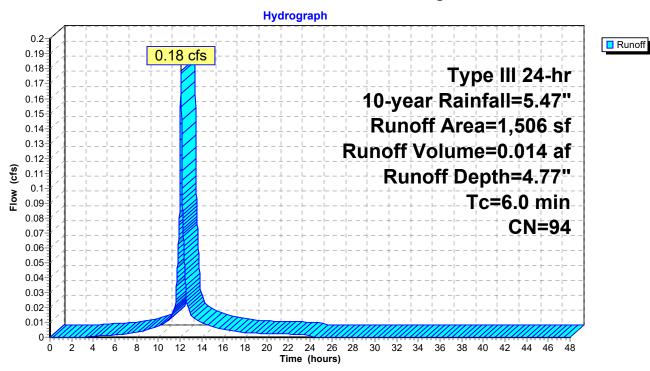
## **Summary for Subcatchment 64S: Building**

Runoff = 0.18 cfs @ 12.08 hrs, Volume= 0.014 af, Depth= 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description							
_		1,224	98	Roofs, HSG C							
_		282	74	>75% Gras	>75% Grass cover, Good, HSG C						
		1,506	94	Weighted A	Weighted Average						
		282		18.73% Per	vious Area						
		1,224		81.27% Imp	pervious Ar	ea					
	т.	1 41.	01		0	D					
	Tc	Length	Slope	e Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
_	6.0					Direct Entry					

## **Subcatchment 64S: Building**



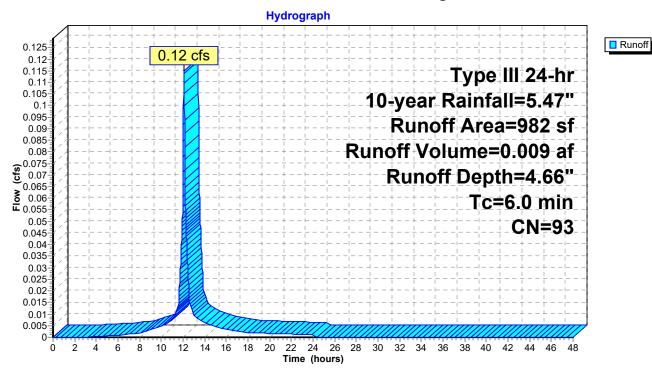
## **Summary for Subcatchment 65S: Building**

Runoff = 0.12 cfs @ 12.08 hrs, Volume= 0.009 af, Depth= 4.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description							
		794	98	Roofs, HSG C							
_		188	74	>75% Gras	>75% Grass cover, Good, HSG C						
		982	93	Weighted A	Weighted Average						
		188		19.14% Per	vious Area						
		794		80.86% Imp	ervious Ar	ea					
	т.	1 41-	Cl		Oit.	Danamination					
	Tc	Length	Slope	,	Capacity	Description					
	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
	6.0					Direct Entry					

## **Subcatchment 65S: Building**



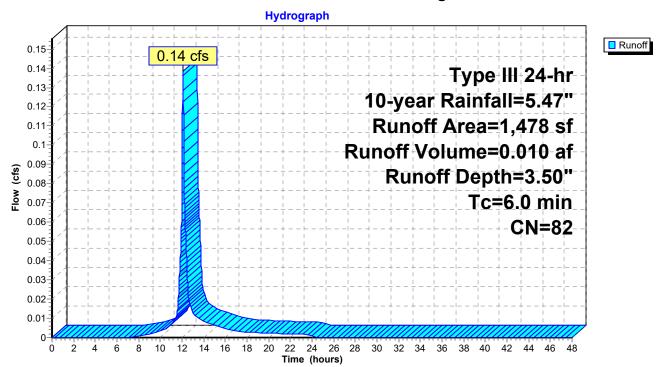
## **Summary for Subcatchment 66S: Building**

Runoff = 0.14 cfs @ 12.09 hrs, Volume= 0.010 af, Depth= 3.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	25	98	Paved parking, HSG C							
	161	98	Roofs, HSG	i Č						
	476	98	Roofs, HSG	В						
	486	74	>75% Gras	s cover, Go	ood, HSG C					
	330	61	>75% Gras	s cover, Go	ood, HSG B					
	1,478	82	Weighted A	verage						
	816		55.21% Per	vious Area						
	662		44.79% Imp	ervious Ar	ea					
Tc	Length	Slope	e Velocity	Capacity	Description					
(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
6.0					Direct Entry,					

## **Subcatchment 66S: Building**



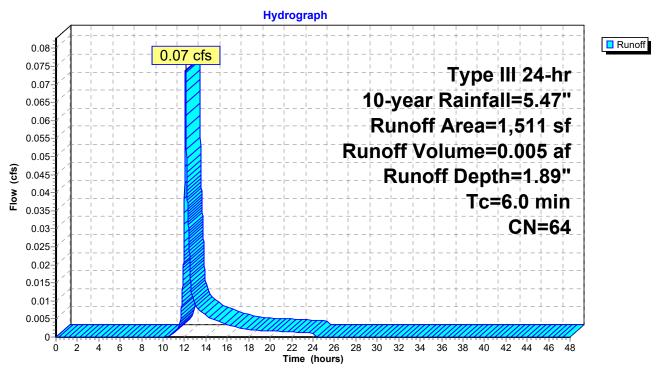
## **Summary for Subcatchment 67S: Landscape**

Runoff = 0.07 cfs @ 12.09 hrs, Volume= 0.005 af, Depth= 1.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	156	98	Paved parking, HSG B							
	1,168	61	>75% Gras	s cover, Go	ood, HSG B					
	187	55	Woods, Go	od, HSG B						
	1,511	64	Weighted Average							
	1,355		89.68% Per	vious Area						
	156		10.32% Imp	ervious Ar	ea					
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)						
6.0					Direct Entry.					

# Subcatchment 67S: Landscape



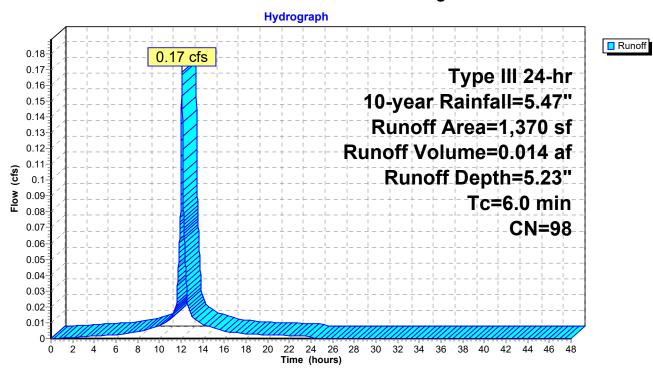
## **Summary for Subcatchment 68S: Building**

Runoff = 0.17 cfs @ 12.08 hrs, Volume= 0.014 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Α	rea (sf)	CN	Description						
		424	98	Roofs, HSG C						
		946	98	Roofs, HSC	B					
		1,370	98	Weighted A	Veighted Average					
		1,370		100.00% In	npervious A	Area .				
	Тс	Length	Slop	e Velocity	Capacity	Description				
(	min)	(feet)	(ft/f	(ft/sec)	(cfs)					
	6.0					Direct Entry,				

## **Subcatchment 68S: Building**



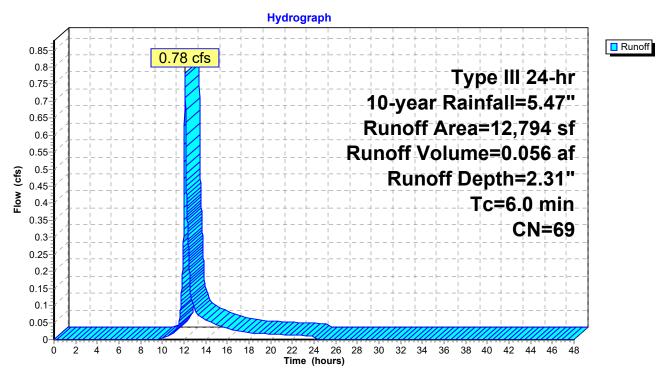
## **Summary for Subcatchment 69S: To Pond**

Runoff = 0.78 cfs @ 12.09 hrs, Volume= 0.056 af, Depth= 2.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Aı	rea (sf)	CN	Description							
		7,562	74	>75% Grass cover, Good, HSG C							
_		5,232	61	>75% Gras	s cover, Go	ood, HSG B					
	12,794 69 Weighted Average										
		12,794		100.00% Pe	ervious Are	а					
	Tc	Length	Slope	,	Capacity	Description					
_	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)						
	6.0					Direct Entry					

#### **Subcatchment 69S: To Pond**



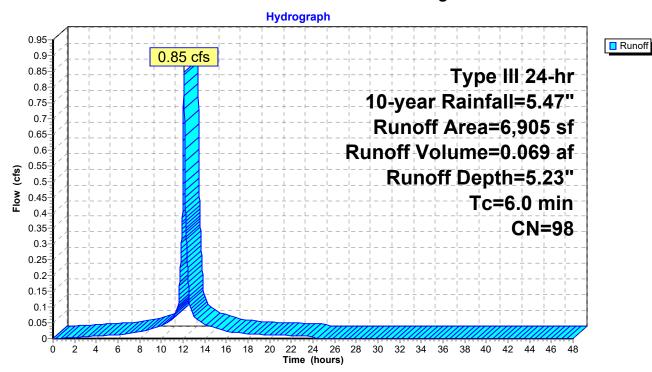
## **Summary for Subcatchment 70S: Building**

Runoff = 0.85 cfs @ 12.08 hrs, Volume= 0.069 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description							
		6,802	98	Roofs, HSG C							
_		103	98	Roofs, HSG	Roofs, HSG B						
		6,905	98	Weighted A	Weighted Average						
		6,905		100.00% Im	pervious A	rea					
	Тс	Length	Slop	,	Capacity	Description					
_	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)						
	6.0					Direct Entry					

## **Subcatchment 70S: Building**



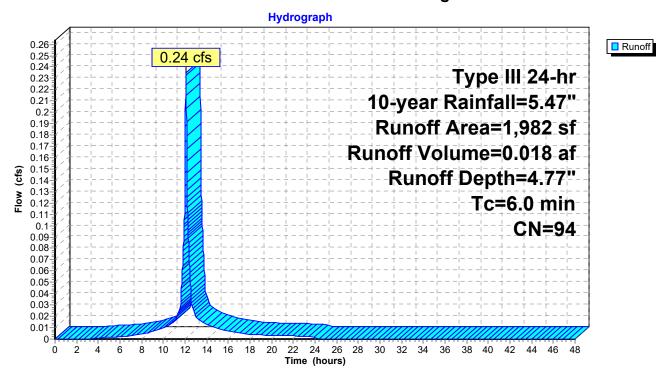
## **Summary for Subcatchment 80S: Building**

Runoff = 0.24 cfs @ 12.08 hrs, Volume= 0.018 af, Depth= 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

A	rea (sf)	CN	Description							
	1,200	98	Roofs, HSG C							
	476	98	Paved park	ing, HSG C	;					
	306	74	>75% Gras	s cover, Go	ood, HSG C					
	1,982	94	Weighted Average							
	306		15.44% Per	vious Area						
	1,676		84.56% lmp	ervious Ar	ea					
Тс	Length	Slope	•	Capacity	Description					
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)						
6.0					Direct Entry,					

# Subcatchment 80S: Building



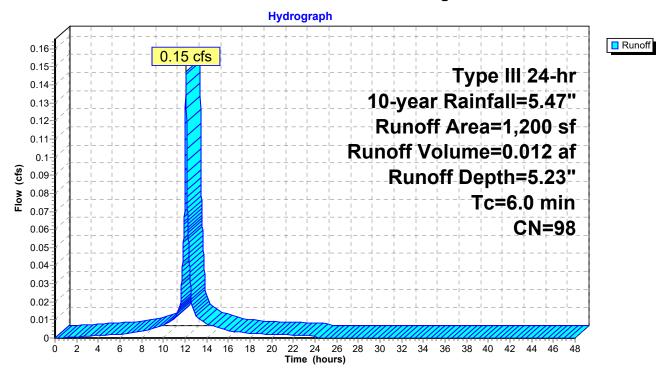
## **Summary for Subcatchment 81S: Building**

Runoff = 0.15 cfs @ 12.08 hrs, Volume= 0.012 af, Depth= 5.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	rea (sf)	CN I	Description				
	1,200	98 I	Roofs, HSG C				
	1,200		100.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

## **Subcatchment 81S: Building**



## **Summary for Subcatchment 82S: Parking Lot**

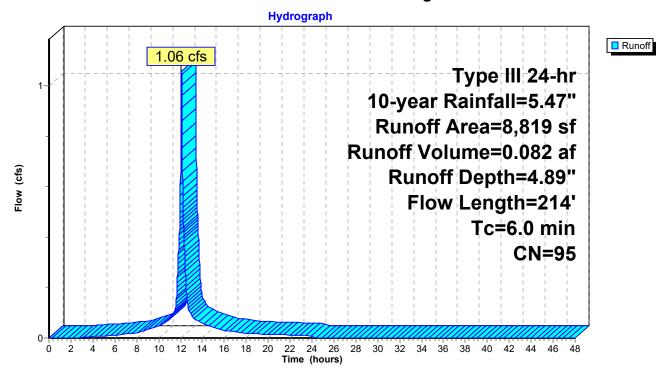
Runoff = 1.06 cfs @ 12.08 hrs, Volume= 0.082 af, Depth= 4.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

	Α	rea (sf)	CN	Description					
		7,436	98	Paved park	ing, HSG C				
		460	98	Paved park	ing, HSG B	3			
		303	74			ood, HSG C			
		620	61	>75% Gras	s cover, Go	ood, HSG B			
		8,819	95	95 Weighted Average					
		923		10.47% Per	rvious Area				
		7,896		89.53% Imp	pervious Ar	ea			
	Tc	Length	Slop	e Velocity	Capacity	Description			
_	(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)				
	2.2	29	0.063	1 0.22		Sheet Flow,			
						Grass: Short n= 0.150 P2= 3.61"			
	0.4	95	0.040	0 4.06		Shallow Concentrated Flow,			
						Paved Kv= 20.3 fps			
	0.7	90	0.010	0 2.03		Shallow Concentrated Flow,			
_						Paved Kv= 20.3 fps			
	3 3	21/	Total	Increased t	o minimum	To = 6.0 min			

#### 3.3 214 Total, Increased to minimum Tc = 6.0 min

## **Subcatchment 82S: Parking Lot**



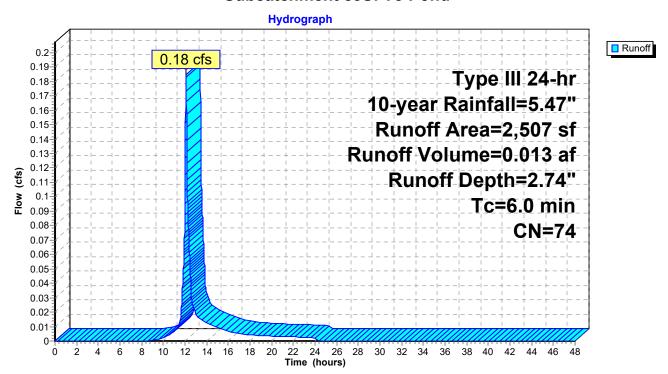
## **Summary for Subcatchment 83S: To Pond**

Runoff = 0.18 cfs @ 12.09 hrs, Volume= 0.013 af, Depth= 2.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-year Rainfall=5.47"

_	Α	rea (sf)	CN	Description						
		2,507	74	>75% Gras	75% Grass cover, Good, HSG C					
		2,507		100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•				
	6.0					Direct Entry,				

#### **Subcatchment 83S: To Pond**



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## **Summary for Reach 2.1R: Wetland Flow Path**

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 18.63 cfs @ 12.05 hrs, Volume= 1.395 af

Outflow = 16.73 cfs @ 12.09 hrs, Volume= 1.395 af, Atten= 10%, Lag= 2.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 2.53 fps, Min. Travel Time= 2.3 min Avg. Velocity = 0.72 fps, Avg. Travel Time= 7.9 min

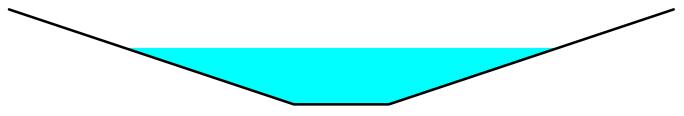
Peak Storage= 2,278 cf @ 12.09 hrs Average Depth at Peak Storage= 1.19' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 54.59 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

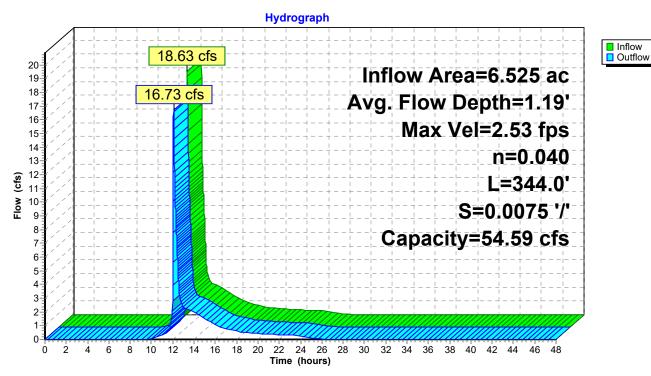
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 344.0' Slope= 0.0075 '/'

Inlet Invert= 52.58', Outlet Invert= 50.00'



Reach 2.1R: Wetland Flow Path



Inflow
Outflow

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## **Summary for Reach 2.2R: Wetland Flow Path**

Inflow Area = 17.467 ac, 10.03% Impervious, Inflow Depth > 2.69" for 10-year event

Inflow = 19.20 cfs @ 12.50 hrs, Volume= 3.919 af

Outflow = 18.90 cfs @ 12.48 hrs, Volume= 3.919 af, Atten= 2%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 5.27 fps, Min. Travel Time= 0.8 min Avg. Velocity = 1.34 fps, Avg. Travel Time= 3.3 min

Peak Storage= 944 cf @ 12.48 hrs Average Depth at Peak Storage= 0.81

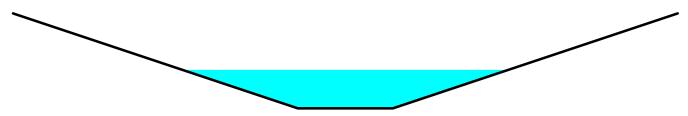
Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 141.18 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

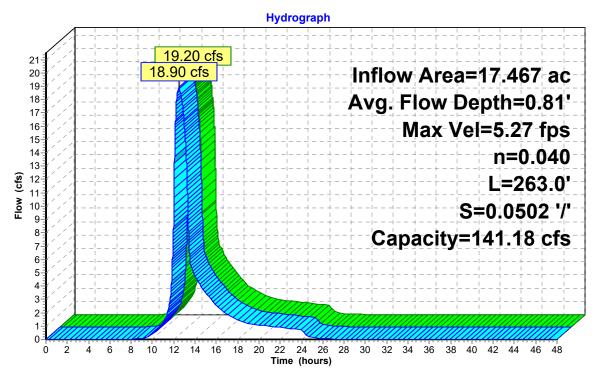
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 263.0' Slope= 0.0502 '/'

Inlet Invert= 46.52', Outlet Invert= 33.33'



Reach 2.2R: Wetland Flow Path



Inflow
Outflow

### 5440-Post

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## **Summary for Reach 2R: Wetland Flow Path**

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 18.70 cfs @ 12.05 hrs, Volume= 1.395 af

Outflow = 18.63 cfs @ 12.05 hrs, Volume= 1.395 af, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 5.02 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.45 fps, Avg. Travel Time= 1.7 min

Peak Storage= 560 cf @ 12.05 hrs Average Depth at Peak Storage= 0.83'

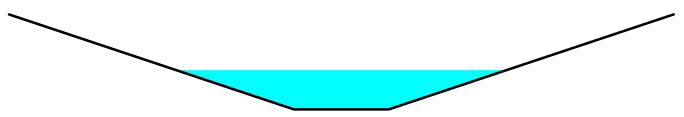
Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 133.09 cfs

2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

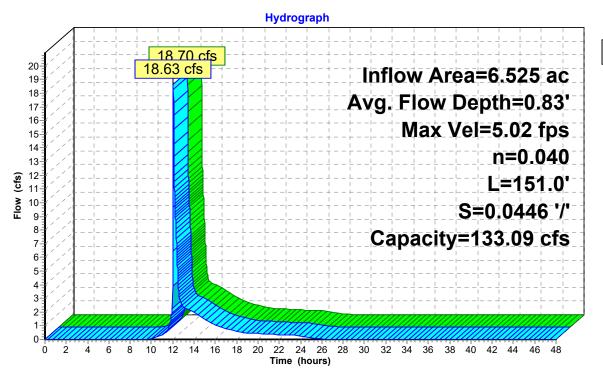
Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 151.0' Slope= 0.0446 '/'

Inlet Invert= 59.31', Outlet Invert= 52.58'



#### Reach 2R: Wetland Flow Path



## **Summary for Reach 10R: Swale**

Inflow Area = 0.230 ac, 42.35% Impervious, Inflow Depth > 3.73" for 10-year event

Inflow = 0.30 cfs @ 12.42 hrs, Volume= 0.072 af

Outflow = 0.30 cfs @ 12.43 hrs, Volume= 0.072 af, Atten= 0%, Lag= 0.7 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 0.64 fps, Min. Travel Time= 1.1 min Avg. Velocity = 0.20 fps, Avg. Travel Time= 3.7 min

Peak Storage= 20 cf @ 12.43 hrs Average Depth at Peak Storage= 0.11'

Bank-Full Depth= 1.00' Flow Area= 7.0 sf, Capacity= 16.22 cfs

4.00' x 1.00' deep channel, n= 0.035 Earth, dense weeds

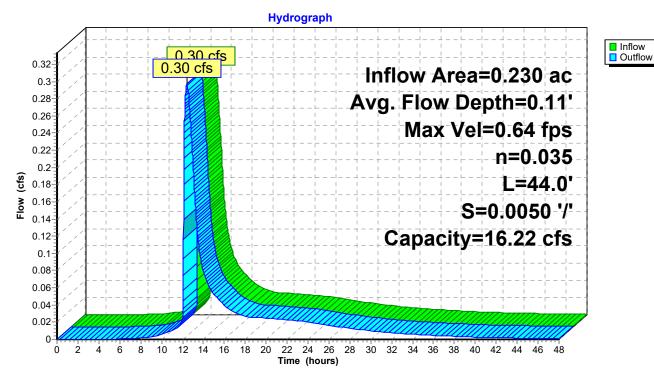
Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 44.0' Slope= 0.0050 '/'

Inlet Invert= 53.60', Outlet Invert= 53.38'



#### Reach 10R: Swale



## Summary for Reach 22R: Wetland Flow Path

Inflow Area = 0.362 ac, 74.85% Impervious, Inflow Depth > 4.56" for 10-year event

Inflow = 0.44 cfs @ 12.46 hrs, Volume= 0.137 af

Outflow = 0.44 cfs @ 12.51 hrs, Volume= 0.137 af, Atten= 0%, Lag= 3.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 0.80 fps, Min. Travel Time= 4.4 min Avg. Velocity = 0.44 fps, Avg. Travel Time= 8.0 min

Peak Storage= 116 cf @ 12.51 hrs Average Depth at Peak Storage= 0.05'

Bank-Full Depth= 2.00' Flow Area= 60.0 sf, Capacity= 392.58 cfs

10.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals

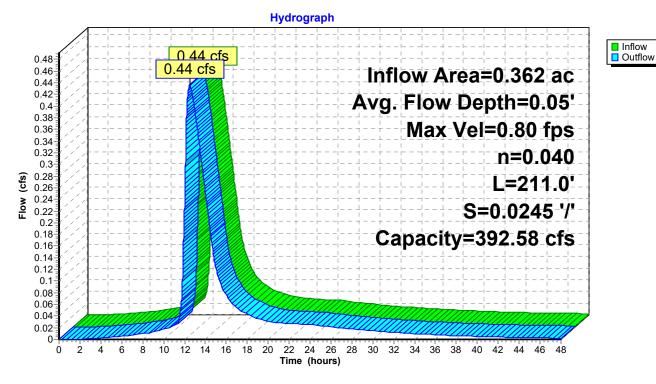
Side Slope Z-value= 10.0 '/' Top Width= 50.00'

Length= 211.0' Slope= 0.0245 '/'

Inlet Invert= 55.16', Outlet Invert= 50.00'



### Reach 22R: Wetland Flow Path



Inflow
Outflow

### 5440-Post

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## Summary for Reach 23R: Wetland Flow Path

Inflow Area = 6.886 ac, 10.36% Impervious, Inflow Depth > 2.67" for 10-year event

Inflow = 17.02 cfs @ 12.09 hrs, Volume= 1.532 af

Outflow = 16.92 cfs @ 12.10 hrs, Volume= 1.532 af, Atten= 1%, Lag= 0.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

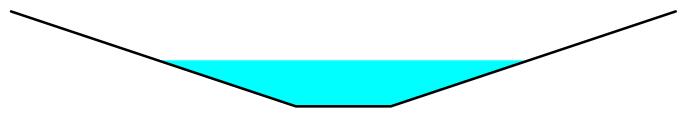
Max. Velocity= 3.54 fps, Min. Travel Time= 0.6 min Avg. Velocity = 0.74 fps, Avg. Travel Time= 2.9 min

Peak Storage= 625 cf @ 12.10 hrs Average Depth at Peak Storage= 0.97' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 85.86 cfs

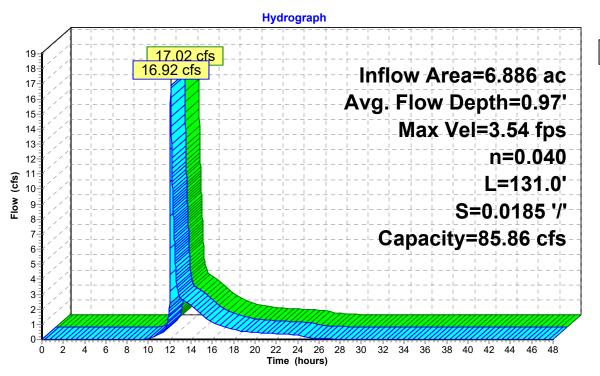
2.00' x 2.00' deep channel, n= 0.040 Winding stream, pools & shoals Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 131.0' Slope= 0.0185 '/'

Inlet Invert= 50.00', Outlet Invert= 47.57'



### Reach 23R: Wetland Flow Path



## **Summary for Reach 69R: Swale**

Inflow Area = 1.645 ac, 63.94% Impervious, Inflow Depth > 4.03" for 10-year event

Inflow = 2.47 cfs @ 12.38 hrs, Volume= 0.552 af

Outflow = 2.47 cfs (a) 12.38 hrs, Volume= 0.552 af, Atten= 0%, Lag= 0.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 1.21 fps, Min. Travel Time= 0.2 min Avg. Velocity = 0.34 fps, Avg. Travel Time= 0.8 min

Peak Storage= 35 cf @ 12.38 hrs Average Depth at Peak Storage= 0.39'

Bank-Full Depth= 1.00' Flow Area= 7.0 sf, Capacity= 14.11 cfs

4.00' x 1.00' deep channel, n= 0.069 Riprap, 6-inch

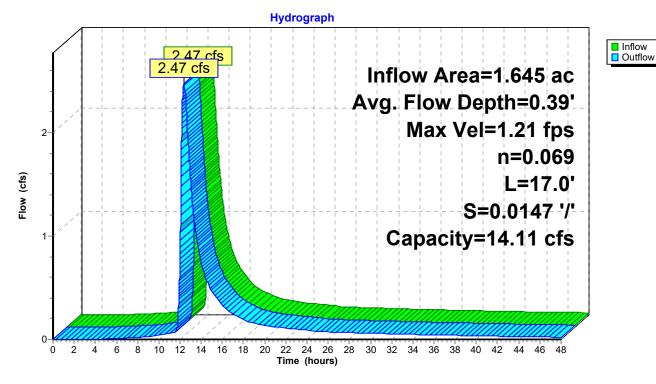
Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 17.0' Slope= 0.0147 '/'

Inlet Invert= 45.25', Outlet Invert= 45.00'



### Reach 69R: Swale



Inflow
Outflow

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## Summary for Reach 70R: Woodland Flow Path

Inflow Area = 1.645 ac, 63.94% Impervious, Inflow Depth > 4.03" for 10-year event

Inflow = 2.47 cfs @ 12.38 hrs, Volume= 0.552 af

Outflow = 2.47 cfs (a) 12.40 hrs, Volume= 0.552 af, Atten= 0%, Lag= 1.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 0.57 fps, Min. Travel Time= 1.7 min Avg. Velocity = 0.16 fps, Avg. Travel Time= 5.8 min

Peak Storage= 247 cf @ 12.40 hrs Average Depth at Peak Storage= 0.33'

Bank-Full Depth= 1.00' Flow Area= 20.0 sf, Capacity= 21.20 cfs

10.00' x 1.00' deep channel, n= 0.400 Sheet flow: Woods+light brush

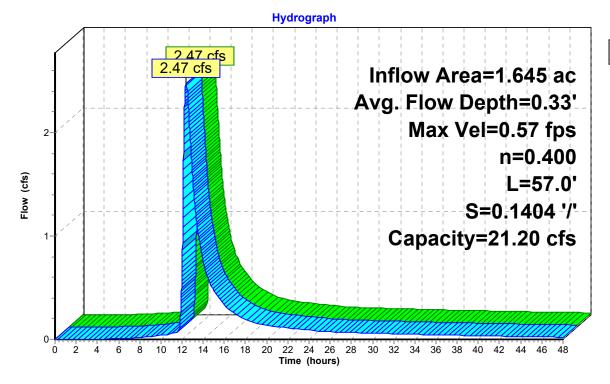
Side Slope Z-value= 10.0 '/' Top Width= 30.00'

Length= 57.0' Slope= 0.1404 '/'

Inlet Invert= 45.00', Outlet Invert= 37.00'



### Reach 70R: Woodland Flow Path



## **Summary for Reach 71R: Stream**

Inflow Area = 1.645 ac, 63.94% Impervious, Inflow Depth > 4.03" for 10-year event

Inflow = 2.47 cfs @ 12.40 hrs, Volume= 0.552 af

Outflow = 2.47 cfs (a) 12.41 hrs, Volume= 0.552 af, Atten= 0%, Lag= 0.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 3.10 fps, Min. Travel Time= 0.4 min Avg. Velocity = 0.93 fps, Avg. Travel Time= 1.4 min

Peak Storage= 64 cf @ 12.41 hrs Average Depth at Peak Storage= 0.28'

Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 31.12 cfs

2.00' x 1.00' deep channel, n= 0.040 Winding stream, pools & shoals

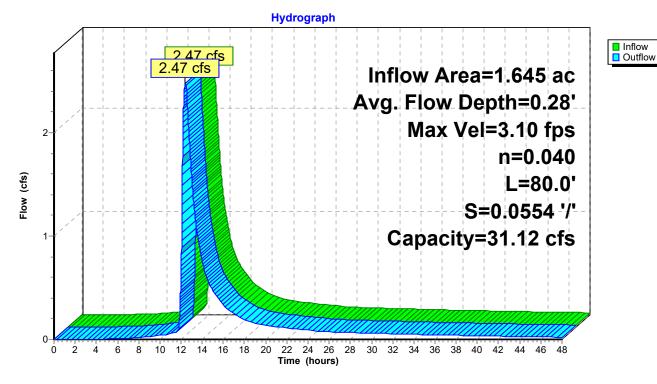
Side Slope Z-value= 3.0 '/' Top Width= 8.00'

Length= 80.0' Slope= 0.0554 '/'

Inlet Invert= 37.00', Outlet Invert= 32.57'



### Reach 71R: Stream



Inflow
Outflow

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## Summary for Reach 72R: Stream

Inflow Area = 1.645 ac, 63.94% Impervious, Inflow Depth > 4.03" for 10-year event

Inflow = 2.47 cfs @ 12.41 hrs, Volume= 0.552 af

Outflow = 2.47 cfs (a) 12.42 hrs, Volume= 0.552 af, Atten= 0%, Lag= 0.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 1.80 fps, Min. Travel Time= 0.8 min Avg. Velocity = 0.50 fps, Avg. Travel Time= 2.9 min

Peak Storage= 121 cf @ 12.42 hrs Average Depth at Peak Storage= 0.28'

Bank-Full Depth= 1.00' Flow Area= 7.0 sf, Capacity= 25.40 cfs

4.00' x 1.00' deep channel, n= 0.040 Winding stream, pools & shoals

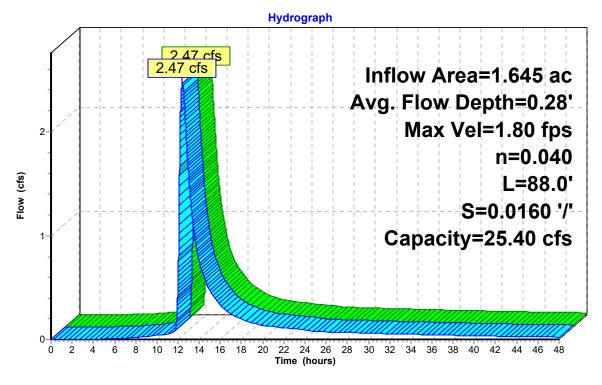
Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 88.0' Slope= 0.0160 '/'

Inlet Invert= 32.57', Outlet Invert= 31.16'



#### Reach 72R: Stream



Inflow
Outflow

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## Summary for Reach 73R: Stream

Inflow Area = 1.978 ac, 65.68% Impervious, Inflow Depth > 4.11" for 10-year event

Inflow = 2.96 cfs @ 12.42 hrs, Volume= 0.677 af

Outflow = 2.95 cfs @ 12.46 hrs, Volume= 0.676 af, Atten= 0%, Lag= 1.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 1.91 fps, Min. Travel Time= 2.7 min Avg. Velocity = 0.54 fps, Avg. Travel Time= 9.5 min

Peak Storage= 478 cf @ 12.46 hrs Average Depth at Peak Storage= 0.31'

Bank-Full Depth= 1.00' Flow Area= 7.0 sf, Capacity= 25.38 cfs

4.00' x 1.00' deep channel, n= 0.040 Winding stream, pools & shoals

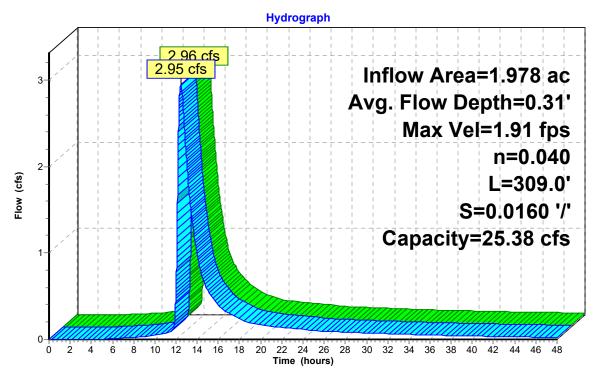
Side Slope Z-value= 3.0 '/' Top Width= 10.00'

Length= 309.0' Slope= 0.0160 '/'

Inlet Invert= 31.16', Outlet Invert= 26.22'



#### Reach 73R: Stream



## Summary for Reach 83R: Woodland Flow Path

Inflow Area = 0.333 ac, 74.25% Impervious, Inflow Depth > 4.51" for 10-year event

Inflow = 0.50 cfs @ 12.40 hrs, Volume= 0.125 af

Outflow = 0.49 cfs @ 12.49 hrs, Volume= 0.125 af, Atten= 1%, Lag= 5.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Max. Velocity= 0.29 fps, Min. Travel Time= 6.9 min Avg. Velocity = 0.09 fps, Avg. Travel Time= 23.7 min

Peak Storage= 205 cf @ 12.49 hrs Average Depth at Peak Storage= 0.15'

Bank-Full Depth= 1.00' Flow Area= 20.0 sf, Capacity= 17.44 cfs

10.00' x 1.00' deep channel, n= 0.400 Sheet flow: Woods+light brush

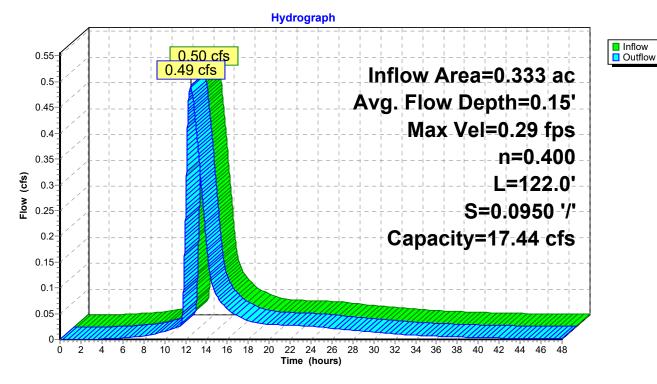
Side Slope Z-value= 10.0 '/' Top Width= 30.00'

Length= 122.0' Slope= 0.0950 '/'

Inlet Invert= 42.75', Outlet Invert= 31.16'



### Reach 83R: Woodland Flow Path



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## **Summary for Pond 1P: 15" RCP**

Inflow Area = 1.723 ac, 14.18% Impervious, Inflow Depth > 2.96" for 10-year event

Inflow = 4.57 cfs @ 12.14 hrs, Volume= 0.424 af

Outflow = 3.74 cfs @ 12.22 hrs, Volume= 0.424 af, Atten= 18%, Lag= 4.8 min

Primary = 3.74 cfs @ 12.22 hrs, Volume= 0.424 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 53.52' @ 12.22 hrs Surf.Area= 2,322 sf Storage= 659 cf

Plug-Flow detention time= 1.0 min calculated for 0.424 af (100% of inflow)

Center-of-Mass det. time= 0.9 min (874.6 - 873.7)

Volume	Invert	Avail.Storage	Storage	Description
#1	52.26'	9,237 cf	Custom	Stage Data (Prismatic)Listed below (Recalc)
Elevation	Surf A	roo Inc	Store	Cum Storo

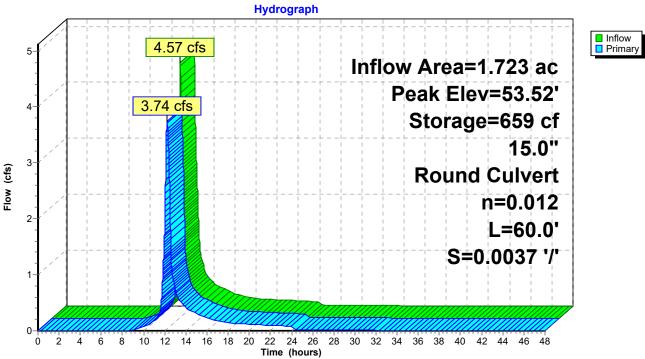
Elevation	Suri.Area	inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
52.26	10	0	0
53.00	85	35	35
54.00	4,401	2,243	2,278
55.00	9,516	6,959	9,237

Device	Routing	invert	Outlet Devices
#1	Primary	52.26'	15.0" Round Culvert

L= 60.0' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 52.26' / 52.04' S= 0.0037 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

Primary OutFlow Max=3.74 cfs @ 12.22 hrs HW=53.52' TW=0.00' (Dynamic Tailwater) 1=Culvert (Barrel Controls 3.74 cfs @ 3.77 fps)

Pond 1P: 15" RCP





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## Summary for Pond 2.1P: 24" RCP

Inflow Area = 17.114 ac, 8.97% Impervious, Inflow Depth = 2.66" for 10-year event

Inflow = 35.08 cfs @ 12.18 hrs, Volume= 3.795 af

Outflow = 18.86 cfs @ 12.54 hrs, Volume= 3.795 af, Atten= 46%, Lag= 21.8 min

Primary = 18.86 cfs @ 12.54 hrs, Volume= 3.795 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 51.35' @ 12.50 hrs Surf.Area= 20,687 sf Storage= 23,483 cf

Plug-Flow detention time= 7.7 min calculated for 3.795 af (100% of inflow)

Center-of-Mass det. time= 7.6 min (872.3 - 864.6)

<u>Volume</u>	Invert	Avail.Storage	Storage Description
#1	47.57'	80,071 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

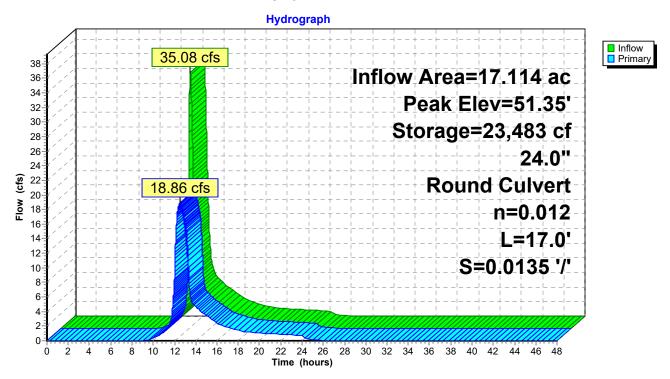
Elevation	Surt.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
47.57	100	0	0
48.00	164	57	57
49.00	2,506	1,335	1,392
50.00	7,196	4,851	6,243
51.00	14,807	11,002	17,244
52.00	31,534	23,171	40,415
53.00	47,779	39,657	80,071

Device	Routing	invert	Outlet Devices
#1	Primary	47.57'	24.0" Round Culvert

L= 17.0' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 47.57' / 47.34' S= 0.0135 '/' Cc= 0.900 n= 0.012, Flow Area= 3.14 sf

Primary OutFlow Max=18.22 cfs @ 12.54 hrs HW=51.34' TW=49.89' (Dynamic Tailwater) 1=Culvert (Inlet Controls 18.22 cfs @ 5.80 fps)

Pond 2.1P: 24" RCP



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# Summary for Pond 2P: 12" CPP

Inflow Area = 6.525 ac, 6.78% Impervious, Inflow Depth = 2.57" for 10-year event

Inflow = 23.92 cfs @ 12.00 hrs, Volume= 1.395 af

Outflow = 18.70 cfs @ 12.05 hrs, Volume= 1.395 af, Atten= 22%, Lag= 2.6 min

Primary = 18.70 cfs @ 12.05 hrs, Volume= 1.395 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 60.93' @ 12.05 hrs Surf.Area= 15,490 sf Storage= 11,719 cf

Plug-Flow detention time= 44.2 min calculated for 1.395 af (100% of inflow)

Center-of-Mass det. time= 44.1 min ( 876.6 - 832.4 )

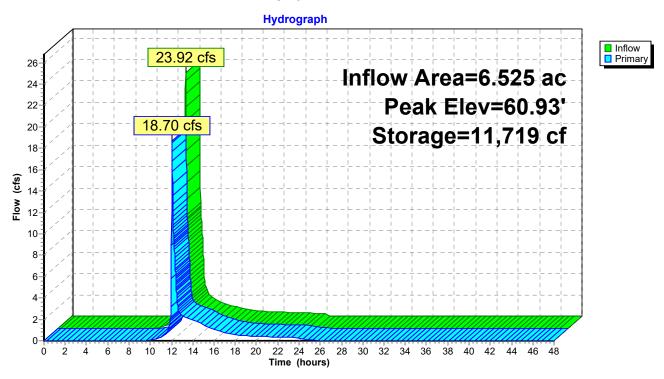
Volume	Inve	ert Avail.Sto	rage Sto	orage Description	
#1	59.6	35,7	64 cf <b>Cu</b>	stom Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on	Surf.Area	Inc.Sto	re Cum.Store	
(fee	et)	(sq-ft)	(cubic-fee	et) (cubic-feet)	
59.0	65	100		0 0	
60.0	00	6,996	1,24	1,242	
61.0	00	16,111	11,58	54 12,795	
62.0	00	29,827	22,96	35,764	
Device	Routing	Invert	Outlet D	evices	
#1	Primary	59.65'	12.0" R	ound Culvert	
			L= 9.0'	CPP, projecting, no	headwall, Ke= 0.900
			Inlet / Ou	utlet Invert= 59.65' / \$	59.31' S= 0.0378 '/' Cc= 0.900
				2, Flow Area= 0.79 s	
#2	Primary	60.75'		•	oad-Crested Rectangular Weir
			`	,	0.80 1.00 1.20 1.40 1.60 1.80 2.00
				0 3.50 4.00 4.50 5	
			,	0 /	.69 2.68 2.67 2.67 2.65 2.66 2.66
			2.68 2.7	'2 2.73 2.76 2.79 <i>2</i>	2.88 3.07 3.32

Primary OutFlow Max=18.66 cfs @ 12.05 hrs HW=60.93' TW=60.13' (Dynamic Tailwater)

1=Culvert (Inlet Controls 2.64 cfs @ 3.36 fps)

-2=Broad-Crested Rectangular Weir (Weir Controls 16.02 cfs @ 1.01 fps)

# Pond 2P: 12" CPP



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## **Summary for Pond 10P: Porous Pavement**

Inflow Area = 0.234 ac, 99.02% Impervious, Inflow Depth > 5.20" for 10-year event

Inflow = 0.09 cfs @ 21.94 hrs, Volume= 0.101 af

Outflow = 0.04 cfs @ 30.53 hrs, Volume= 0.097 af, Atten= 59%, Lag= 515.5 min

Discarded = 0.04 cfs @ 30.53 hrs, Volume= 0.097 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Peak Elev= 1.48' @ 30.53 hrs Surf.Area= 2,761 sf Storage= 1,631 cf

Plug-Flow detention time= 434.0 min calculated for 0.097 af (95% of inflow)

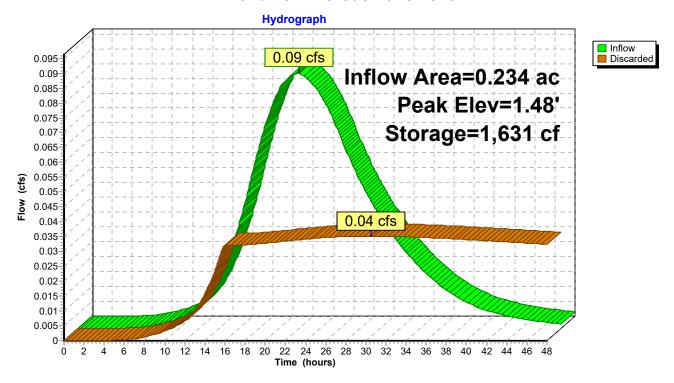
Center-of-Mass det. time= 386.3 min (1,842.5 - 1,456.2)

Volume	Inver	t Ava	il.Storage	Storage Descrip	tion		
#1	0.00	)'	2,808 cf	<b>Custom Stage</b>	Data (Conic)Listed be	elow	
Elevatio		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
0.0	00	2,761	0.0	0	0	2,761	
1.2	25	2,761	40.0	1,381	1,381	2,994	
1.5	50	2,761	40.0	276	1,657	3,040	
2.5	50	2,761	5.0	138	1,795	3,227	
3.1	7	2,761	40.0	740	2,535	3,351	
3.5	50	2,761	30.0	273	2,808	3,413	
Device	Routing	In	vert Outl	et Devices			
#1	Discarded	1 (	0.50	0 in/hr Exfiltration	on over Wetted area	Phase-In= $0.01$ '	

Discarded OutFlow Max=0.04 cfs @ 30.53 hrs HW=1.48' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

### **Pond 10P: Porous Pavement**



# Summary for Pond 11P: YD #3-1

Inflow Area = 0.013 ac, 65.82% Impervious, Inflow Depth = 4.33" for 10-year event

Inflow = 0.07 cfs @ 12.08 hrs, Volume= 0.005 af

Outflow = 0.07 cfs @ 12.08 hrs, Volume= 0.005 af, Atten= 0%, Lag= 0.0 min

Primary = 0.07 cfs @ 12.08 hrs, Volume= 0.005 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

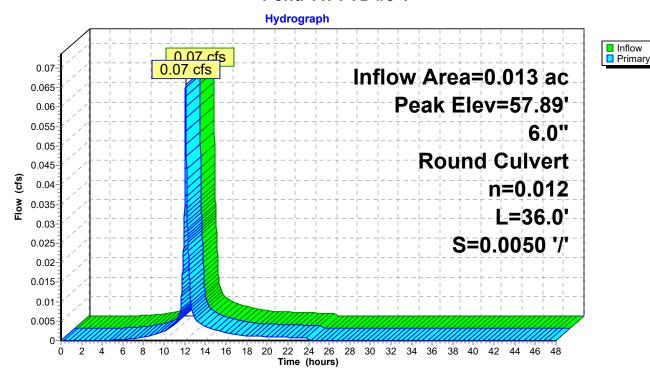
Peak Elev= 57.89' @ 12.43 hrs

Flood Elev= 60.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.16'	6.0" Round Culvert
			L= 36.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 57.16' / 56.98' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.20 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=57.59' TW=57.60' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

#### Pond 11P: YD #3-1



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## **Summary for Pond 12P: YD #7**

Inflow Area = 0.043 ac, 65.12% Impervious, Inflow Depth = 4.33" for 10-year event

Inflow = 0.21 cfs @ 12.08 hrs, Volume= 0.016 af

Outflow = 0.21 cfs @ 12.08 hrs, Volume= 0.016 af, Atten= 0%, Lag= 0.0 min

Primary = 0.21 cfs @ 12.08 hrs, Volume= 0.016 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

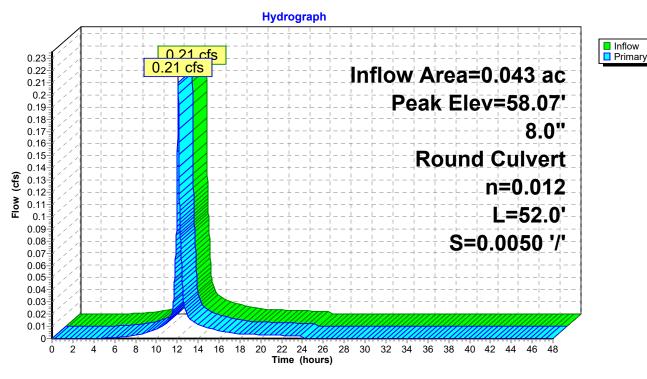
Peak Elev= 58.07' @ 12.10 hrs

Flood Elev= 59.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.76'	8.0" Round Culvert
			L= 52.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 57.76' / 57.50' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.35 sf

Primary OutFlow Max=0.20 cfs @ 12.08 hrs HW=58.07' TW=57.79' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.20 cfs @ 1.91 fps)

### Pond 12P: YD #7



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## **Summary for Pond 13P: YD #6**

Inflow Area = 0.074 ac, 68.76% Impervious, Inflow Depth = 4.42" for 10-year event

Inflow = 0.37 cfs @ 12.08 hrs, Volume= 0.027 af

Outflow = 0.37 cfs @ 12.08 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Primary = 0.37 cfs @ 12.08 hrs, Volume= 0.027 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

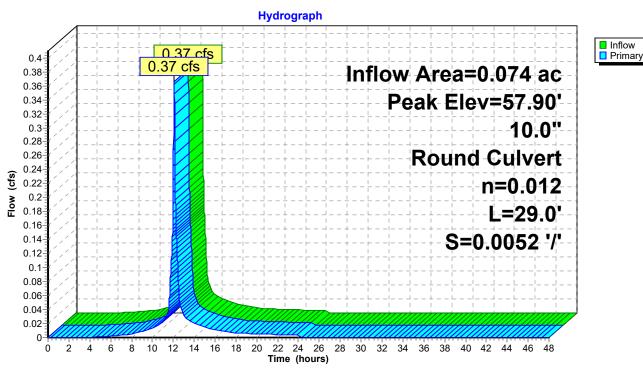
Peak Elev= 57.90' @ 12.42 hrs

Flood Elev= 60.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.33'	10.0" Round Culvert
			L= 29.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 57.33' / 57.18' S= 0.0052 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.55 sf

Primary OutFlow Max=0.33 cfs @ 12.08 hrs HW=57.79' TW=57.69' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.33 cfs @ 1.56 fps)

## Pond 13P: YD #6



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## Summary for Pond 14P: YD #5

Inflow Area = 0.098 ac, 70.93% Impervious, Inflow Depth = 4.48" for 10-year event

Inflow = 0.49 cfs @ 12.08 hrs, Volume= 0.036 af

Outflow = 0.49 cfs @ 12.08 hrs, Volume= 0.036 af, Atten= 0%, Lag= 0.0 min

Primary = 0.49 cfs @ 12.08 hrs, Volume= 0.036 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

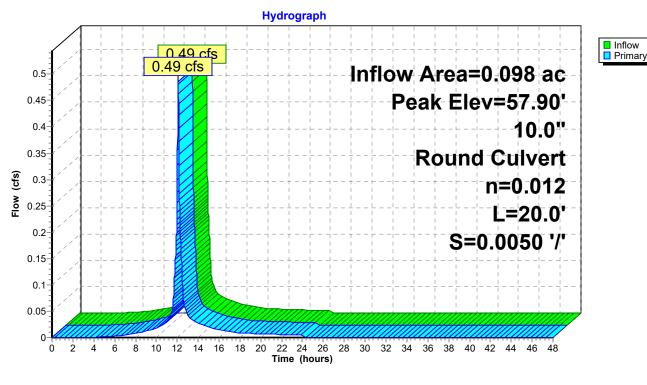
Peak Elev= 57.90' @ 12.42 hrs

Flood Elev= 60.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.08'	10.0" Round Culvert
			L= 20.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 57.08' / 56.98' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.55 sf

Primary OutFlow Max=0.40 cfs @ 12.08 hrs HW=57.69' TW=57.63' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.40 cfs @ 1.31 fps)

### Pond 14P: YD #5



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# Summary for Pond 15P: YD #4

Inflow Area = 0.129 ac, 64.15% Impervious, Inflow Depth = 4.29" for 10-year event

Inflow = 0.62 cfs @ 12.08 hrs, Volume= 0.046 af

Outflow = 0.62 cfs @ 12.08 hrs, Volume= 0.046 af, Atten= 0%, Lag= 0.0 min

Primary = 0.62 cfs @ 12.08 hrs, Volume= 0.046 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

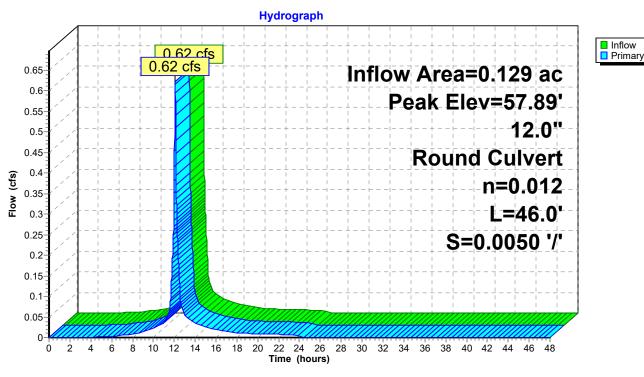
Peak Elev= 57.89' @ 12.42 hrs

Flood Elev= 60.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	56.81'	12.0" Round Culvert
			L= 46.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 56.81' / 56.58' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.44 cfs @ 12.08 hrs HW=57.63' TW=57.60' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.44 cfs @ 0.87 fps)

## Pond 15P: YD #4



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# Summary for Pond 16P: CB #3

Inflow Area = 0.164 ac, 59.40% Impervious, Inflow Depth = 4.17" for 10-year event

Inflow = 0.77 cfs @ 12.09 hrs, Volume= 0.057 af

Outflow = 0.77 cfs @ 12.09 hrs, Volume= 0.057 af, Atten= 0%, Lag= 0.0 min

Primary = 0.77 cfs @ 12.09 hrs, Volume= 0.057 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

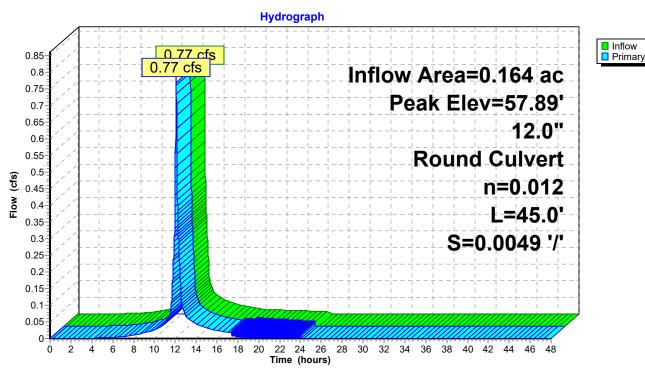
Peak Elev= 57.89' @ 12.42 hrs

Flood Elev= 61.25'

Device	Routing	Invert	Outlet Devices
#1	Primary	56.48'	12.0" Round Culvert
			L= 45.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 56.48' / 56.26' S= 0.0049 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.45 cfs @ 12.09 hrs HW=57.60' TW=57.59' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.45 cfs @ 0.63 fps)

### Pond 16P: CB #3



Printed 7/15/2025

### **Summary for Pond 17P: Bio #1**

Inflow Area = 0.230 ac, 42.35% Impervious, Inflow Depth = 3.76" for 10-year event

0.98 cfs @ 12.09 hrs, Volume= Inflow 0.072 af

0.30 cfs @ 12.42 hrs, Volume= Outflow = 0.072 af, Atten= 70%, Lag= 19.8 min

0.30 cfs @ 12.42 hrs, Volume= Primary 0.072 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 56.25' Surf.Area= 487 sf Storage= 37 cf

Peak Elev= 57.89' @ 12.42 hrs Surf.Area= 1,182 sf Storage= 1,368 cf (1,331 cf above start)

Flood Elev= 59.25' Surf.Area= 1,950 sf Storage= 3,480 cf (3,444 cf above start)

Plug-Flow detention time= 283.3 min calculated for 0.071 af (98% of inflow)

Center-of-Mass det. time= 266.2 min (1,065.8 - 799.6)

Volume	Inver	t Ava	il.Storage	e Storage Descri	iption		
#1	54.75	5'	3,480 c	f Custom Stage	Data (Conic)Listed	l below (Recalc)	
<b>□</b> 14:		<b></b>	\	lus a Ottama	Orana Otama	\M_+4_A_==	
Elevation		Surf.Area	Voids	Inc.Store	Cum.Store	Wet.Area	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>	
54.	75	487	0.0	0	0	487	
56.2	25	487	5.0	37	37	604	
57.0	00	774	100.0	469	505	899	
58.0	00	1,239	100.0	997	1,503	1,377	
59.0		1,797	100.0	1,509	3,012	1,952	
59.2		1,950	100.0	468	3,480	2,110	
		,,,,,,,			2, 122	_,	
Device	Routing	In	vert O	utlet Devices			
#1	Primary	53	3.75' <b>15</b>	5.0" Round Culve	ert		
	,		L=	: 30.0' CPP. squa	are edge headwall,  I	Ke= 0.500	
						0.0050 '/' Cc= 0.900	
				0.012, Flow Area			
#2	Device 1	53		0" Vert. Underdra			
#3	Device 2		-			over Wetted area abo	ve 56 25'
110	D01100 2	00			ea = 604 sf Phase-l		VC 00.20
#4	Device 1	57		0" Vert. Orifice/G		11- 0.01	
#5	Device 1				Orifice/Grate C= (	n 600	
π0	Device 1	50		mited to weir flow a		3.000	

Primary OutFlow Max=0.30 cfs @ 12.42 hrs HW=57.89' TW=53.71' (Dynamic Tailwater)

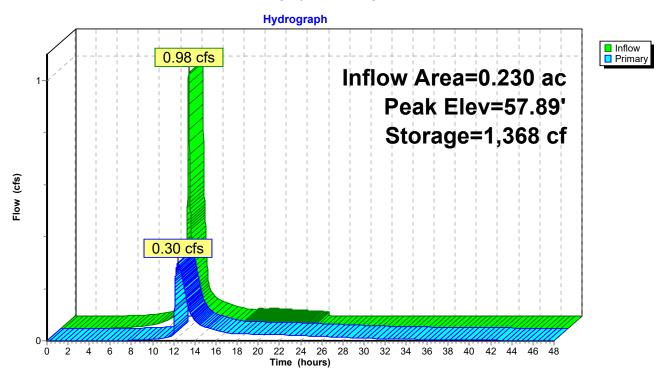
-1=Culvert (Passes 0.30 cfs of 11.08 cfs potential flow)

<sup>-2=</sup>Underdrain (Passes 0.04 cfs of 0.84 cfs potential flow)
-3=Exfiltration throiugh Media (Exfiltration Controls 0.04 cfs)

<sup>-4=</sup>Orifice/Grate (Orifice Controls 0.26 cfs @ 2.94 fps)

<sup>-5=</sup>Orifice/Grate (Controls 0.00 cfs)

### Pond 17P: Bio #1



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## Summary for Pond 21P: CB #8

Inflow Area = 0.060 ac,100.00% Impervious, Inflow Depth = 5.23" for 10-year event

Inflow = 0.32 cfs @ 12.08 hrs, Volume= 0.026 af

Outflow = 0.32 cfs @ 12.08 hrs, Volume= 0.026 af, Atten= 0%, Lag= 0.0 min

Primary = 0.32 cfs @ 12.08 hrs, Volume= 0.026 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

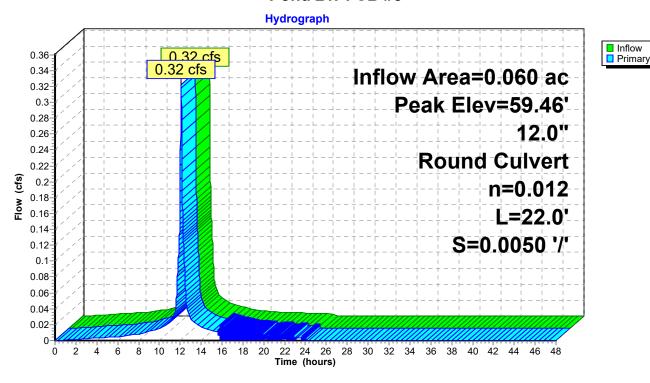
Peak Elev= 59.46' @ 12.47 hrs

Flood Elev= 60.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	57.86'	12.0" Round Culvert
			L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 57.86' / 57.75' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=59.12' TW=59.14' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

#### Pond 21P: CB #8



Volume

Printed 7/15/2025

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### **Summary for Pond 22P: Bio #2**

Inflow Area = 0.362 ac, 74.85% Impervious, Inflow Depth = 4.61" for 10-year event

Inflow 1.74 cfs @ 12.08 hrs, Volume= 0.139 af

0.44 cfs @ 12.46 hrs, Volume= Outflow = 0.137 af, Atten= 75%, Lag= 22.4 min

0.44 cfs @ 12.46 hrs, Volume= Primary 0.137 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 57.75' Surf.Area= 1,027 sf Storage= 77 cf

Peak Elev= 59.46' @ 12.46 hrs Surf.Area= 2,117 sf Storage= 2,733 cf (2,656 cf above start)

Flood Elev= 60.00' Surf.Area= 2,511 sf Storage= 3,983 cf (3,906 cf above start)

Avail.Storage Storage Description

Plug-Flow detention time= 263.1 min calculated for 0.136 af (98% of inflow)

Center-of-Mass det. time= 240.0 min (999.5 - 759.5)

Invert

#1	56.25'		3,983 cf	Custom Stage D	Data (Conic)Listed	below (Recalc)	
Elevation (fee		ırf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
56.2		1,027	0.0	0	0	1,027	
57.7		1,027	5.0	77	77	1,197	
58.0		•	100.0	275	352	1,348	
59.0		,	100.0	1,481	1,833	1,997	
60.0		•	100.0	2,150	3,983	2,718	
Device	Routing	Inv	ert Outle	et Devices			
#1	Primary	55.:	L= 1 Inlet		e edge headwall, K 5.25' / 55.16' S= 0	(e= 0.500 .0050 '/'	
#2	Device 1	55.2		Vert. Underdrain			
#3	Device 2	57.			n throiugh Media = 1,197 sf Phase-	over Wetted area abo	ove 57.75'
#4	Device 1	58.		Vert. Orifice/Gra			
#5	Device 1	59.		" x 24.0" Horiz. O	Orifice/Grate C= 0 low heads	.600	

Primary OutFlow Max=0.44 cfs @ 12.46 hrs HW=59.46' TW=55.21' (Dynamic Tailwater)

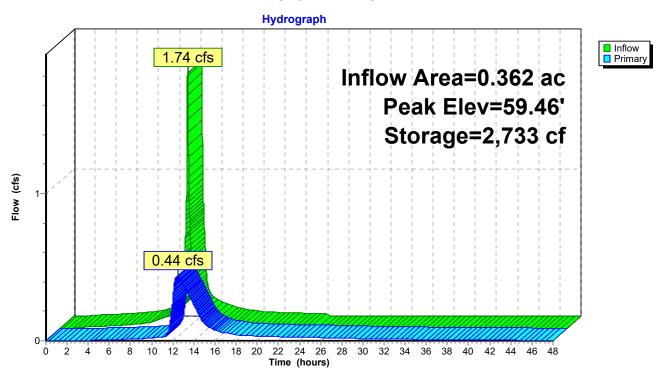
**1=Culvert** (Passes 0.44 cfs of 11.19 cfs potential flow)

<sup>2=</sup>Underdrain (Passes 0.06 cfs of 0.84 cfs potential flow)
3=Exfiltration throiugh Media (Exfiltration Controls 0.06 cfs)

**<sup>-4=</sup>Orifice/Grate** (Orifice Controls 0.37 cfs @ 4.29 fps)

<sup>-5=</sup>Orifice/Grate (Controls 0.00 cfs)

### Pond 22P: Bio #2



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# Summary for Pond 30P: CB #10-2

Inflow Area = 0.189 ac, 53.10% Impervious, Inflow Depth = 4.01" for 10-year event

Inflow = 0.87 cfs @ 12.09 hrs, Volume= 0.063 af

Outflow = 0.87 cfs @ 12.09 hrs, Volume= 0.063 af, Atten= 0%, Lag= 0.0 min

Primary = 0.87 cfs @ 12.09 hrs, Volume= 0.063 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

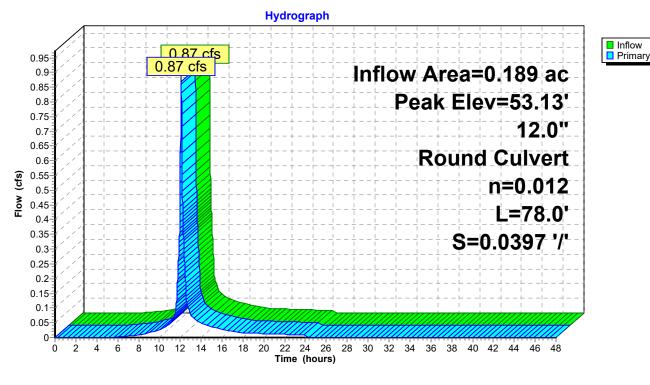
Peak Elev= 53.13' @ 12.09 hrs

Flood Elev= 56.65'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.65'	12.0" Round Culvert
			L= 78.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 52.65' / 49.55' S= 0.0397 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.87 cfs @ 12.09 hrs HW=53.13' TW=49.20' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.87 cfs @ 2.35 fps)

## Pond 30P: CB #10-2



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# Summary for Pond 31P: CB #10-1

Inflow Area = 0.164 ac, 71.11% Impervious, Inflow Depth = 4.44" for 10-year event

Inflow = 0.81 cfs @ 12.08 hrs, Volume= 0.061 af

Outflow = 0.81 cfs @ 12.08 hrs, Volume= 0.061 af, Atten= 0%, Lag= 0.0 min

Primary = 0.81 cfs @ 12.08 hrs, Volume= 0.061 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

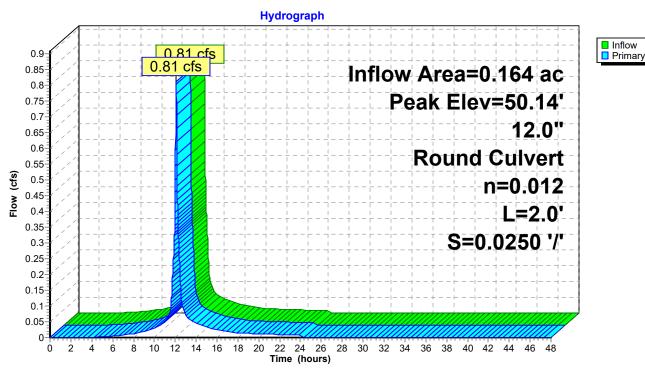
Peak Elev= 50.14' @ 12.08 hrs

Flood Elev= 53.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.60'	12.0" Round Culvert
	_		L= 2.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.60' / 49.55' S= 0.0250 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.81 cfs @ 12.08 hrs HW=50.13' TW=49.20' (Dynamic Tailwater) 1=Culvert (Barrel Controls 0.81 cfs @ 2.75 fps)

## Pond 31P: CB #10-1



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## Summary for Pond 32P: DMH #10

Inflow Area = 17.467 ac, 10.03% Impervious, Inflow Depth > 2.69" for 10-year event

Inflow = 19.20 cfs @ 12.50 hrs, Volume= 3.919 af

Outflow = 19.20 cfs @ 12.50 hrs, Volume= 3.919 af, Atten= 0%, Lag= 0.0 min

Primary = 19.20 cfs @ 12.50 hrs, Volume= 3.919 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

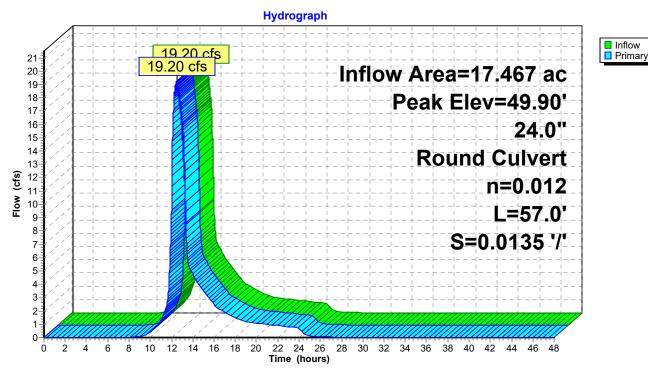
Peak Elev= 49.90' @ 12.50 hrs

Flood Elev= 53.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	47.29'	24.0" Round Culvert
	_		L= 57.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 47.29' / 46.52' S= 0.0135 '/' Cc= 0.900
			n= 0.012. Flow Area= 3.14 sf

Primary OutFlow Max=19.20 cfs @ 12.50 hrs HW=49.90' TW=47.33' (Dynamic Tailwater) 1=Culvert (Inlet Controls 19.20 cfs @ 6.11 fps)

## Pond 32P: DMH #10



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## Summary for Pond 40P: 6" CPP

Inflow Area = 0.070 ac,100.00% Impervious, Inflow Depth = 5.23" for 10-year event

Inflow = 0.38 cfs @ 12.08 hrs, Volume= 0.031 af

Outflow = 0.38 cfs @ 12.08 hrs, Volume= 0.031 af, Atten= 0%, Lag= 0.0 min

Primary = 0.38 cfs @ 12.08 hrs, Volume= 0.031 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

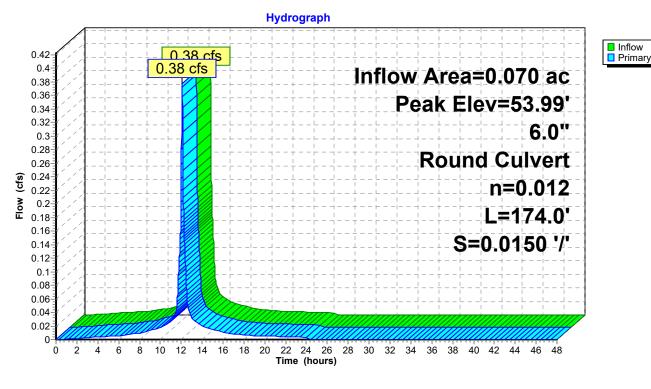
Peak Elev= 53.99' @ 12.08 hrs

Flood Elev= 56.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	53.58'	6.0" Round Culvert
			L= 174.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 53.58' / 50.97' S= 0.0150 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.20 sf

Primary OutFlow Max=0.38 cfs @ 12.08 hrs HW=53.99' TW=52.15' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.38 cfs @ 2.18 fps)

#### Pond 40P: 6" CPP



## **Summary for Pond 41P: YD #15**

Inflow Area = 0.119 ac, 96.30% Impervious, Inflow Depth = 5.14" for 10-year event

Inflow = 0.63 cfs @ 12.08 hrs, Volume= 0.051 af

Outflow = 0.63 cfs @ 12.08 hrs, Volume= 0.051 af, Atten= 0%, Lag= 0.0 min

Primary = 0.63 cfs @ 12.08 hrs, Volume= 0.051 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

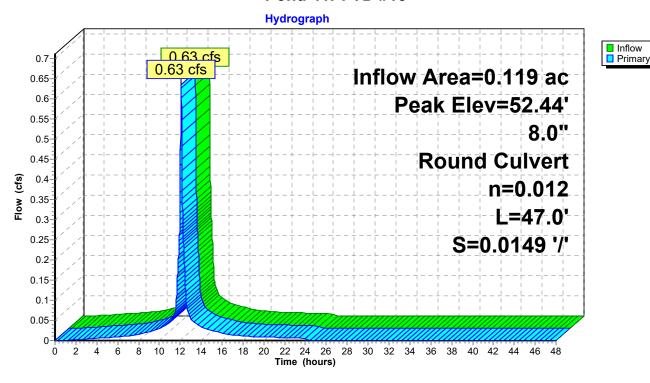
Peak Elev= 52.44' @ 12.12 hrs

Flood Elev= 55.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	50.80'	8.0" Round Culvert
	_		L= 47.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.80' / 50.10' S= 0.0149 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.35 sf

Primary OutFlow Max=0.36 cfs @ 12.08 hrs HW=52.15' TW=52.09' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.36 cfs @ 1.03 fps)

#### Pond 41P: YD #15



## Summary for Pond 42P: 6" CPP

Inflow Area = 0.050 ac,100.00% Impervious, Inflow Depth = 5.23" for 10-year event

Inflow = 0.27 cfs @ 12.08 hrs, Volume= 0.022 af

Outflow = 0.27 cfs @ 12.08 hrs, Volume= 0.022 af, Atten= 0%, Lag= 0.0 min

Primary = 0.27 cfs @ 12.08 hrs, Volume= 0.022 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

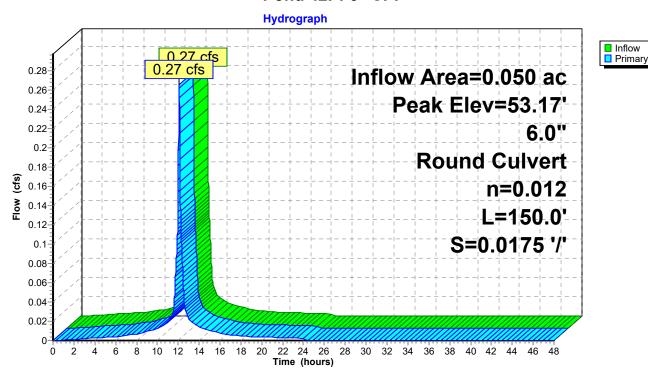
Peak Elev= 53.17' @ 12.11 hrs

Flood Elev= 56.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	52.81'	6.0" Round Culvert
			L= 150.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 52.81' / 50.19' S= 0.0175 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.20 sf

Primary OutFlow Max=0.25 cfs @ 12.08 hrs HW=53.15' TW=52.09' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.25 cfs @ 2.46 fps)

#### Pond 42P: 6" CPP



☐ Inflow☐ Primary

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# Summary for Pond 43P: 10" CPP

Inflow Area = 0.169 ac, 97.39% Impervious, Inflow Depth = 5.17" for 10-year event

Inflow = 0.90 cfs @ 12.08 hrs, Volume= 0.073 af

Outflow = 0.90 cfs @ 12.08 hrs, Volume= 0.073 af, Atten= 0%, Lag= 0.0 min

Primary = 0.90 cfs @ 12.08 hrs, Volume= 0.073 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

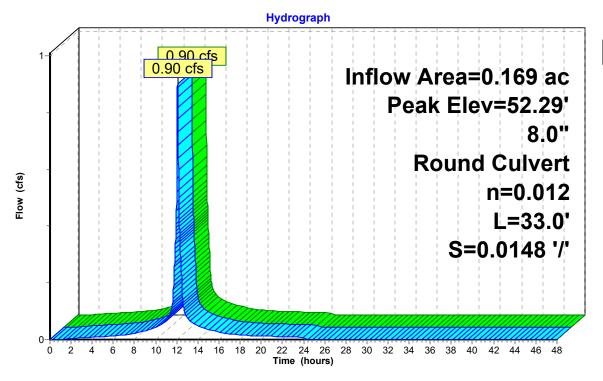
Peak Elev= 52.29' @ 12.12 hrs

Flood Elev= 56.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	50.10'	8.0" Round Culvert
			L= 33.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.10' / 49.61' S= 0.0148 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.35 sf

Primary OutFlow Max=0.74 cfs @ 12.08 hrs HW=52.09' TW=51.88' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.74 cfs @ 2.11 fps)

#### Pond 43P: 10" CPP



## **Summary for Pond 44P: CB #14**

Inflow Area = 0.276 ac, 75.46% Impervious, Inflow Depth = 4.60" for 10-year event

Inflow = 1.36 cfs @ 12.08 hrs, Volume= 0.106 af

Outflow = 1.36 cfs @ 12.08 hrs, Volume= 0.106 af, Atten= 0%, Lag= 0.0 min

Primary = 1.36 cfs @ 12.08 hrs, Volume= 0.106 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

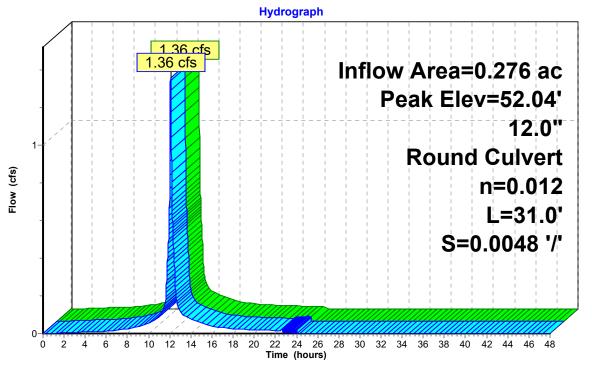
Peak Elev= 52.04' @ 12.12 hrs

Flood Elev= 54.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.27'	12.0" Round Culvert
			L= 31.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.27' / 49.12' S= 0.0048 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.87 cfs @ 12.08 hrs HW=51.89' TW=51.84' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.87 cfs @ 1.10 fps)

#### Pond 44P: CB #14





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## Summary for Pond 45P: CB #13-2

Inflow Area = 0.088 ac, 71.88% Impervious, Inflow Depth = 4.44" for 10-year event

Inflow = 0.44 cfs @ 12.08 hrs, Volume= 0.033 af

Outflow = 0.44 cfs @ 12.08 hrs, Volume= 0.033 af, Atten= 0%, Lag= 0.0 min

Primary = 0.44 cfs @ 12.08 hrs, Volume= 0.033 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

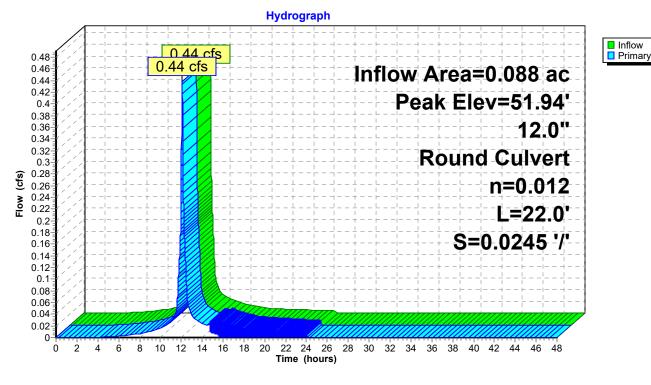
Peak Elev= 51.94' @ 12.12 hrs

Flood Elev= 54.65'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.65'	12.0" Round Culvert
			L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.65' / 49.11' S= 0.0245 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=51.78' TW=51.84' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

### Pond 45P: CB #13-2



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# Summary for Pond 46P: CB #13-1

Inflow Area = 0.103 ac, 73.25% Impervious, Inflow Depth = 4.55" for 10-year event

Inflow = 0.52 cfs @ 12.08 hrs, Volume= 0.039 af

Outflow = 0.52 cfs @ 12.08 hrs, Volume= 0.039 af, Atten= 0%, Lag= 0.0 min

Primary = 0.52 cfs @ 12.08 hrs, Volume= 0.039 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

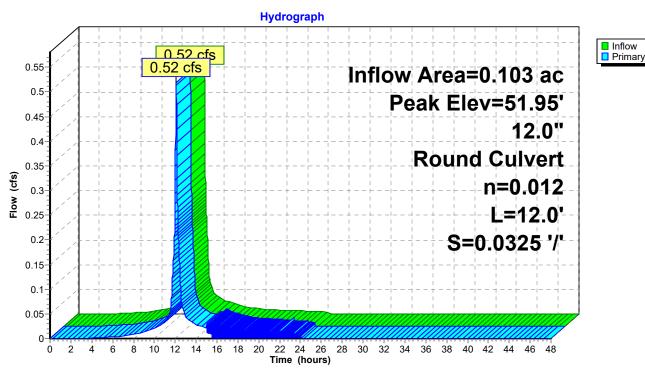
Peak Elev= 51.95' @ 12.12 hrs

Flood Elev= 54.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.50'	12.0" Round Culvert
			L= 12.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.50' / 49.11' S= 0.0325 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=51.78' TW=51.84' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

## Pond 46P: CB #13-1



# Summary for Pond 47P: DMH #13

Inflow Area = 0.467 ac, 74.30% Impervious, Inflow Depth = 4.56" for 10-year event

Inflow = 2.32 cfs @ 12.08 hrs, Volume= 0.177 af

Outflow = 2.32 cfs @ 12.08 hrs, Volume= 0.177 af, Atten= 0%, Lag= 0.0 min

Primary = 2.32 cfs @ 12.08 hrs, Volume= 0.177 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

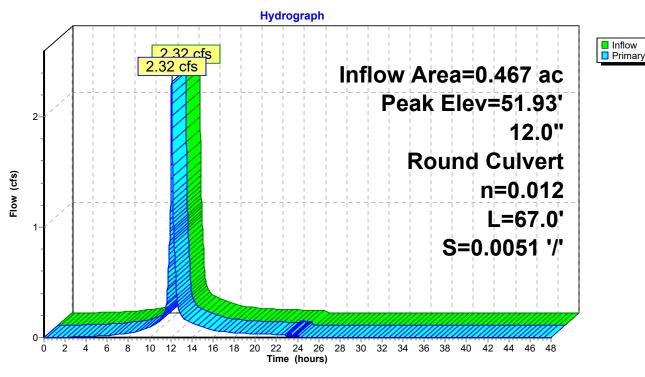
Peak Elev= 51.93' @ 12.11 hrs

Flood Elev= 54.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.01'	12.0" Round Culvert
			L= 67.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.01' / 48.67' S= 0.0051 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=2.15 cfs @ 12.08 hrs HW=51.84' TW=51.45' (Dynamic Tailwater) 1=Culvert (Outlet Controls 2.15 cfs @ 2.74 fps)

## Pond 47P: DMH #13



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## Summary for Pond 48P: CB #12-2

Inflow Area = 0.078 ac, 55.67% Impervious, Inflow Depth = 4.12" for 10-year event

Inflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af

Outflow = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Primary = 0.37 cfs @ 12.09 hrs, Volume= 0.027 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

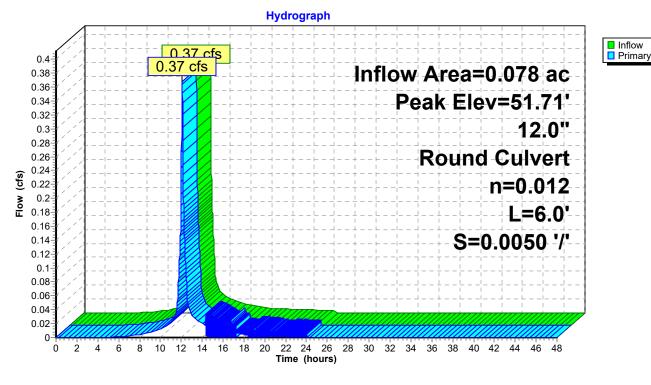
Peak Elev= 51.71' @ 12.36 hrs

Flood Elev= 52.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	48.70'	12.0" Round Culvert
	-		L= 6.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 48.70' / 48.67' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=51.41' TW=51.46' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

## Pond 48P: CB #12-2



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# Summary for Pond 49P: CB #12-1

Inflow Area = 0.084 ac, 83.90% Impervious, Inflow Depth = 4.66" for 10-year event

Inflow = 0.43 cfs @ 12.08 hrs, Volume= 0.033 af

Outflow = 0.43 cfs @ 12.08 hrs, Volume= 0.033 af, Atten= 0%, Lag= 0.0 min

Primary = 0.43 cfs @ 12.08 hrs, Volume= 0.033 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

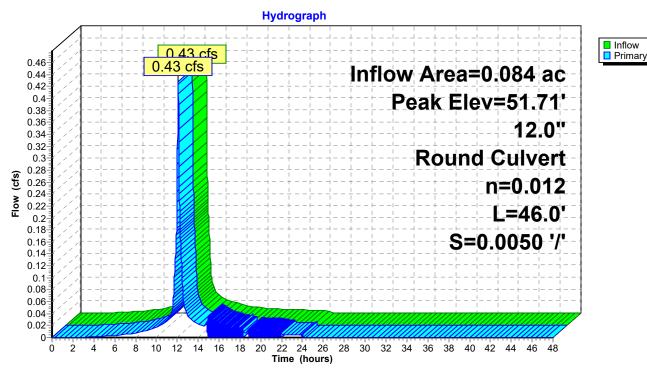
Peak Elev= 51.71' @ 12.36 hrs

Flood Elev= 52.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	48.90'	12.0" Round Culvert
			L= 46.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 48.90' / 48.67' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=51.41' TW=51.45' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

### Pond 49P: CB #12-1



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# Summary for Pond 50P: DMH #12

Inflow Area = 0.629 ac, 73.25% Impervious, Inflow Depth = 4.51" for 10-year event

Inflow = 3.11 cfs @ 12.08 hrs, Volume= 0.237 af

Outflow = 3.11 cfs @ 12.08 hrs, Volume= 0.237 af, Atten= 0%, Lag= 0.0 min

Primary = 3.11 cfs @ 12.08 hrs, Volume= 0.237 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

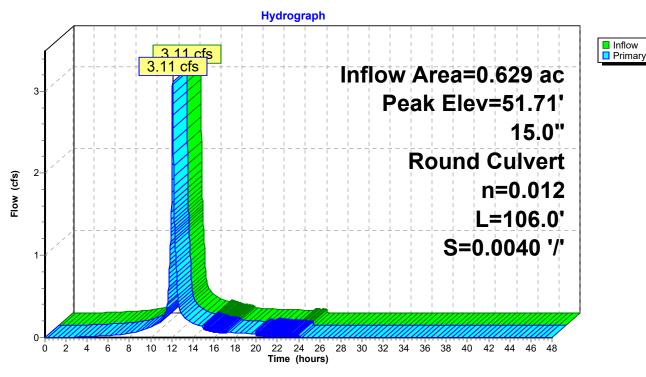
Peak Elev= 51.71' @ 12.35 hrs

Flood Elev= 54.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	48.42'	15.0" Round Culvert
			L= 106.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 48.42' / 48.00' S= 0.0040 '/' Cc= 0.900
			n= 0.012. Flow Area= 1.23 sf

Primary OutFlow Max=2.86 cfs @ 12.08 hrs HW=51.46' TW=51.15' (Dynamic Tailwater) 1=Culvert (Outlet Controls 2.86 cfs @ 2.33 fps)

### Pond 50P: DMH #12



☐ Inflow☐ Primary

#### 5440-Post

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## Summary for Pond 60P: CB #17-1-2

Inflow Area = 0.210 ac, 78.19% Impervious, Inflow Depth = 4.66" for 10-year event

Inflow = 1.07 cfs @ 12.08 hrs, Volume= 0.082 af

Outflow = 1.07 cfs @ 12.08 hrs, Volume= 0.082 af, Atten= 0%, Lag= 0.0 min

Primary = 1.07 cfs @ 12.08 hrs, Volume= 0.082 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

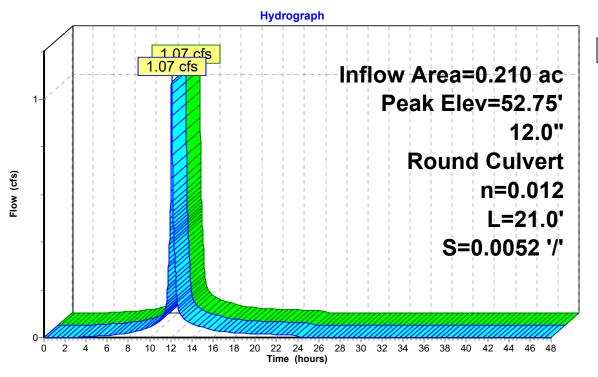
Peak Elev= 52.75' @ 12.12 hrs

Flood Elev= 54.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	50.40'	12.0" Round Culvert
	_		L= 21.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.40' / 50.29' S= 0.0052 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=52.48' TW=52.53' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

## Pond 60P: CB #17-1-2



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## Summary for Pond 61P: CB #17-1-1

Inflow Area = 0.162 ac, 91.98% Impervious, Inflow Depth = 5.00" for 10-year event

Inflow = 0.86 cfs @ 12.08 hrs, Volume= 0.068 af

Outflow = 0.86 cfs @ 12.08 hrs, Volume= 0.068 af, Atten= 0%, Lag= 0.0 min

Primary = 0.86 cfs @ 12.08 hrs, Volume= 0.068 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

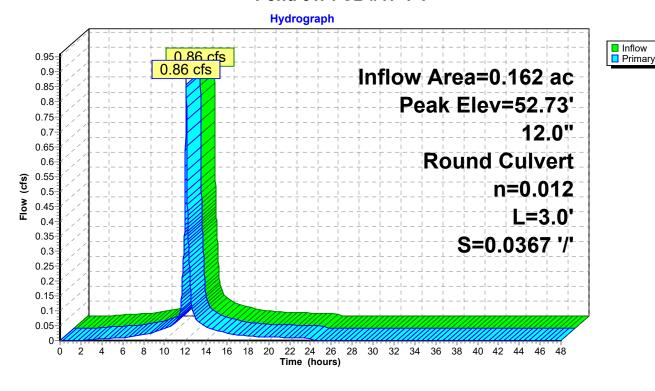
Peak Elev= 52.73' @ 12.12 hrs

Flood Elev= 54.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	50.40'	12.0" Round Culvert
	_		L= 3.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.40' / 50.29' S= 0.0367 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=52.44' TW=52.53' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

#### Pond 61P: CB #17-1-1



## Summary for Pond 62P: DMH #17-1

Inflow Area = 0.373 ac, 84.19% Impervious, Inflow Depth = 4.81" for 10-year event

Inflow = 1.93 cfs @ 12.08 hrs, Volume= 0.149 af

Outflow = 1.93 cfs @ 12.08 hrs, Volume= 0.149 af, Atten= 0%, Lag= 0.0 min

Primary = 1.93 cfs @ 12.08 hrs, Volume= 0.149 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

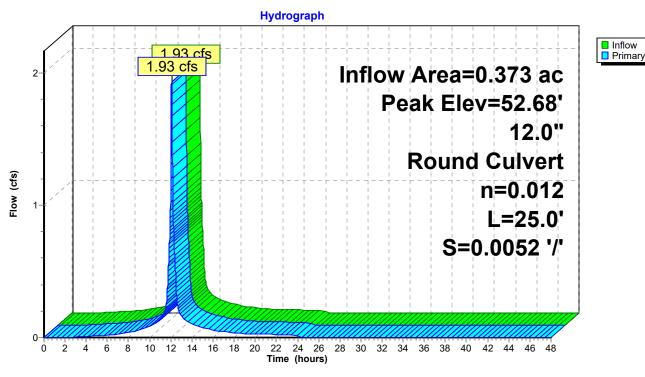
Peak Elev= 52.68' @ 12.11 hrs

Flood Elev= 54.95'

Device	Routing	Invert	Outlet Devices
#1	Primary	50.19'	12.0" Round Culvert
			L= 25.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.19' / 50.06' S= 0.0052 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=1.52 cfs @ 12.08 hrs HW=52.53' TW=52.37' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.52 cfs @ 1.94 fps)

### Pond 62P: DMH #17-1



## **Summary for Pond 63P: YD #21**

Inflow Area = 0.033 ac, 65.52% Impervious, Inflow Depth = 4.33" for 10-year event

Inflow = 0.16 cfs @ 12.08 hrs, Volume= 0.012 af

Outflow = 0.16 cfs @ 12.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary = 0.16 cfs @ 12.08 hrs, Volume= 0.012 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

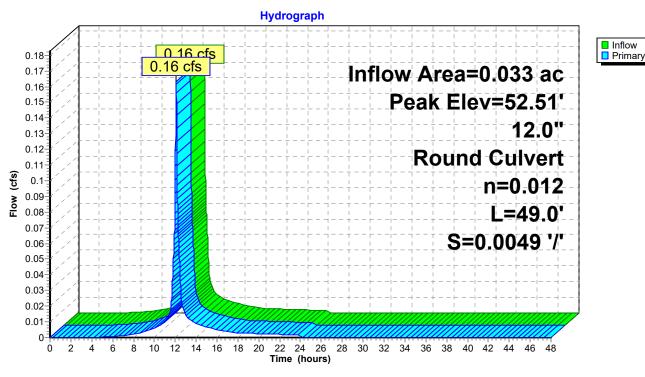
Peak Elev= 52.51' @ 12.14 hrs

Flood Elev= 55.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	51.70'	12.0" Round Culvert
	-		L= 49.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 51.70' / 51.46' S= 0.0049 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=52.02' TW=52.07' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

## Pond 63P: YD #21



## **Summary for Pond 64P: YD #20**

Inflow Area = 0.068 ac, 73.52% Impervious, Inflow Depth = 4.55" for 10-year event

Inflow = 0.34 cfs @ 12.08 hrs, Volume= 0.026 af

Outflow = 0.34 cfs @ 12.08 hrs, Volume= 0.026 af, Atten= 0%, Lag= 0.0 min

Primary = 0.34 cfs @ 12.08 hrs, Volume= 0.026 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

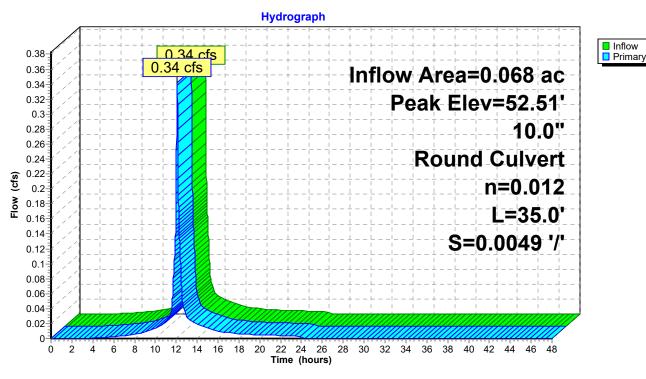
Peak Elev= 52.51' @ 12.13 hrs

Flood Elev= 55.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	51.28'	10.0" Round Culvert
			L= 35.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 51.28' / 51.11' S= 0.0049 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.55 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=52.07' TW=52.20' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

## Pond 64P: YD #20



## **Summary for Pond 65P: YD #19**

Inflow Area = 0.091 ac, 75.35% Impervious, Inflow Depth = 4.58" for 10-year event

Inflow = 0.46 cfs @ 12.08 hrs, Volume= 0.035 af

Outflow = 0.46 cfs @ 12.08 hrs, Volume= 0.035 af, Atten= 0%, Lag= 0.0 min

Primary = 0.46 cfs @ 12.08 hrs, Volume= 0.035 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

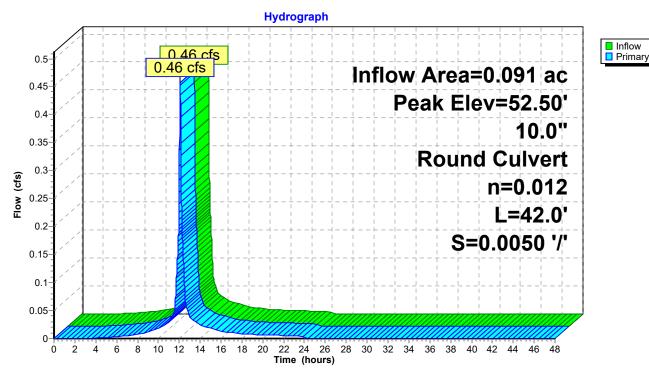
Peak Elev= 52.50' @ 12.12 hrs

Flood Elev= 56.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	51.00'	10.0" Round Culvert
			L= 42.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 51.00' / 50.79' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.55 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=52.20' TW=52.30' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

## Pond 65P: YD #19



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## **Summary for Pond 66P: YD #18**

Inflow Area = 0.125 ac, 67.02% Impervious, Inflow Depth = 4.29" for 10-year event

Inflow = 0.60 cfs @ 12.08 hrs, Volume= 0.044 af

Outflow = 0.60 cfs @ 12.08 hrs, Volume= 0.044 af, Atten= 0%, Lag= 0.0 min

Primary = 0.60 cfs @ 12.08 hrs, Volume= 0.044 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

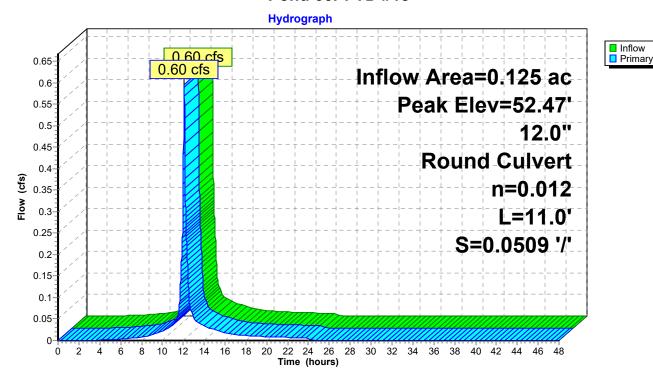
Peak Elev= 52.47' @ 12.11 hrs

Flood Elev= 55.55'

Device	Routing	Invert	Outlet Devices
#1	Primary	50.62'	12.0" Round Culvert
			L= 11.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.62' / 50.06' S= 0.0509 '/' Cc= 0.900
			n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.08 hrs HW=52.31' TW=52.38' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

#### Pond 66P: YD #18



☐ Inflow☐ Primary

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## Summary for Pond 67P: CB #17

Inflow Area = 0.532 ac, 75.35% Impervious, Inflow Depth = 4.50" for 10-year event

Inflow = 2.60 cfs @ 12.08 hrs, Volume= 0.199 af

Outflow = 2.60 cfs @ 12.08 hrs, Volume= 0.199 af, Atten= 0%, Lag= 0.0 min

Primary = 2.60 cfs @ 12.08 hrs, Volume= 0.199 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

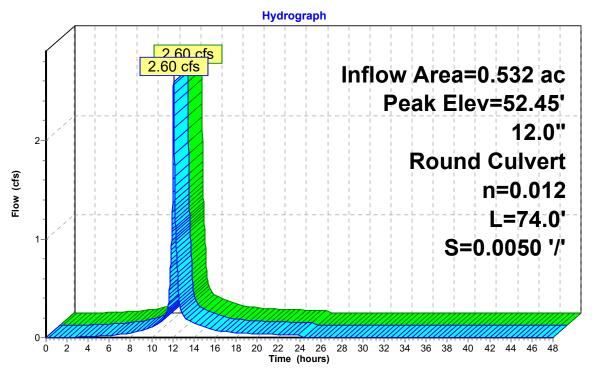
Peak Elev= 52.45' @ 12.10 hrs

Flood Elev= 55.55'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.96'	12.0" Round Culvert
			L= 74.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.96' / 49.59' S= 0.0050 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=2.45 cfs @ 12.08 hrs HW=52.37' TW=51.85' (Dynamic Tailwater) 1=Culvert (Outlet Controls 2.45 cfs @ 3.12 fps)

## Pond 67P: CB #17



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## Summary for Pond 68P: DMH #16

Inflow Area = 0.563 ac, 76.73% Impervious, Inflow Depth = 4.54" for 10-year event

Inflow = 2.77 cfs @ 12.08 hrs, Volume= 0.213 af

Outflow = 2.77 cfs @ 12.08 hrs, Volume= 0.213 af, Atten= 0%, Lag= 0.0 min

Primary = 2.77 cfs @ 12.08 hrs, Volume= 0.213 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

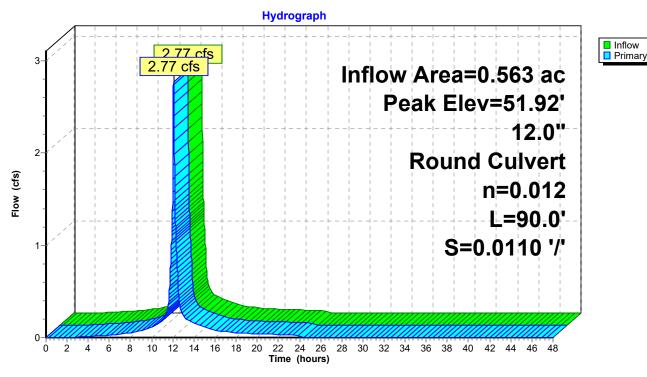
Peak Elev= 51.92' @ 12.11 hrs

Flood Elev= 56.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.49'	12.0" Round Culvert
	_		L= 90.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 49.49' / 48.50' S= 0.0110 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=2.66 cfs @ 12.08 hrs HW=51.85' TW=51.15' (Dynamic Tailwater) 1=Culvert (Outlet Controls 2.66 cfs @ 3.39 fps)

### Pond 68P: DMH #16



Volume

Invert

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## **Summary for Pond 69P: Bio #3**

Inflow Area = 1.645 ac, 63.94% Impervious, Inflow Depth = 4.20" for 10-year event

Inflow 7.51 cfs @ 12.09 hrs. Volume= 0.575 af

2.47 cfs @ 12.38 hrs, Volume= Outflow = 0.552 af, Atten= 67%, Lag= 17.7 min

2.47 cfs @ 12.38 hrs, Volume= Primary 0.552 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 48.00' Surf.Area= 1,706 sf Storage= 128 cf

Peak Elev= 51.67' @ 12.38 hrs Surf.Area= 4,580 sf Storage= 11,205 cf (11,077 cf above start)

Flood Elev= 53.00' Surf.Area= 6,019 sf Storage= 18,236 cf (18,109 cf above start)

Avail.Storage Storage Description

Plug-Flow detention time= 303.7 min calculated for 0.549 af (95% of inflow)

Center-of-Mass det. time= 274.0 min (1,052.3 - 778.3)

#1	46.5	0'	18,236 c	f Custom Stage I	Data (Conic)Listed	below (Recalc)
Elevation	on	Surf.Area	Voids	Inc.Store	Cum.Store	Wet.Area
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	(sq-ft)
46.5	50	1,706	0.0	0	0	1,706
48.0	00	1,706	5.0	128	128	1,926
49.0	00	2,381	100.0	2,034	2,162	2,619
50.0	00	3,056	100.0	2,711	4,874	3,319
51.0	00	3,935	100.0	3,486	8,360	4,223
52.0		4,918	100.0	4,417	12,777	5,233
53.0	00	6,019	100.0	5,459	18,236	6,365
Device	Routing	In	vert Ou	ıtlet Devices		
#1	Primary	45	5.50' <b>18</b>	.0" Round Culvert		
				50.0' CPP, square	•	
						.0050 '/' Cc= 0.900
""				0.012, Flow Area=		
#2	Device 1	_		" Vert. Underdrain		
#3	Device 2	48				over Wetted area above 48.00'
<i>!! 4</i>	D : 4	50		cluded Wetted area		
#4	Device 1		-	)" W x 30.0" H Vert		
#5	Device 1	52		. <b>0" x 48.0" Horiz. C</b> nited to weir flow at		.600

Primary OutFlow Max=2.47 cfs @ 12.38 hrs HW=51.67' TW=45.64' (Dynamic Tailwater)

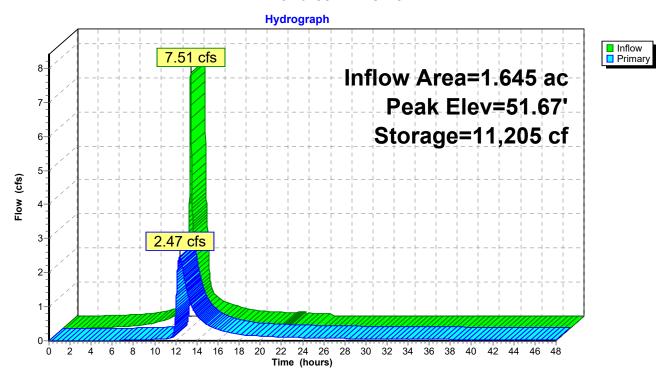
-1=Culvert (Passes 2.47 cfs of 19.81 cfs potential flow)

-2=Underdrain (Passes 0.16 cfs of 1.03 cfs potential flow)
-3=Exfiltration through Media (Exfiltration Controls 0.16 cfs)

-4=Orifice/Grate (Orifice Controls 2.31 cfs @ 4.15 fps)

-5=Orifice/Grate (Controls 0.00 cfs)

## Pond 69P: Bio #3



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## **Summary for Pond 80P: YD #24**

Inflow Area = 0.046 ac, 84.56% Impervious, Inflow Depth = 4.77" for 10-year event

Inflow = 0.24 cfs @ 12.08 hrs, Volume= 0.018 af

Outflow = 0.24 cfs @ 12.08 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min

Primary = 0.24 cfs @ 12.08 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

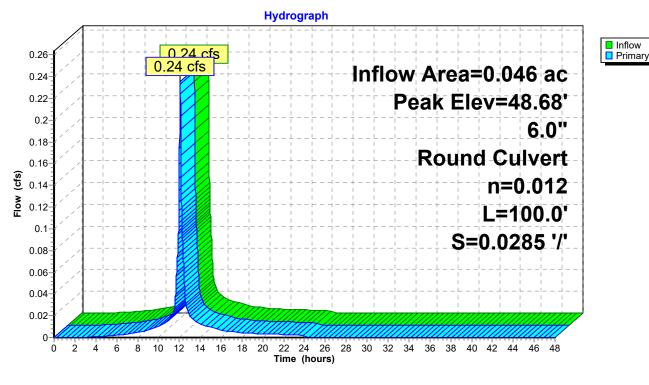
Peak Elev= 48.68' @ 12.10 hrs

Flood Elev= 52.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	48.35'	6.0" Round Culvert
			L= 100.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 48.35' / 45.50' S= 0.0285 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.20 sf

Primary OutFlow Max=0.23 cfs @ 12.08 hrs HW=48.67' TW=47.91' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.23 cfs @ 2.42 fps)

## Pond 80P: YD #24



## Summary for Pond 81P: 6" CPP

Inflow Area = 0.028 ac,100.00% Impervious, Inflow Depth = 5.23" for 10-year event

Inflow = 0.15 cfs @ 12.08 hrs, Volume= 0.012 af

Outflow = 0.15 cfs @ 12.08 hrs, Volume= 0.012 af, Atten= 0%, Lag= 0.0 min

Primary = 0.15 cfs @ 12.08 hrs, Volume= 0.012 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

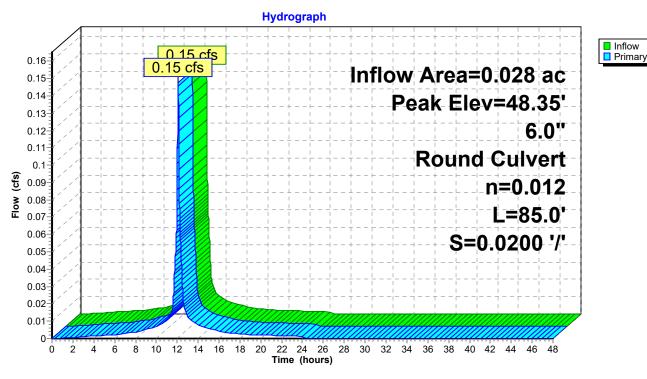
Peak Elev= 48.35' @ 12.12 hrs

Flood Elev= 52.25'

Device	Routing	Invert	Outlet Devices
#1	Primary	48.05'	6.0" Round Culvert
			L= 85.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 48.05' / 46.35' S= 0.0200 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.20 sf

Primary OutFlow Max=0.14 cfs @ 12.08 hrs HW=48.34' TW=47.97' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.14 cfs @ 1.72 fps)

## Pond 81P: 6" CPP



☐ Inflow☐ Primary

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## **Summary for Pond 82P: CB #23**

Inflow Area = 0.230 ac, 90.79% Impervious, Inflow Depth = 4.93" for 10-year event

Inflow = 1.21 cfs @ 12.08 hrs, Volume= 0.094 af

Outflow = 1.21 cfs @ 12.08 hrs, Volume= 0.094 af, Atten= 0%, Lag= 0.0 min

Primary = 1.21 cfs @ 12.08 hrs, Volume= 0.094 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

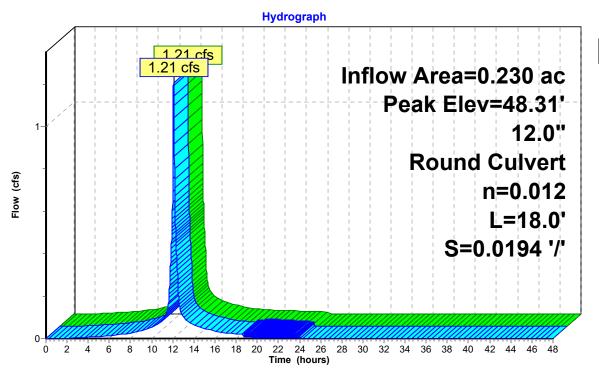
Peak Elev= 48.31' @ 12.40 hrs

Flood Elev= 49.85'

Device	Routing	Invert	Outlet Devices
#1	Primary	45.85'	12.0" Round Culvert
			L= 18.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 45.85' / 45.50' S= 0.0194 '/' Cc= 0.900
			n= 0.012. Flow Area= 0.79 sf

Primary OutFlow Max=0.95 cfs @ 12.08 hrs HW=47.97' TW=47.91' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.95 cfs @ 1.21 fps)

## Pond 82P: CB #23



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## Summary for Pond 83P: Bio #4

Inflow Area = 0.333 ac, 74.25% Impervious, Inflow Depth = 4.53" for 10-year event

Inflow 1.63 cfs @ 12.08 hrs, Volume= 0.126 af

0.50 cfs @ 12.40 hrs, Volume= Outflow = 0.125 af, Atten= 69%, Lag= 18.9 min

0.50 cfs @ 12.40 hrs, Volume= Primary 0.125 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 45.50' Surf.Area= 315 sf Storage= 24 cf

Peak Elev= 48.30' @ 12.40 hrs Surf.Area= 1,345 sf Storage= 2,203 cf (2,179 cf above start)

Flood Elev= 49.00' Surf.Area= 1,691 sf Storage= 3,270 cf (3,247 cf above start)

Plug-Flow detention time= 216.0 min calculated for 0.125 af (99% of inflow)

Center-of-Mass det. time= 208.3 min ( 980.2 - 771.9 )

Volume	Inve	ert Ava	il.Storaç	je Storage Descr	iption	
#1	44.0	0'	3,270	cf Custom Stage	e Data (Prismatio	Listed below (Recalc)
Clayetie	<b>.</b> .	Curf Area	Voido	Ina Ctara	Cum Stara	
Elevation		Surf.Area	Voids	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
44.(	00	315	0.0	0	0	
45.5	50	315	5.0	24	24	
46.0	00	451	100.0	192	215	
47.0		785	100.0	618	833	
48.0		1,199	100.0	992	1,825	
49.0		1,691	100.0	1,445	3,270	
49.0	30	1,091	100.0	1,445	3,270	
Device	Routing	In	vert C	outlet Devices		
#1	Primary			5.0" Round Culve	ort	_
$\pi$ 1	1 IIIIIai y	70		= 26.0' CPP, squa		L Ko- 0 500
						S= 0.0058 '/' Cc= 0.900
				= 0.012, Flow Area		
#2	Device 1	43	3.00' <b>4</b>	.0" Vert. Underdra	ain C= 0.600	
#3	Device 2	45	5.50' <b>2</b>	.500 in/hr Exfiltrat	tion through Med	lia over Surface area above 45.50'
			Е	xcluded Surface a	rea = 315 sf Phas	se-In= 0.01'
#4	Device 1	47	'.05' <b>4</b>	4.0" Vert. Orifice/Grate C= 0.600		
#5	Device 1			4.0" x 24.0" Horiz		C= 0.600
110	D 0 1 100 1	7.0	<u>L</u>	T.V A 2-7.0	. Ormoo, Orate	0.000

Primary OutFlow Max=0.50 cfs @ 12.40 hrs HW=48.30' TW=42.90' (Dynamic Tailwater)

Limited to weir flow at low heads

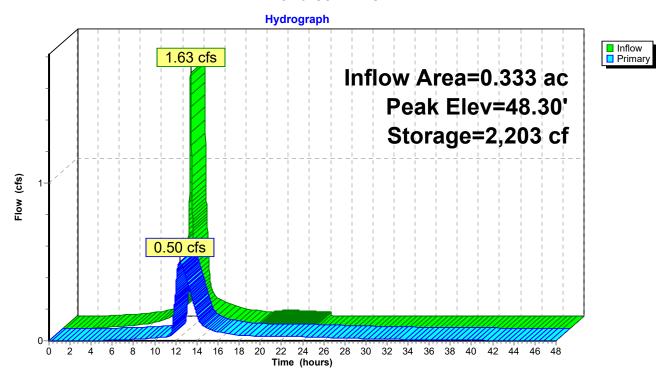
-1=Culvert (Passes 0.50 cfs of 12.77 cfs potential flow)

<sup>2=</sup>Underdrain (Passes 0.06 cfs of 0.95 cfs potential flow)
3=Exfiltration through Media (Exfiltration Controls 0.06 cfs)

**<sup>-4=</sup>Orifice/Grate** (Orifice Controls 0.44 cfs @ 5.00 fps)

<sup>-5=</sup>Orifice/Grate (Controls 0.00 cfs)

## Pond 83P: Bio #4



# Summary for Link 100L: POA #100 - SW

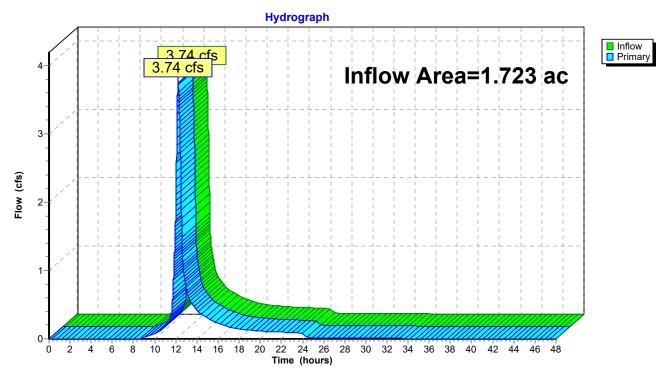
Inflow Area = 1.723 ac, 14.18% Impervious, Inflow Depth > 2.96" for 10-year event

Inflow = 3.74 cfs @ 12.22 hrs, Volume= 0.424 af

Primary = 3.74 cfs @ 12.22 hrs, Volume= 0.424 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

## Link 100L: POA #100 - SW



# Summary for Link 200L: POA #200 - South

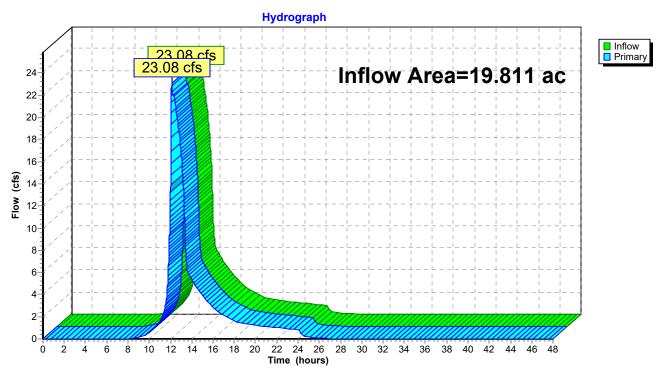
Inflow Area = 19.811 ac, 10.04% Impervious, Inflow Depth = 2.73" for 10-year event

Inflow = 23.08 cfs @ 12.12 hrs, Volume= 4.509 af

Primary = 23.08 cfs @ 12.12 hrs, Volume= 4.509 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 200L: POA #200 - South



# Summary for Link 300L: POA #300 - SE

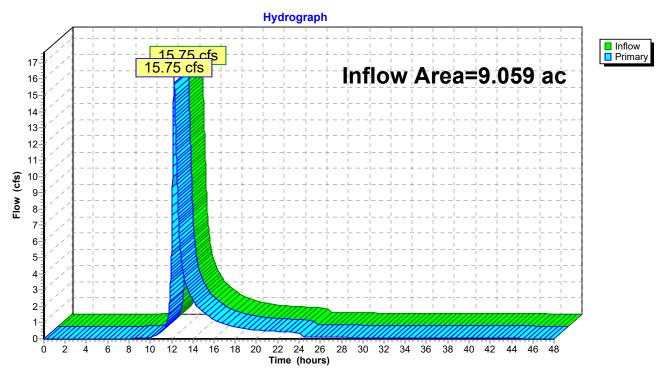
Inflow Area = 9.059 ac, 16.05% Impervious, Inflow Depth > 2.63" for 10-year event

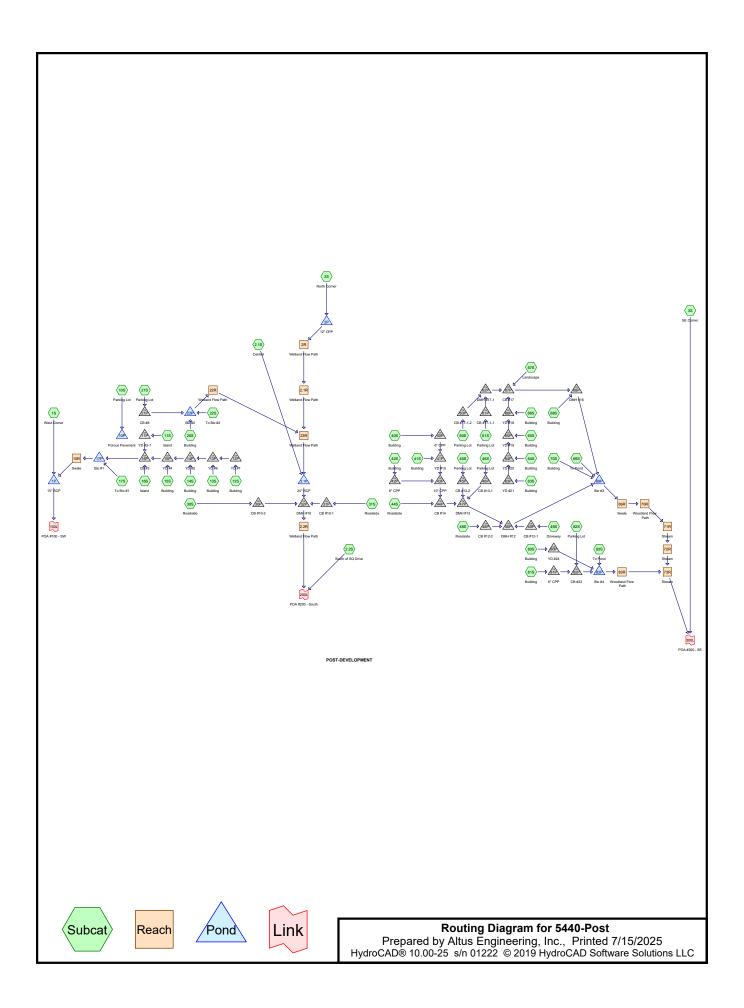
Inflow = 15.75 cfs @ 12.24 hrs, Volume= 1.987 af

Primary = 15.75 cfs @ 12.24 hrs, Volume= 1.987 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 300L: POA #300 - SE





Runoff Area=3,961 sf 0.00% Impervious Runoff Depth=3.98"

Tc=6.0 min CN=74 Runoff=0.42 cfs 0.030 af

Subcatchment 22S: To Bio #2

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=65,016 sf 9.83% Impervious Runoff Depth=4.09" Subcatchment 1S: West Corner Flow Length=366' Tc=9.8 min CN=75 Runoff=6.29 cfs 0.508 af Runoff Area=445,535 sf 8.04% Impervious Runoff Depth=3.87" Subcatchment 2.1S: Central Flow Length=1,341' Tc=15.8 min CN=73 Runoff=34.43 cfs 3.303 af Runoff Area=102,088 sf 10.13% Impervious Runoff Depth=4.30" Subcatchment 2.2S: South of SQ Drive Flow Length=391' Tc=6.0 min CN=77 Runoff=11.79 cfs 0.840 af Runoff Area=284,221 sf 6.78% Impervious Runoff Depth=3.77" Subcatchment 2S: North Corner Tc=0.0 min CN=72 Runoff=35.33 cfs 2.050 af Runoff Area=308,423 sf 2.18% Impervious Runoff Depth=3.35" Subcatchment 3S: SE Corner Flow Length=1,149' Tc=15.9 min CN=68 Runoff=20.46 cfs 1.979 af Runoff Area=10,178 sf 99.02% Impervious Runoff Depth>6.65" Subcatchment 10S: Parking Lot Tc=790.0 min CN=98 Runoff=0.11 cfs 0.130 af Runoff Area=588 sf 65.82% Impervious Runoff Depth=5.75" Subcatchment 11S: Island Tc=6.0 min CN=90 Runoff=0.09 cfs 0.006 af Runoff Area=1,878 sf 65.12% Impervious Runoff Depth=5.75" Subcatchment 12S: Building Tc=6.0 min CN=90 Runoff=0.27 cfs 0.021 af Runoff Area=1,349 sf 73.83% Impervious Runoff Depth=5.99" Subcatchment 13S: Building Tc=6.0 min CN=92 Runoff=0.20 cfs 0.015 af Runoff Area=1,022 sf 77.79% Impervious Runoff Depth=6.10" Subcatchment 14S: Building Tc=6.0 min CN=93 Runoff=0.15 cfs 0.012 af Runoff Area=1,377 sf 43.21% Impervious Runoff Depth=5.07" Subcatchment 15S: Building Tc=6.0 min CN=84 Runoff=0.18 cfs 0.013 af Runoff Area=928 sf 26.51% Impervious Runoff Depth=4.63" Subcatchment 16S: Island Tc=6.0 min CN=80 Runoff=0.11 cfs 0.008 af Subcatchment 17S: To Bio #1 Runoff Area=2,893 sf 0.28% Impervious Runoff Depth=3.98" Tc=6.0 min CN=74 Runoff=0.31 cfs 0.022 af Runoff Area=9,167 sf 100.00% Impervious Runoff Depth=6.69" Subcatchment 20S: Building Tc=6.0 min CN=98 Runoff=1.43 cfs 0.117 af Runoff Area=2,620 sf 100.00% Impervious Runoff Depth=6.69" **Subcatchment 21S: Parking Lot** Tc=6.0 min CN=98 Runoff=0.41 cfs 0.034 af

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Subcatchment30S: Roadside	Runoff Area=8,230 sf 53.10% Impervious Runoff Depth=5.41" Flow Length=204' Tc=6.0 min CN=87 Runoff=1.15 cfs 0.085 af
Subcatchment31S: Roadside	Runoff Area=7,135 sf 71.11% Impervious Runoff Depth=5.87" Flow Length=143' Tc=6.0 min CN=91 Runoff=1.06 cfs 0.080 af
Subcatchment40S: Building	Runoff Area=3,066 sf 100.00% Impervious Runoff Depth=6.69" Tc=6.0 min CN=98 Runoff=0.48 cfs 0.039 af
Subcatchment41S: Building	Runoff Area=2,120 sf 90.94% Impervious Runoff Depth=6.45" Tc=6.0 min CN=96 Runoff=0.33 cfs 0.026 af
Subcatchment42S: Building	Runoff Area=2,162 sf 100.00% Impervious Runoff Depth=6.69" Tc=6.0 min CN=98 Runoff=0.34 cfs 0.028 af
Subcatchment44S: Roadside	Runoff Area=4,663 sf 40.92% Impervious Runoff Depth=5.07" Tc=6.0 min CN=84 Runoff=0.62 cfs 0.045 af
Subcatchment45S: Parking Lot	Runoff Area=3,851 sf 71.88% Impervious Runoff Depth=5.87" Tc=6.0 min CN=91 Runoff=0.57 cfs 0.043 af
Subcatchment46S: Parking Lot	Runoff Area=4,489 sf 73.25% Impervious Runoff Depth=5.99" Tc=6.0 min CN=92 Runoff=0.67 cfs 0.051 af
Subcatchment48S: Roadside	Runoff Area=3,415 sf 55.67% Impervious Runoff Depth=5.53" Tc=6.0 min CN=88 Runoff=0.49 cfs 0.036 af
Subcatchment49S: Driveway	Runoff Area=3,652 sf 83.90% Impervious Runoff Depth=6.10" Tc=6.0 min CN=93 Runoff=0.55 cfs 0.043 af
Subcatchment 60S: Parking Lot	Runoff Area=9,169 sf 78.19% Impervious Runoff Depth=6.10" Flow Length=116' Tc=6.0 min CN=93 Runoff=1.39 cfs 0.107 af
Subcatchment 61S: Parking Lot	Runoff Area=7,068 sf 91.98% Impervious Runoff Depth=6.45" Flow Length=111' Tc=6.0 min CN=96 Runoff=1.09 cfs 0.087 af
Subcatchment 63S: Building	Runoff Area=1,459 sf 65.52% Impervious Runoff Depth=5.75" Tc=6.0 min CN=90 Runoff=0.21 cfs 0.016 af
Subcatchment 64S: Building	Runoff Area=1,506 sf 81.27% Impervious Runoff Depth=6.22" Tc=6.0 min CN=94 Runoff=0.23 cfs 0.018 af
Subcatchment 65S: Building	Runoff Area=982 sf 80.86% Impervious Runoff Depth=6.10" Tc=6.0 min CN=93 Runoff=0.15 cfs 0.011 af
Subcatchment 66S: Building	Runoff Area=1,478 sf 44.79% Impervious Runoff Depth=4.85" Tc=6.0 min CN=82 Runoff=0.19 cfs 0.014 af
Subcatchment 67S: Landscape	Runoff Area=1,511 sf 10.32% Impervious Runoff Depth=2.95" Tc=6.0 min CN=64 Runoff=0.12 cfs 0.009 af
Subcatchment 68S: Building	Runoff Area=1,370 sf 100.00% Impervious Runoff Depth=6.69" Tc=6.0 min CN=98 Runoff=0.21 cfs 0.018 af

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Runoff Area=12,794 sf 0.00% Impervious Runoff Depth=3.46" Subcatchment 69S: To Pond

Tc=6.0 min CN=69 Runoff=1.19 cfs 0.085 af

Subcatchment 70S: Building Runoff Area=6,905 sf 100.00% Impervious Runoff Depth=6.69"

Tc=6.0 min CN=98 Runoff=1.08 cfs 0.088 af

Runoff Area=1,982 sf 84.56% Impervious Runoff Depth=6.22" Subcatchment 80S: Building

Tc=6.0 min CN=94 Runoff=0.30 cfs 0.024 af

Subcatchment81S: Building Runoff Area=1,200 sf 100.00% Impervious Runoff Depth=6.69"

Tc=6.0 min CN=98 Runoff=0.19 cfs 0.015 af

Runoff Area=8,819 sf 89.53% Impervious Runoff Depth=6.34" Subcatchment 82S: Parking Lot

Flow Length=214' Tc=6.0 min CN=95 Runoff=1.35 cfs 0.107 af

Runoff Area=2,507 sf 0.00% Impervious Runoff Depth=3.98" Subcatchment 83S: To Pond

Tc=6.0 min CN=74 Runoff=0.27 cfs 0.019 af

Avg. Flow Depth=1.53' Max Vel=2.91 fps Inflow=31.17 cfs 2.050 af Reach 2.1R: Wetland Flow Path

n=0.040 L=344.0' S=0.0075'/' Capacity=54.59 cfs Outflow=29.25 cfs 2.050 af

Avg. Flow Depth=0.86' Max Vel=5.45 fps Inflow=22.19 cfs 5.697 af Reach 2.2R: Wetland Flow Path

n=0.040 L=263.0' S=0.0502 '/' Capacity=141.18 cfs Outflow=21.54 cfs 5.697 af

Avg. Flow Depth=1.05' Max Vel=5.74 fps Inflow=31.29 cfs 2.050 af Reach 2R: Wetland Flow Path

n=0.040 L=151.0' S=0.0446 '/' Capacity=133.09 cfs Outflow=31.17 cfs 2.050 af

Avg. Flow Depth=0.13' Max Vel=0.72 fps Inflow=0.40 cfs 0.098 af Reach 10R: Swale

n=0.035 L=44.0' S=0.0050 '/' Capacity=16.22 cfs Outflow=0.40 cfs 0.098 af

Avg. Flow Depth=0.09' Max Vel=1.11 fps Inflow=1.15 cfs 0.180 af Reach 22R: Wetland Flow Path

n=0.040 L=211.0' S=0.0245'/' Capacity=392.58 cfs Outflow=1.09 cfs 0.180 af

Avg. Flow Depth=1.25' Max Vel=4.09 fps Inflow=29.59 cfs 2.229 af Reach 23R: Wetland Flow Path

n=0.040 L=131.0' S=0.0185'/' Capacity=85.86 cfs Outflow=29.49 cfs 2.229 af

Avg. Flow Depth=0.49' Max Vel=1.36 fps Inflow=3.63 cfs 0.740 af Reach 69R: Swale

n=0.069 L=17.0' S=0.0147'/' Capacity=14.11 cfs Outflow=3.63 cfs 0.740 af

Avg. Flow Depth=0.40' Max Vel=0.64 fps Inflow=3.63 cfs 0.740 af Reach 70R: Woodland Flow Path

n=0.400 L=57.0' S=0.1404 '/' Capacity=21.20 cfs Outflow=3.63 cfs 0.740 af

Reach 71R: Stream Avg. Flow Depth=0.34' Max Vel=3.47 fps Inflow=3.63 cfs 0.740 af

n=0.040 L=80.0' S=0.0554 '/' Capacity=31.12 cfs Outflow=3.63 cfs 0.740 af

Reach 72R: Stream Avg. Flow Depth=0.35' Max Vel=2.04 fps Inflow=3.63 cfs 0.740 af

n=0.040 L=88.0' S=0.0160 '/' Capacity=25.40 cfs Outflow=3.63 cfs 0.740 af

Avg. Flow Depth=0.40' Max Vel=2.18 fps Inflow=4.49 cfs 0.904 af Reach 73R: Stream

n=0.040 L=309.0' S=0.0160 '/' Capacity=25.38 cfs Outflow=4.47 cfs 0.904 af

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Reach 83R: Woodland Flow Path n=0.400         Avg. Flow Depth=0.20'         Max Vel=0.36 fps         Inflow=0.97 cfs         0.164 af           L=122.0'         S=0.0950 '/'         Capacity=17.44 cfs         Outflow=0.86 cfs         0.164 af						
Pond 1P: 15" RCP	Peak Elev=53.82' Storage=1,539 cf Inflow=6.63 cfs 0.606 af 15.0" Round Culvert n=0.012 L=60.0' S=0.0037 '/' Outflow=4.75 cfs 0.606 af					
Pond 2.1P: 24" RCP	Peak Elev=52.28' Storage=49,734 cf Inflow=51.33 cfs 5.532 af 24.0" Round Culvert n=0.012 L=17.0' S=0.0135 '/' Outflow=21.90 cfs 5.532 af					
Pond 2P: 12" CPP	Peak Elev=61.01' Storage=13,034 cf Inflow=35.33 cfs 2.050 af Outflow=31.29 cfs 2.050 af					
Pond 10P: Porous Pavement	Peak Elev=3.14' Storage=2,501 cf Inflow=0.11 cfs 0.130 af Outflow=0.04 cfs 0.105 af					
Pond 11P: YD #3-1	Peak Elev=58.23' Inflow=0.09 cfs 0.006 af 6.0" Round Culvert n=0.012 L=36.0' S=0.0050 '/' Outflow=0.09 cfs 0.006 af					
Pond 12P: YD #7	Peak Elev=58.25' Inflow=0.27 cfs 0.021 af 8.0" Round Culvert n=0.012 L=52.0' S=0.0050 '/' Outflow=0.27 cfs 0.021 af					
Pond 13P: YD #6	Peak Elev=58.24' Inflow=0.48 cfs 0.036 af 10.0" Round Culvert n=0.012 L=29.0' S=0.0052 '/' Outflow=0.48 cfs 0.036 af					
Pond 14P: YD #5	Peak Elev=58.23' Inflow=0.63 cfs 0.048 af 10.0" Round Culvert n=0.012 L=20.0' S=0.0050 '/' Outflow=0.63 cfs 0.048 af					
Pond 15P: YD #4	Peak Elev=58.23' Inflow=0.81 cfs 0.061 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.81 cfs 0.061 af					
Pond 16P: CB #3	Peak Elev=58.23' Inflow=1.02 cfs 0.076 af 12.0" Round Culvert n=0.012 L=45.0' S=0.0049 '/' Outflow=1.02 cfs 0.076 af					
Pond 17P: Bio #1	Peak Elev=58.22' Storage=1,786 cf Inflow=1.32 cfs 0.098 af Outflow=0.40 cfs 0.098 af					
Pond 21P: CB #8	Peak Elev=59.59' Inflow=0.41 cfs 0.034 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0050 '/' Outflow=0.41 cfs 0.034 af					
Pond 22P: Bio #2	Peak Elev=59.59' Storage=3,011 cf Inflow=2.26 cfs 0.181 af Outflow=1.15 cfs 0.180 af					
Pond 30P: CB #10-2	Peak Elev=53.21' Inflow=1.15 cfs 0.085 af 12.0" Round Culvert n=0.012 L=78.0' S=0.0397 '/' Outflow=1.15 cfs 0.085 af					
Pond 31P: CB #10-1	Peak Elev=50.44' Inflow=1.06 cfs 0.080 af 12.0" Round Culvert n=0.012 L=2.0' S=0.0250 '/' Outflow=1.06 cfs 0.080 af					
Pond 32P: DMH #10	Peak Elev=50.44' Inflow=22.19 cfs 5.697 af 24.0" Round Culvert n=0.012 L=57.0' S=0.0135 '/' Outflow=22.19 cfs 5.697 af					
Pond 40P: 6" CPP	Peak Elev=54.86' Inflow=0.48 cfs 0.039 af 6.0" Round Culvert n=0.012 L=174.0' S=0.0150 '/' Outflow=0.48 cfs 0.039 af					

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Pond 41P: YD #15	Peak Elev=53.85' Inflow=0.81 cfs 0.065 af 8.0" Round Culvert n=0.012 L=47.0' S=0.0149 '/' Outflow=0.81 cfs 0.065 af
Pond 42P: 6" CPP	Peak Elev=54.05' Inflow=0.34 cfs 0.028 af 6.0" Round Culvert n=0.012 L=150.0' S=0.0175 '/' Outflow=0.34 cfs 0.028 af
Pond 43P: 10" CPP	Peak Elev=53.60' Inflow=1.14 cfs 0.093 af 8.0" Round Culvert n=0.012 L=33.0' S=0.0148 '/' Outflow=1.14 cfs 0.093 af
Pond 44P: CB #14	Peak Elev=53.17' Inflow=1.77 cfs 0.138 af 12.0" Round Culvert n=0.012 L=31.0' S=0.0048 '/' Outflow=1.77 cfs 0.138 af
Pond 45P: CB #13-2	Peak Elev=52.99' Inflow=0.57 cfs 0.043 af 12.0" Round Culvert n=0.012 L=22.0' S=0.0245 '/' Outflow=0.57 cfs 0.043 af
Pond 46P: CB #13-1	Peak Elev=53.00' Inflow=0.67 cfs 0.051 af 12.0" Round Culvert n=0.012 L=12.0' S=0.0325 '/' Outflow=0.67 cfs 0.051 af
Pond 47P: DMH #13	Peak Elev=52.97' Inflow=3.01 cfs 0.233 af 12.0" Round Culvert n=0.012 L=67.0' S=0.0051 '/' Outflow=3.01 cfs 0.233 af
Pond 48P: CB #12-2	Peak Elev=52.33' Inflow=0.49 cfs 0.036 af 12.0" Round Culvert n=0.012 L=6.0' S=0.0050 '/' Outflow=0.49 cfs 0.036 af
Pond 49P: CB #12-1	Peak Elev=52.33' Inflow=0.55 cfs 0.043 af 12.0" Round Culvert n=0.012 L=46.0' S=0.0050 '/' Outflow=0.55 cfs 0.043 af
Pond 50P: DMH #12	Peak Elev=52.32' Inflow=4.05 cfs 0.312 af 15.0" Round Culvert n=0.012 L=106.0' S=0.0040 '/' Outflow=4.05 cfs 0.312 af
Pond 60P: CB #17-1-2	Peak Elev=54.38' Inflow=1.39 cfs 0.107 af 12.0" Round Culvert n=0.012 L=21.0' S=0.0052 '/' Outflow=1.39 cfs 0.107 af
Pond 61P: CB #17-1-1	Peak Elev=54.34' Inflow=1.09 cfs 0.087 af 12.0" Round Culvert n=0.012 L=3.0' S=0.0367 '/' Outflow=1.09 cfs 0.087 af
Pond 62P: DMH #17-1	Peak Elev=54.26' Inflow=2.48 cfs 0.194 af 12.0" Round Culvert n=0.012 L=25.0' S=0.0052 '/' Outflow=2.48 cfs 0.194 af
Pond 63P: YD #21	Peak Elev=53.98' Inflow=0.21 cfs 0.016 af 12.0" Round Culvert n=0.012 L=49.0' S=0.0049 '/' Outflow=0.21 cfs 0.016 af
Pond 64P: YD #20	Peak Elev=53.97' Inflow=0.44 cfs 0.034 af 10.0" Round Culvert n=0.012 L=35.0' S=0.0049 '/' Outflow=0.44 cfs 0.034 af
Pond 65P: YD #19	Peak Elev=53.95' Inflow=0.59 cfs 0.045 af 10.0" Round Culvert n=0.012 L=42.0' S=0.0050 '/' Outflow=0.59 cfs 0.045 af
Pond 66P: YD #18	Peak Elev=53.91' Inflow=0.78 cfs 0.059 af 12.0" Round Culvert n=0.012 L=11.0' S=0.0509 '/' Outflow=0.78 cfs 0.059 af

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Type III 24-hr 25-year Rainfall=6.93"

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Pond 67P: CB #17	Peak Elev=53.87'	Inflow=3.38 cfs 0.262 af
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12.0" Round Culvert n=0.012 L=74.0' S=0.0050 '/' Outflow=3.38 cfs 0.262 af

Pond 68P: DMH #16 Peak Elev=52.92' Inflow=3.59 cfs 0.280 af

12.0" Round Culvert n=0.012 L=90.0' S=0.0110 '/' Outflow=3.59 cfs 0.280 af

Pond 69P: Bio #3 Peak Elev=52.18' Storage=13,667 cf Inflow=9.90 cfs 0.764 af

Outflow=3.63 cfs 0.740 af

Pond 80P: YD #24 Peak Elev=48.78' Inflow=0.30 cfs 0.024 af

6.0" Round Culvert n=0.012 L=100.0' S=0.0285 '/' Outflow=0.30 cfs 0.024 af

Pond 81P: 6" CPP Peak Elev=48.62' Inflow=0.19 cfs 0.015 af

6.0" Round Culvert  $\,$  n=0.012 L=85.0' S=0.0200 '/' Outflow=0.19 cfs  $\,$  0.015 af

Pond 82P: CB #23 Peak Elev=48.60' Inflow=1.54 cfs 0.122 af

12.0" Round Culvert n=0.012 L=18.0' S=0.0194 '/' Outflow=1.54 cfs 0.122 af

Pond 83P: Bio #4 Peak Elev=48.56' Storage=2,578 cf Inflow=2.11 cfs 0.165 af

Outflow=0.97 cfs 0.164 af

Link 100L: POA #100 - SW Inflow=4.75 cfs 0.606 af

Primary=4.75 cfs 0.606 af

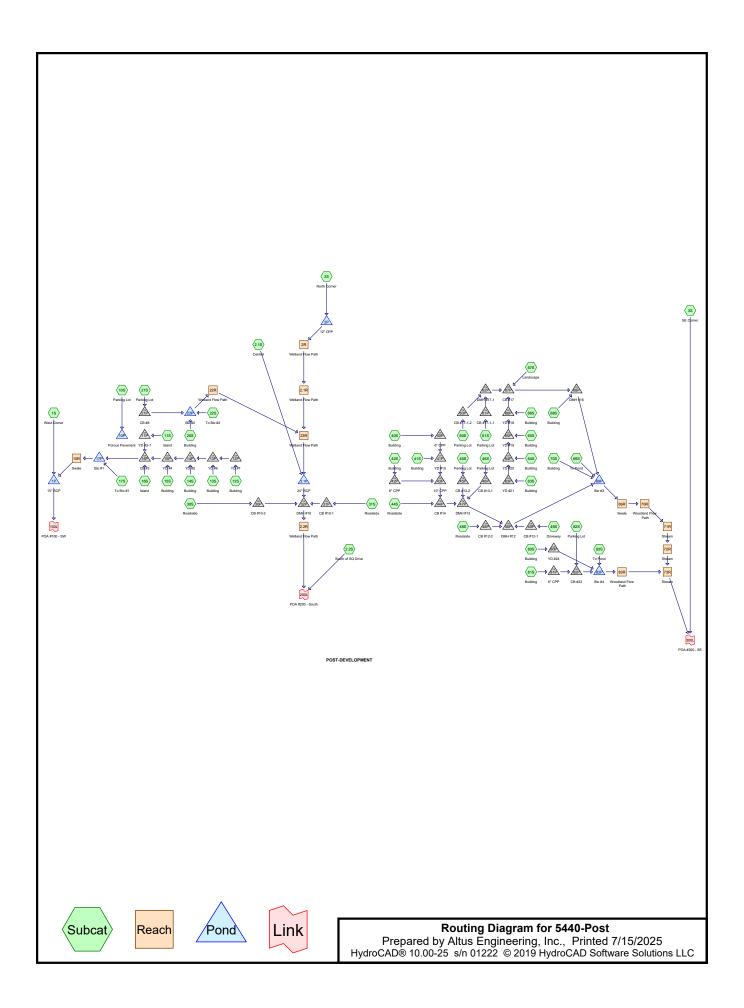
Link 200L: POA #200 - South Inflow=30.05 cfs 6.538 af

Primary=30.05 cfs 6.538 af

Link 300L: POA #300 - SE Inflow=24.24 cfs 2.882 af

Primary=24.24 cfs 2.882 af

Total Runoff Area = 30.826 ac Runoff Volume = 10.183 af Average Runoff Depth = 3.96" 87.29% Pervious = 26.907 ac 12.71% Impervious = 3.919 ac



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#### **Summary for Pond 17P: Bio #1**

[80] Warning: Exceeded Pond 16P by 0.84' @ 24.25 hrs (1.72 cfs 0.168 af)

Inflow Area = 0.230 ac, 42.35% Impervious, Inflow Depth = 7.99" for 100-year event

2.03 cfs @ 12.08 hrs, Volume= Inflow 0.153 af

0.66 cfs @ 12.38 hrs, Volume= Outflow = 0.153 af, Atten= 67%, Lag= 17.7 min

Primary 0.66 cfs @ 12.38 hrs, Volume= 0.153 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs. dt= 0.01 hrs

Starting Elev= 56.25' Surf.Area= 487 sf Storage= 37 cf

Peak Elev= 58.78' @ 12.38 hrs Surf.Area= 1,664 sf Storage= 2,627 cf (2,591 cf above start)

Flood Elev= 59.25' Surf.Area= 1,950 sf Storage= 3,480 cf (3,444 cf above start)

Plug-Flow detention time= 185.0 min calculated for 0.152 af (99% of inflow)

Center-of-Mass det. time= 176.0 min (957.2 - 781.2)

Volume	Inver	t Ava	il.Stora	age Storage Desc	e Storage Description							
#1	54.75	5'	3,480	of Custom Stag	<b>e Data (Conic)</b> List	ed below (Recalc)						
Elevatio		Surf.Area	Voids (%		Cum.Store (cubic-feet)	Wet.Area						
(fee		(sq-ft)		, , , , , , , , , , , , , , , , , , , ,		(sq-ft)						
	54.75 487 0.0				0	487						
56.2	25	487	5.0	37	37	604						
57.0	00	774	100.0	469	505	899						
58.0	00	1,239	100.0	997	1,503	1,377						
59.0		1,797	100.0		3,012	1,952						
	· · · · · · · · · · · · · · · · · · ·		100.0	•	3,480	2,110						
Device	Routing	In	vert	Outlet Devices								
#1	Primary	53	3.75'	15.0" Round Culv	ert							
	•			L= 30.0' CPP, squ	are edge headwall	, Ke= 0.500						
						= 0.0050 '/' Cc= 0.9	00					
				n= 0.012, Flow Are								
#2	Device 1	53		4.0" Vert. Underdr								
#3	Device 2		_			lia over Wetted area	ahove 56 25'					
#0	DCVICC 2	50		Excluded Wetted ar			4 4BOVC 00.20					
#4	Device 1	57		4.0" Vert. Orifice/G		J-111 - U.U I						
						- 0.600						
#5	Device 1	58	3.75'	<b>24.0" x 24.0" Horiz</b> Limited to weir flow		= 0.000						

Primary OutFlow Max=0.66 cfs @ 12.38 hrs HW=58.78' TW=53.77' (Dynamic Tailwater)

**-1=Culvert** (Passes 0.66 cfs of 12.40 cfs potential flow)

-2=Underdrain (Passes 0.07 cfs of 0.93 cfs potential flow)
-3=Exfiltration throiugh Media (Exfiltration Controls 0.07 cfs)

-4=Orifice/Grate (Orifice Controls 0.47 cfs @ 5.41 fps)

-5=Orifice/Grate (Weir Controls 0.12 cfs @ 0.54 fps)

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#### **Summary for Pond 22P: Bio #2**

[80] Warning: Exceeded Pond 21P by 0.75' @ 19.32 hrs (1.38 cfs 0.424 af)

Inflow Area = 0.362 ac, 74.85% Impervious, Inflow Depth = 8.94" for 100-year event

3.35 cfs @ 12.08 hrs, Volume= Inflow 0.269 af

Outflow 2.92 cfs @ 12.13 hrs, Volume= = 0.268 af, Atten= 13%, Lag= 2.7 min

2.92 cfs @ 12.13 hrs, Volume= Primary 0.268 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 57.75' Surf.Area= 1,027 sf Storage= 77 cf

Peak Elev= 59.70' @ 12.13 hrs Surf.Area= 2,292 sf Storage= 3,274 cf (3,197 cf above start)

Flood Elev= 60.00' Surf.Area= 2,511 sf Storage= 3,983 cf (3,906 cf above start)

Plug-Flow detention time= 168.1 min calculated for 0.266 af (99% of inflow)

Center-of-Mass det. time= 155.4 min (907.1 - 751.7)

Volume	Inve	t Ava	il.Storage	Storage Descrip	tion						
#1	56.25	5'	3,983 cf	Custom Stage I	Data (Conic)Listed	below (Recalc)					
Elevation (fee		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)					
56.2 57. 58.0	56.25       1,027       0.         57.75       1,027       5.         58.00       1,175       100.		0.0 5.0 100.0 100.0	0 77 275 1,481	0 77 352 1,833	1,027 1,197 1,348 1,997					
60.0	60.00 2,511 100			2,150	3,983	2,718					
Device	Routing	In	vert Out	let Devices							
#1	Primary	55	L= <sup>·</sup> Inle		e edge headwall,  K 5.25' / 55.16'   S= 0	e= 0.500 .0050 '/'     Cc= 0.900					
#2 #3	Device 1 Device 2		5.25' <b>4.0'</b> 7.75' <b>2.5</b> 0	' Vert. Underdrair 00 in/hr Exfiltratio	n C= 0.600	over Wetted area above	57.75'				
#4 #5											

Primary OutFlow Max=2.92 cfs @ 12.13 hrs HW=59.70' TW=55.31' (Dynamic Tailwater)

-1=Culvert (Passes 2.92 cfs of 11.56 cfs potential flow)

-2=Underdrain (Passes 0.07 cfs of 0.87 cfs potential flow)
-3=Exfiltration throiugh Media (Exfiltration Controls 0.07 cfs)

-4=Orifice/Grate (Orifice Controls 0.43 cfs @ 4.90 fps)

-5=Orifice/Grate (Weir Controls 2.42 cfs @ 1.48 fps)

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#### **Summary for Pond 69P: Bio #3**

[80] Warning: Exceeded Pond 50P by 1.72' @ 24.27 hrs (4.88 cfs 0.898 af) [80] Warning: Exceeded Pond 68P by 0.63' @ 24.37 hrs (1.17 cfs 0.057 af)

1.645 ac, 63.94% Impervious, Inflow Depth = 8.47" for 100-year event Inflow Area =

Inflow 14.86 cfs @ 12.08 hrs, Volume= 1.162 af

9.90 cfs @ 12.17 hrs, Volume= Outflow 1.137 af, Atten= 33%, Lag= 5.2 min

9.90 cfs @ 12.17 hrs, Volume= Primary 1.137 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

Starting Elev= 48.00' Surf.Area= 1,706 sf Storage= 128 cf

Peak Elev= 52.71' @ 12.17 hrs Surf.Area= 5,687 sf Storage= 16,535 cf (16,407 cf above start)

Flood Elev= 53.00' Surf.Area= 6,019 sf Storage= 18,236 cf (18,109 cf above start)

Plug-Flow detention time= 183.9 min calculated for 1.134 af (98% of inflow)

Center-of-Mass det. time= 167.5 min (933.2 - 765.6)

Volume	ne Invert Avail.Storage Storage Description											
#1	46.5	50'	18,236 c	Custom Stage	Data (Conic)Listed	below (Recalc)						
Elevation (fee		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)						
	46.50 1,706 0			0	1,706							
	48.00 1,706 5			128	0 128	1,926						
49.0	00	2,381	100.0	2,034	2,162	2,619						
50.0	00	3,056	100.0	2,711	4,874	3,319						
51.0	00	3,935	100.0	3,486	8,360	4,223						
52.0		4,918	100.0									
53.0	00	6,019	100.0	5,459	18,236	6,365						
Device	Routing	In	vert Ou	Outlet Devices								
#1	Primary	45	5.50' <b>18</b>	.0" Round Culver	t							
			L=	50.0' CPP, squar	e edge headwall, 🧍	(e= 0.500						
						0.0050 '/' Cc= 0.900						
				0.012, Flow Area								
#2	Device 1	_		)" Vert. Underdrai								
#3	<b>U</b>											
11.4	5 . 4	<b>5</b> 0			a = 1,926 sf Phase							
#4	Device 1				t. Orifice/Grate C							
#5	#5 Device 1 52.50' <b>48.0" x 48.0" Horiz. Orifice/Grate</b> C= 0.600  Limited to weir flow at low heads											

Primary OutFlow Max=9.89 cfs @ 12.17 hrs HW=52.71' TW=46.08' (Dynamic Tailwater) **1=Culvert** (Passes 9.89 cfs of 21.62 cfs potential flow)

-2=Underdrain (Passes 0.23 cfs of 1.08 cfs potential flow)

3=Exfiltration through Media (Exfiltration Controls 0.23 cfs)

-4=Orifice/Grate (Orifice Controls 4.67 cfs @ 5.60 fps)

-5=Orifice/Grate (Weir Controls 5.00 cfs @ 1.49 fps)

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#### Summary for Pond 83P: Bio #4

[80] Warning: Exceeded Pond 82P by 1.22' @ 24.13 hrs (3.22 cfs 0.357 af)

Inflow Area = 0.333 ac, 74.25% Impervious, Inflow Depth = 8.89" for 100-year event

3.12 cfs @ 12.08 hrs, Volume= Inflow 0.247 af

0.246 af, Atten= 11%, Lag= 2.5 min Outflow = 2.76 cfs @ 12.13 hrs, Volume=

Primary 2.76 cfs @ 12.13 hrs, Volume= 0.246 af

Routing by Dvn-Stor-Ind method. Time Span= 0.00-48.00 hrs. dt= 0.01 hrs

Starting Elev= 45.50' Surf.Area= 315 sf Storage= 24 cf

Peak Elev= 48.69' @ 12.13 hrs Surf.Area= 1,539 sf Storage= 2,771 cf (2,747 cf above start)

Flood Elev= 49.00' Surf.Area= 1,691 sf Storage= 3,270 cf (3,247 cf above start)

Plug-Flow detention time= 140.8 min calculated for 0.246 af (100% of inflow)

Center-of-Mass det. time= 136.3 min (895.4 - 759.1)

Volume	Inver	t Ava	Avail.Storage Storage Description											
#1	44.00	)'	3,270 cf	Custom Stage	Data (Prismatio	Listed below (Recalc)								
	_													
Elevation		Surf.Area	Voids	Inc.Store	Cum.Store									
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)									
44.0			0.0	0	0									
45.5	50	315	5.0	24	24									
46.0	00	451	100.0	192	215									
47.0	00	785	100.0	618	833									
48.0	00	1,199	100.0	992	1,825									
49.0	· ·		100.0	1,445	3,270									
Device	Routing	In	vert Ou	tlet Devices										
#1	Primary	43	3.00' <b>15</b> .	0" Round Culve	rt									
			L=	26.0' CPP, squa	re edge headwal	I, Ke= 0.500								
			Inle	et / Outlet Invert=	43.00 <sup>°</sup> / 42.85' S	S= 0.0058 '/' Cc= 0.900								
			n=	0.012, Flow Area	n= 1.23 sf									
#2	Device 1	43	3.00' <b>4.0</b>	" Vert. Underdra	in C= 0.600									
#3	Device 2	45	5.50' <b>2.5</b>	00 in/hr Exfiltrati	on through Med	lia over Surface area above 45.50'								
				cluded Surface are										
#4	Device 1	47	'.05' <b>4.0</b>	" Vert. Orifice/Gr	rate C= 0.600									
#5	#5 Device 1 48.50' <b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads													

Primary OutFlow Max=2.76 cfs @ 12.13 hrs HW=48.69' TW=43.05' (Dynamic Tailwater)

**-1=Culvert** (Passes 2.76 cfs of 13.30 cfs potential flow)

**-2=Underdrain** (Passes 0.07 cfs of 0.99 cfs potential flow) **3=Exfiltration through Media** (Exfiltration Controls 0.07 cfs)

-4=Orifice/Grate (Orifice Controls 0.51 cfs @ 5.85 fps)

-5=Orifice/Grate (Weir Controls 2.18 cfs @ 1.43 fps)

## Section 5

## Precipitation Table



### **Extreme Precipitation Tables**

#### **Northeast Regional Climate Center**

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

	Metadata for Point									
Smoothing	Yes									
State	New Hampshire									
Location	New Hampshire, United States									
Latitude	43.141 degrees North									
Longitude	70.907 degrees West									
Elevation	10 feet									
Date/Time	Tue Apr 15 2025 15:34:24 GMT-0400 (Eastern Daylight Time)									

#### **Extreme Precipitation Estimates**

			· Pro									- 1		1						
	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12h	· 24hr	+15%	1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.65	0.81	1.03							2.61	2	2.31	2.74	3.14	3.87	4.44	1yr
2yr	0.32	0.49	0.61	0.81	1.01	1.29	2yr	0.88	1.17	1.50	1.91	2.45	3.14	3.61	2.78	3.35	3.85	4.58	5.21	2yr
5yr	0.37	0.57	0.72	0.96	1.23	1.58	5yr	1.06	1.44	1.85	2.39	3.08	3.98	A	3.52	4.30	4.91	5.80	6.56	5yr
10yr	0.40	0.63	0.80	1.09	1.42	1.85	10yr	1.22	1.69	2.18	2.83	3.67	4.76	5.47	4.21	5.19	5.91	6.93	7.81	10yr
25yr	0.46	0.74	0.94	1.29	1.72	2.27	25yr	1.48	2.09	2.70	3.53	4.62	6.03	6.93	5.34	6.66	7.55	8.78	9.83	25yr
50yr	0.51	0.83	1.06	1.48	1.99	2.66	50yr	1.72	2.46	3.18	4.19	5.51	7.22	8.30	6.39	8.05	9.09	10.51	11.72	50yr
100yı	0.58	0.93	1.20	1.70	2.31	3.12	100yr	2.00	2.89	3.74	4.97	6.56	8.64	9.94	r 7.65	9.73	10.94	12.58	13.96	100yr
200yı	0.64	1.04	1.35	1.94	2.69	3.66	200yr	2.32	3.40	4.42	5.90	7.83	10.35	12.24 200 <sub>3</sub>	yr 9.16	11.77	13.18	15.07	16.65	200yr
500yı	0.75	1.24	1.61	2.34	3.29	4.52	500yr	2.84	4.22	5.49	7.39	9.88	13.15	15.74 500 <u>y</u>	yr 11.64	15.14	16.87	19.14	21.03	500yr

#### **Lower Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.24	0.37	0.45	0.60	0.74	0.90	1yr	0.64	0.88	0.91	1.27	1.58	2.06	2.50	1yr	1.82	2.41	2.90	3.27	4.00	1yr
2yr	0.31	0.49	0.60	0.81	1.00	1.18	2yr	0.86	1.16	1.36	1.83	2.36	3.04	3.39	2yr	2.69	3.26	3.74	4.46	5.05	2yr
5yr	0.35	0.54	0.67	0.91	1.16	1.40	5yr	1.00	1.37	1.61	2.15	2.78	3.72	4.13	5yr	3.29	3.98	4.60	5.43	6.14	5yr
10yr	0.38	0.59	0.73	1.02	1.32	1.60	10yr	1.14	1.56	1.82	2.45	3.13	4.30	4.81	10yr	3.80	4.63	5.34	6.29	7.07	10yr
25yr	0.44	0.66	0.83	1.18	1.55	1.91	25yr	1.34	1.87	2.11	2.84	3.65	4.98	5.85	25yr	4.41	5.63	6.53	7.66	8.54	25yr
50yr	0.48	0.73	0.91	1.31	1.76	2.18	50yr	1.52	2.13	2.36	3.20	4.10	5.70	6.77	50yr	5.05	6.51	7.60	8.87	9.83	50yr
100yr	0.54	0.81	1.02	1.47	2.02	2.50	100yr	1.74	2.44	2.64	3.58	4.58	6.51	7.84	100yr	5.76	7.54	8.86	10.29	11.30	100yr
200yr	0.60	0.90	1.14	1.65	2.29	2.86	200yr	1.98	2.79	2.94	4.01	5.12	7.43	9.08	200yr	6.57	8.73	10.33	11.94	13.02	200yr
500yr	0.70	1.04	1.33	1.94	2.75	3.44	500yr	2.38	3.36	3.41	4.64	5.95	8.82	11.01	500yr	7.80	10.59	12.66	14.55	15.64	500yr

#### **Upper Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.43	0.53	0.71	0.88	1.08	1yr	0.76	1.05	1.24	1.75	2.22	2.86	3.05	1yr	2.53	2.93	3.40	4.20	4.80	1yr
2yr	0.33	0.51	0.62	0.85	1.04	1.25	2yr	0.90	1.22	1.47	1.96	2.51	3.28	3.59	2yr	2.90	3.45	3.96	4.72	5.42	2yr
5yr	0.39	0.60	0.75	1.03	1.31	1.58	5yr	1.13	1.55	1.86	2.50	3.20	4.24	4.79	5yr	3.75	4.61	5.24	6.18	6.95	5yr
10yr	0.46	0.70	0.87	1.21	1.57	1.92	10yr	1.35	1.88	2.23	3.05	3.86	5.22	5.97	10yr	4.62	5.75	6.53	7.59	8.48	10yr
25yr	0.55	0.84	1.05	1.50	1.97	2.48	25yr	1.70	2.42	2.88	3.97	4.95	7.11	8.00	25yr	6.29	7.70	8.67	9.98	11.05	25yr
50yr	0.64	0.97	1.21	1.74	2.34	3.00	50yr	2.02	2.93	3.49	4.85	6.01	8.81	10.00	50yr	7.79	9.62	10.77	12.26	13.51	50yr
100yr	0.74	1.12	1.41	2.03	2.79	3.62	100yr	2.41	3.54	4.24	5.93	7.31	10.91	12.50	100yr	9.65	12.02	13.36	15.09	16.54	100yr
200yr	0.86	1.30	1.64	2.38	3.32	4.39	200yr	2.86	4.29	5.15	7.26	8.87	13.55	15.65	200yr	11.99	15.05	16.59	18.56	20.27	200yr
500yr	1.05	1.57	2.01	2.93	4.16	5.64	500yr	3.59	5.52	6.65	9.52	11.49	18.09	21.05	500yr	16.01	20.24	22.09	24.44	26.53	500yr

## Section 6

NRCS Soils Report Site Specific Soil Survey Geotechnical Report

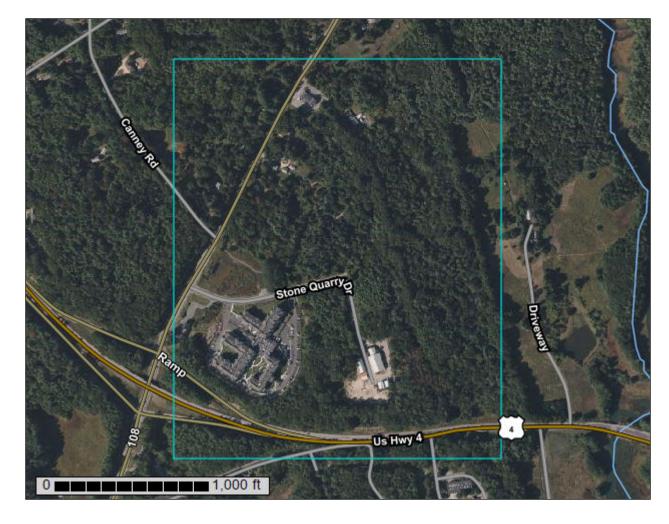




Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

## **Custom Soil Resource** Report for **Strafford County, New Hampshire**



#### **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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HdC—Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent	
slopes	13
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## Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



## MAP LEGEND

#### Special Line Features Streams and Canals Interstate Highways Very Stony Spot Major Roads Stony Spot US Routes Spoil Area Wet Spot Other Rails Nater Features **Fransportation** W 8 ◁ ŧ Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Closed Depression Special Point Features **Gravelly Spot Borrow Pit** Clay Spot **Gravel Pit** Area of Interest (AOI) Blowout 9 Soils

# MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

Aerial Photography

Marsh or swamp

Lava Flow

Landfill

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot Sandy Spot

**3ackground** 

Local Roads

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Strafford County, New Hampshire Survey Area Data: Version 25, Sep 3, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Severely Eroded Spot

Slide or Slip

Sinkhole

Sodic Spot

Date(s) aerial images were photographed: Jun 19, 2020—Sep 20, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

#### Map Unit Legend

Map Unit Symbol Map Unit Name		Acres in AOI	Percent of AOI	
BzB	Buxton silt loam, 3 to 8 percent slopes	45.4	35.7%	
GIC	Gloucester fine sandy loam, 8 to 15 percent slopes	0.9	0.7%	
НсВ	Hollis-Charlton fine sandy loams, 3 to 8 percent slopes	36.0	28.3%	
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	0.7	0.6%	
ScA	Scantic silt loam, 0 to 3 percent slopes	36.3	28.5%	
ScB	Scantic silt loam, 3 to 8 percent slopes	3.0	2.3%	
SfC	Suffield silt loam, 8 to 15 percent slopes	4.2	3.3%	
Та	Tidal marsh	0.0	0.0%	
W	Water	0.8	0.6%	
Totals for Area of Interest		127.3	100.0%	

#### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the

scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### Strafford County, New Hampshire

#### BzB—Buxton silt loam, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d6p

Elevation: 0 to 260 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Buxton and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Buxton**

#### Setting

Parent material: Glaciomarine

#### **Typical profile**

H1 - 0 to 10 inches: silt loam
H2 - 10 to 28 inches: silty clay loam
H3 - 28 to 43 inches: silty clay

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 12 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C/D

Ecological site: F145XY006CT - Semi-Rich Moist Lake Plain

Hydric soil rating: No

#### **Minor Components**

#### **Elmwood**

Percent of map unit: 10 percent

Hydric soil rating: No

#### Not named

Percent of map unit: 5 percent

#### GIC—Gloucester fine sandy loam, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d74 Elevation: 20 to 970 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Gloucester and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Gloucester**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: fine sandy loam

H2 - 14 to 28 inches: very gravelly loamy sand H3 - 28 to 40 inches: very gravelly coarse sand

#### Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00

to 20.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: A

Ecological site: F144AY032NH - Dry Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Not named pan

Percent of map unit: 5 percent

#### **Hollis**

Percent of map unit: 5 percent

Hydric soil rating: No

#### Acton

Percent of map unit: 5 percent

Hydric soil rating: No

#### HcB—Hollis-Charlton fine sandy loams, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7j Elevation: 0 to 1,020 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Farmland of local importance

#### **Map Unit Composition**

Hollis and similar soils: 55 percent Charlton and similar soils: 35 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: fine sandy loam H2 - 14 to 18 inches: bedrock

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

#### **Description of Charlton**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 13 inches: fine sandy loam
H2 - 13 to 36 inches: fine sandy loam
H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 5.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Not named

Percent of map unit: 5 percent

Hydric soil rating: No

#### **Buxton**

Percent of map unit: 5 percent

Hydric soil rating: No

## HdC—Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7n

Elevation: 0 to 1,200 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hollis and similar soils: 40 percent Charlton and similar soils: 30 percent Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: very stony fine sandy loam

H2 - 14 to 18 inches: bedrock

#### Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

#### **Description of Charlton**

#### Setting

Parent material: Till

#### **Typical profile**

H1 - 0 to 13 inches: very stony fine sandy loam

H2 - 13 to 36 inches: fine sandy loam H3 - 36 to 40 inches: gravelly loamy sand

#### Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 5.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### **Rock outcrop**

Percent of map unit: 10 percent

Hydric soil rating: No

#### Not named

Percent of map unit: 10 percent

Hydric soil rating: No

#### Woodbridge

Percent of map unit: 5 percent

Hydric soil rating: No

#### Sutton

Percent of map unit: 5 percent

Hydric soil rating: No

#### ScA—Scantic silt loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d8s

Elevation: 0 to 260 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of local importance

#### **Map Unit Composition**

Scantic and similar soils: 85 percent *Minor components*: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Scantic**

#### Setting

Landform: Marine terraces

#### Typical profile

H1 - 0 to 13 inches: silt loam

H2 - 13 to 23 inches: silty clay loam H3 - 23 to 40 inches: silty clay

#### Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: C/D

Ecological site: F144AY019NH - Wet Lake Plain

Hydric soil rating: Yes

#### **Minor Components**

#### **Swanton**

Percent of map unit: 5 percent Landform: Marine terraces Hydric soil rating: Yes

#### Not named wet

Percent of map unit: 5 percent Landform: Marine terraces Hydric soil rating: Yes

#### **Biddeford**

Percent of map unit: 5 percent Landform: Marine terraces Hydric soil rating: Yes

#### ScB—Scantic silt loam, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d8t

Elevation: 0 to 260 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of local importance

#### **Map Unit Composition**

Scantic and similar soils: 85 percent *Minor components:* 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Scantic**

#### Setting

Landform: Marine terraces

#### Typical profile

H1 - 0 to 13 inches: silt loam
H2 - 13 to 23 inches: silty clay loam
H3 - 23 to 40 inches: silty clay

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: C/D

Ecological site: F144AY019NH - Wet Lake Plain

Hydric soil rating: Yes

#### **Minor Components**

#### **Swanton**

Percent of map unit: 5 percent Landform: Marine terraces Hydric soil rating: Yes

#### Not named wet

Percent of map unit: 5 percent Landform: Marine terraces Hydric soil rating: Yes

#### **Buxton**

Percent of map unit: 5 percent

Hydric soil rating: No

#### SfC—Suffield silt loam, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 9d8v

Elevation: 0 to 250 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### Map Unit Composition

Suffield and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Suffield**

#### **Typical profile**

H1 - 0 to 19 inches: silt loam H2 - 19 to 28 inches: silt loam H3 - 28 to 41 inches: silty clay

#### Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C

Ecological site: F144AY017NH - Well Drained Lake Plain

Hydric soil rating: No

#### **Minor Components**

#### Not named

Percent of map unit: 9 percent

Hydric soil rating: No

#### **Buxton**

Percent of map unit: 5 percent

Hydric soil rating: No

#### Rock outcrop

Percent of map unit: 1 percent

#### Ta—Tidal marsh

#### **Map Unit Setting**

National map unit symbol: 9d92

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Tidal marsh: 98 percent Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Tidal Marsh**

#### Setting

Landform: Marshes

#### Typical profile

H1 - 0 to 12 inches: peat

H2 - 12 to 46 inches: mucky peat H3 - 46 to 50 inches: silt loam H4 - 50 to 60 inches: loamy sand

#### **Properties and qualities**

Slope: 0 to 1 percent

Drainage class: Very poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (0.60 to 20.00 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: Frequent

Frequency of ponding: Frequent

Maximum salinity: Very slightly saline to strongly saline (2.0 to 32.0 mmhos/cm)

Available water supply, 0 to 60 inches: Very high (about 14.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8w

Hydric soil rating: Yes

#### **Minor Components**

#### **Rock outcrop**

Percent of map unit: 2 percent

#### W-Water

#### **Map Unit Composition**

Water (less than 40 acres): 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### Michael Cuomo, Soil Scientist

#### 6 York Pond Road, York, Maine 03909 207 363 4532

#### mcuomosoil@gmail.com

Erik Saari, Vice President Altus Engineering, Inc. 133 Court Street Portsmouth, NH 03801

24 February 2024

Dear Mr. Saari;

This report is in reference to the 22.5 acre undeveloped parcel located north of Stone Quarry Drive and east of Route 108 in Durham, NH. This is identified by the town as map 209, lot 33 and is owned by Riverwoods, Durham. A Site Specific Soil Map was prepared for this property in February 2024 to assist you in planning and permitting a residential development served by municipal sewer and water service. There were a few patches of thin snow and the wetlands were mostly iced over when this work was done.

This report is a component of the Site Specific Soil Survey and must be submitted with it for regulatory review. The both comply with 'Site Specific Soil Mapping Standards for New Hampshire and Vermont', SSSNNE Special Publication No.3 version 7.0, July 2021.

The Soil Survey is comprised of two components: a soil map and this report. The soil map is made by traversing the property and observing the soil at locations thought to be representative of the landform. Because soil is highly variable, it is not possible to represent every soil variation on a soil map. The soil map is a simplified two-dimensional interpretation of the complex three dimensional soil-landscape relationship. Standards allow for inclusions of soils other than those named in the soil map unit label, so long as dissimilar inclusions do not exceed 25% of the map unit. Boundaries between different soils are shown as lines on the soil map, but are generally diffuse transition zones.

Soil names were selected using best fit with soils already researched in detail and listed in the 'New Hampshire State-Wide Numerical Soils Legend' issued in 2011 by the USDA Natural Resource Conservation Service. The map unit design and the interpretations of soil properties in this report are specific to this site and were selected considering the proposed use. Therefore, the interpretations and limitation information in this report may be insufficient for some other uses. Hydrologic soil groups were assigned using 'KSAT Values for New Hampshire Soils' SSSNNE Special Publication No. 5, September 2009.

Twenty eight test pits were dug with an excavator and are the primary basis of this soil survey. Other soil observations were made with a soil auger, and two were recorded in detail to document the wetland soils. The test pit data and soil observations are attached at the rear of this report. Eight soil types were identified on this property and are described below. The regulated wetland boundaries were previously flagged and have been survey located.

#### Map Unit: 29

#### Soil Name: Woodbridge

Drainage class: moderately well drained.

Parent material: basal till.

Texture range: fine sandy loam and sandy loam.

Described in: test pit MC6.

Landscape position: upland sideslopes.

Landform: gently rolling to steep.

Slope range: 1 to 25%.

Bedrock class: very deep (more than 60").

Hydrologic group: C.

Flood hazard: none.

Inclusions: test pit MC12 is a non limiting inclusion in which the firm subsoil occurs deeper than is typical.

Use and management: land uses are slightly limited by the presence of basal till, which causes the ground water to perch after rain events and snow melt. This limitation can be overcome by appropriate grading and drainage.

#### Map Unit: 32

#### Soil Name: Boxford

Drainage class: moderately well drained.

Parent material: marine.

Texture range: silt loam over silty clay loam.

Described in: test pit MC10.

Landscape position: gently rolling uplands.

Landform: terraces. Slope range: 1 to 15%.

Bedrock class: very deep (more than 60").

Hydrologic group: C.

Flood hazard: none.

Inclusions: test pit MC2 is a limiting inclusion of Boxford-like soils with bedrock between 48 and 60 inches deep. Test pit MC4 is a non-limiting inclusion of Boxford-like soils underlain by glacial till.

Use and management: land uses are limited by seasonal wetness close to the surface. These are not wetland soils and may be drained or filled to overcome this limitation. Boxford soils are highly erodible and difficult to revegetate. These soils have low bearing strength when saturated.

#### Map Unit: 33

#### Soil Name: Scitico

Drainage class: poorly drained.

Parent material: marine.

Texture range: silt loam over silty clay loam.

Described in: soil observation A.

Landscape position: nearly level to gently sloping wetlands.

Landform: glacial deltas, bays.

Slope range: 1 to 8%.

Bedrock class: very deep (more than 60").

Hydrologic group: C.

Flood hazard: undefined flood hazard may exist along small stream channels.

Inclusions: Scitico map units include small stream channels, which are limiting inclusions. Scitico map units include small areas with stony and bouldery surface layers, which is not typical. Limited historical ditching and filling for trails has occurred.

Use and management: land uses are limited by frequent saturation to the surface, low bearing strength, and fine textures, which makes it difficult to work the soil when wet. These are regulated wetlands and may be not be drained or filled without permits.

#### Map Unit: 42

#### Soil Name: Canton

Drainage class: well drained.

Parent material: loose glacial till.

Texture range: fine sandy loam over loamy sand.

Described in: test pit MC1.

Landscape position: upland.

Landform: ground moraine.

Slope range: 1-15%.

Bedrock class: very deep (more than 60").

Hydrologic group: B.

Flood hazard: none.

Inclusions: none observed.

Use and management: this soil presents no limitations to development.

#### Map Unit: 85

#### Soil Name: Hollis

Drainage class: somewhat excessively drained.

Parent material: loose glacial till.

Texture range: fine sandy loam.

Described in: test pit MC15.

Landscape position: rolling upland.

Landform: scoured ridges.

Slope range: 8 to 25%.

Bedrock class: shallow (10-20").

Hydrologic group: D.

Flood hazard: none.

Inclusions: bedrock outcroppings are found in this map unit and are a limiting inclusion.

Use and management: land uses are limited by bedrock 0 to 20 inches from the soil surface, which can be overcome by blasting and filling.

#### Map Unit: 89

#### Soil Name: Chatfield

Drainage class: well drained.

Parent material: loose glacial till.

Texture range: fine sandy loam.

Described in: test pit MC8.

Landscape position: upland.

Landform: scoured ridges.

Slope range: 1 to 8%.

Bedrock class: moderately deep (20-40").

Hydrologic group: B.

Flood hazard: none.

Inclusions: none noted.

Use and management: land uses are limited by bedrock 20 to 40 inches from the soil surface, which can be overcome by blasting and filling.

#### Map Unit: 134

#### Soil Name: Maybid

Drainage class: very poorly drained.

Parent material: marine.

Texture range: silt loam over silty clay loam.

Described in: soil observation B.

Landscape position: lowland wetlands.

Landform: deltas, bays.

Slope range: 0 to 1%.

Bedrock class: very deep (more than 60").

Hydrologic group: D.

Flood hazard: undefined flood hazard may exist.

Inclusions: none noted.

Use and management: Land uses are very limited by long periods of saturation to the surface, low bearing strength, and fine soil texture. These are regulated wetlands and may be not be drained or filled without permits.

#### Map Unit: 953

#### Soil Name: Boxford SPD

The Boxford SPD (SPD for 'somewhat poorly drained') is very similar to the Boxford soils, which are moderately well drained.

Drainage class: somewhat poorly drained.

Parent material: marine.

Texture range: silt loam over silty clay loam.

Described in: test pit MC3.

Landscape position: lowland.

Landform: terrace.

Slope range: 1 to more than 25%.

Bedrock class: very deep (more than 60").

Hydrologic group: C.

Flood hazard: none.

Inclusions: test pits MC17 and MC27 are Boxford SPD non-limiting variants which are underlain by firm glacial till. Test pit MC26 found bedrock between 48 and 60 inches, which is limiting for some land uses.

Test pits MC22, MC23, and MC24 show a non-limiting inclusion with a thin layer of fill over subsoils typical to Boxford SPD and Boxford soils. This inclusion appears widespread in the south west corner of the property, but could not be accurately separated as a map unit. It was included in the Boxford SPD because it is also somewhat poorly drained. Other areas of Boxford SPD map units are covered with debris from past human occupation, such as broken concrete and brick piles.

Use and management: land uses are limited by seasonal wetness close to the surface. These are not wetland soils and may be drained or filled to overcome this limitation. Boxford SPD soils are highly erodible and difficult to revegetate. These soils have low bearing strength when saturated.

Please call if you have questions regarding this work.

Sincerely,

Michael Cuomo

NH Certified Soil Scientist #6

#### The following must appear on the soil map

#### Site Specific Soil Map Legend

		HYDROLOGIC	
MAP	SOIL	SOIL	DRAINAGE
SYMBOL	NAME	GROUP	CLASS
29	Woodbridge	С	moderately well drained
32	Boxford	С	moderately well drained
33	Scitico	С	poorly drained
42	Canton	В	well drained
85	Hollis	D	somewhat excessively drained
89	Chatfield	В	well drained
134	Maybid	D	very poorly drained
953	Boxford SPD	С	somewhat poorly drained

The letter at the end of the soil map unit label is the slope class. This represents the predominant slope of the map unit.

#### Slope Class

A 0-1% B 1-8%

C 8-15%

D 15-25%

E +25%

This map is within the technical standards of the National Cooperative Soil Survey. It is a special purpose product intended for development planning and engineering interpretations. It was produced by a professional soil scientist, and is not a product of the USDA Natural Resources Conservation Service. There is a report that accompanies this map.

Michael Cuomo NH Cert. Soil Scientist #6 February 2024

#### Michael Cuomo, Soil Scientist

6 York Pond Road, York, Maine 03909 207 363 4532 mcuomosoil@gmail.com

#### TEST PIT DATA

Client: Altus Engineering

Location: Stone Quarry Drive, Durham, NH

Date: 12 and 14 February 2024

Test Pit Number: MC1

Depth
3" Description
Forest litter.

0-8" Dark brown (10YR 3/3) fine sandy loam, granular, friable.

8-18" Brownish yellow (10YR 6/6) fine sandy loam, blocky,

friable.

18-60" Light yellowish brown (2.5Y 6/3) loamy sand, blocky,

friable.

Depth to Seasonal High Water Table: none

Observed water: none Depth to bedrock: none

Soil name: Canton

Test Pit Number: MC2

0-10" Dark yellowish brown (10YR 3/4) silt loam, granular,

friable.

10-15" Yellowish brown (10YR 5/6) silt loam, blocky, friable.

15-24" Olive brown (2.5Y 4/3) silt loam, blocky, friable, redox.

24-50 Olive (5Y 4/3) silty clay loam, massive, firm, redox.

50"+ Bedrock.

Depth to Seasonal High Water Table: 15"

Observed water: none Depth to bedrock: 50"

Soil name: Boxford variant

Test Pit Number: MC3

0-8" Dark olive brown (2.5Y 3/3) silt loam, granular, friable.

8-10" Light olive brown (2.5Y 5/4) silt loam, blocky, friable.

10-14" Light yellowish brown (2.5Y 6/4) silt loam, blocky, friable, redox.

14-54 Olive (5Y 5/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 10"

Observed water: 12"
Depth to bedrock: none
Soil name: Boxford SPD

Percolation test: 22 minutes/inch at 9" depth

#### Depth Description

2" Forest litter.

0-8" Dark brown (10YR 3/3) silt loam, granular, friable.

8-15" Yellowish brown (10YR 5/6) silt loam, blocky, friable.

15-19" Light olive brown (2.5Y 5/4) silt loam, blocky, friable, redox.

19-40" Grayish brown (5Y 5/2) silty clay loam, massive, firm, redox.

40-60" Olive brown (2.5Y 4/4) stony fine sandy loam, massive, friable, redox.

Depth to Seasonal High Water Table: 15"

Observed water: 18" Depth to bedrock: none Soil name: Boxford variant

#### Test Pit Number: MC5

#### Description Depth

Forest litter.

0-7" Dark brown (10YR 3/3) fine sandy loam, granular, friable.

7-12" Brownish yellow (10YR 6/6) fine sandy loam, blocky, friable.

12-24" Light olive brown (2.5Y 5/6) loamy sand, blocky, friable.

24-60" Light yellowish brown (2.5Y 6/3) loamy sand, blocky, friable.

Depth to Seasonal High Water Table: none

Observed water: none Depth to bedrock: none

Soil name: Canton

#### Test Pit Number: MC6

#### Description <u>Depth</u> 3 "

Forest litter.

0-8" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.

8-16" Yellowish brown (10YR 5/4) stony fine sandy loam, blocky, friable.

16-21" Yellowish brown (10YR 5/6) stony sandy loam, blocky, friable.

21-55" Light olive brown (2.5Y 5/4) stony sandy loam, massive, firm, redox.

Depth to Seasonal High Water Table: 21"

Observed water: 50" Depth to bedrock: none Soil name: Woodbridge

<u>Depth</u> <u>Description</u>

1" Forest litter.

0-9" Very dark grayish brown (2.5Y 3/2) silt loam, granular, friable.

9-12" Light olive brown (2.5Y 5/4) silt loam, blocky, friable.

12-16" Light yellowish brown (2.5Y 6/3) silt loam, blocky, friable, redox.

16-60 Olive gray (5Y 5/2) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 12"

Observed water: none Depth to bedrock: none Soil name: Boxford SPD

Test Pit Number: MC8

#### <u>Depth</u> <u>Description</u>

3" Forest litter.

0-8" Very dark brown (10YR 2/2) fine sandy loam, granular, friable.

8-25" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, friable.

25-30" Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, friable.

Depth to Seasonal High Water Table: none

Observed water: none Depth to bedrock: 30" Soil name: Chatfield

Percolation test: 10 minutes/inch at 16" depth

Test Pit Number: MC9

#### <u>Depth</u> <u>Description</u>

2" Forest litter.

0-6" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable.

6-21" Brownish yellow (10YR 6/6) stony fine sandy loam, blocky, friable.

21-55" Light yellowish brown (2.5Y 6/4) loamy sand, blocky, friable.

Depth to Seasonal High Water Table: none

Observed water: none Depth to bedrock: none

Soil name: Canton

Depth Description

0-14" Very dark grayish brown (10YR 3/2) silt loam, granular, friable.

14-20" Yellowish brown (10YR 5/6) silt loam, blocky, friable.

20-25" Light olive brown (2.5Y 5/4) silt loam, blocky, friable, redox.

25-56" Olive (5Y 4/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 20"

Observed water: 25"
Depth to bedrock: none
Soil name: Boxford

Test Pit Number: MC11

Depth
1" Description
Forest litter.

0-8" Very dark grayish brown (2.5Y 3/2) silt loam, granular, friable.

8-10" Light olive brown (2.5Y 5/4) silt loam, blocky, friable.

10-17" Light yellowish brown (2.5Y 6/3) silt loam, blocky, friable, redox.

17-60" Olive (5Y 5/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 10"

Observed water: none Depth to bedrock: none Soil name: Boxford SPD

Test Pit Number: MC12

0-14" Very dark brown (10YR 2/2) fine sandy loam, granular, friable.

14-28" Yellowish brown (10YR 5/6) fine sandy loam, blocky, friable.

28-44" Olive brown (2.5Y 4/4) stony fine sandy loam, blocky, friable, redox.

44-60" Olive brown (2.5Y 4/3) stony fine sandy loam, massive, firm, redox.

Depth to Seasonal High Water Table: 28"

Observed water: 40"
Depth to bedrock: none

Soil name: Woodbridge variant

Test Pit Number: MC13

<u>Depth</u>

<u>Description</u>

2" Forest litter.

- 0-9" Very dark grayish brown (10YR 3/2) stony fine sandy loam, granular, friable.
- 9-16" Dark yellowish brown (10YR 4/6) stony fine sandy loam, blocky, friable.
- 16-24" Light yellowish brown (2.5Y 6/4) stony fine sandy loam, blocky, friable, redox.
- 24-60" Olive brown (2.5Y 4/4) stony sandy loam, massive, firm, redox.

Depth to Seasonal High Water Table: 16"

Observed water: 24"
Depth to bedrock: none
Soil name: Woodbridge

Percolation test: 12 minutes/inch at 15" depth

Test Pit Number: MC14

Depth
1" Description
Forest litter.

- 0-9" Very dark grayish brown (2.5Y 3/2) silt loam, granular, friable.
- 9-12" Light olive brown (2.5Y 5/4) silt loam, blocky, friable, redox.
- 12-20" Olive brown (2.5Y 4/3) silt loam, blocky, firm, redox.
- 20-60" Olive gray (5Y 5/2) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 9"

Observed water: 18"
Depth to bedrock: none
Soil name: Boxford SPD

Test Pit Number: MC15

Depth
1" Description
1 Forest litter.

- 0-8" Very dark grayish brown (10YR 3/2) bouldery fine sandy loam, granular, friable.
- 8-20" Yellowish brown (10YR 5/6) bouldery fine sandy loam, blocky, friable.

20"+ Bedrock.

Depth to Seasonal High Water Table: none

Observed water: none Depth to bedrock: 20" Soil name: Hollis Test Pit Number: MC16

Depth
Description
The Porest litter.

0-8" Very dark grayish brown (2.5Y 3/2) silt loam, granular, friable.

8-12" Light olive brown (2.5Y 5/4) silt loam, blocky, friable.

12-16" Olive brown (2.5Y 4/4) silt loam, blocky, friable, redox.

16-60" Olive gray (5Y 5/2) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 12"

Observed water: none Depth to bedrock: none Soil name: Boxford SPD

### Test Pit Number: MC17

Depth
1" Description
Forest litter.

0-9" Dark brown (10YR 3/3) silt loam, granular, friable.

9-11" Light olive brown (2.5Y 5/4) silt loam, blocky, friable.

11-13" Olive brown (2.5Y 4/4) silt loam, blocky, friable, redox.

13-32" Olive gray (5Y 5/2) silty clay loam, massive, firm, redox.

32-60" Olive brown (2.5Y 4/4) stony fine sandy loam, massive, firm, redox.

Depth to Seasonal High Water Table: 11"

Observed water: 34"
Depth to bedrock: none

Soil name: Boxford SPD variant

#### Test Pit Number: MC18

Depth
2" Description
2 Forest litter.

0-9" Dark brown (10YR 3/3) fine sandy loam, granular, friable.

9-24" Yellowish brown (10YR 5/6) fine sandy loam, blocky,

24-66" Light olive brown (2.5Y 5/4) stony fine sandy loam, blocky, friable, redox.

Depth to Seasonal High Water Table: 24"

Observed water: none Depth to bedrock: none Soil name: Woodbridge Test Pit Number: MC19

Depth Description

0-11" Very dark grayish brown (10YR 3/2) very fine sandy loam, granular, friable.

11-19" Strong brown (7.5YR 5/6) very fine sandy loam, blocky, friable.

19-22" Light olive brown (2.5Y 5/4) silt loam, blocky, fredox.

22-56" Olive (5Y 4/4) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 19"

Observed water: 50"
Depth to bedrock: none
Soil name: Boxford

## Test Pit Number: MC20 <u>Depth</u> <u>Description</u>

1" Forest litter.

0-9" Very dark grayish brown (10YR 3/2) silt loam, granular, friable.

9-11" Olive brown (2.5Y 4/4) silt loam, blocky, friable, redox.

11-18" Grayish brown (2.5Y 5/2) silt loam, blocky, friable, redox.

18-60" Olive gray (5Y 5/2) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 9"

Observed water: 30"
Depth to bedrock: none
Soil name: Boxford SPD

#### Test Pit Number: MC21

Depth
1" Description
Forest litter.

0-6" Dark brown (10YR 3/3) silt loam, granular, friable.

6-11" Light olive brown (2.5Y 5/4) silt loam, blocky, friable.

11-16" Grayish brown (2.5Y 5/2) silt loam, blocky, friable, redox.

16-55" Olive (5Y 4/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 11"

Observed water: 20"
Depth to bedrock: none
Soil name: Boxford SPD

Percolation test: 58 minutes/inch at 10" depth

Depth Description

0-6" Dark olive brown (2.5Y 3/3) fine sandy loam fill, massive, friable.

6-15" Light yellowish brown (2.5Y 6/3) gravelly loamy sand fill, massive, friable.

15-24" Dark grayish brown (2.5Y 4/2) silt loam, blocky, friable, redox.

24-55" Olive (5Y 4/4) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 15"

Observed water: none Depth to bedrock: none

Soil name: Excavated and filled over Boxford or Boxford SPD

Test Pit Number: MC23

<u>Depth</u> <u>Description</u>

0-8" Dark brown (10YR 3/3) fine sandy loam fill, granular, friable.

8-12" Light yellowish brown (2.5Y 6/3) gravelly loamy sand fill, massive, friable.

12-20" Light yellowish brown (2.5Y 6/4) silty clay loam, blocky, firm, redox.

20-58" Olive (5Y 4/4) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 12"

Observed water: none Depth to bedrock: none

Soil name: Excavated and filled over Boxford or Boxford SPD

Test Pit Number: MC24

Depth Description

0-7" Very dark grayish brown (10YR 3/2) fine sandy loam fill, granular, friable.

7-14" Light yellowish brown (2.5Y 6/3) gravelly loamy sand fill, massive, friable.

14-16" Very dark grayish brown (10YR 3/2) silt loam, massive, friable.

16-19" Light olive brown (2.5Y 5/3) silt loam, blocky, friable, redox.

19-60" Olive (5Y 4/4) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 16"

Observed water: none Depth to bedrock: none

Soil name: Excavated and filled over Boxford or Boxford SPD

Test Pit Number: MC25 Depth Description Forest litter. 0-9" Dark brown (10YR 3/3) stony fine sandy loam, granular, friable. 9-24"

Dark yellowish brown (10YR 4/6) stony fine sandy loam,

blocky, friable.

24-40" Light yellowish brown (10YR 6/4) stony loamy sand, blocky, friable.

40-60" Pale brown (2.5Y 7/3) stony loamy sand, massive, friable.

Depth to Seasonal High Water Table: none

Observed water: none Depth to bedrock: none Soil name: Canton

Test Pit Number: MC26

Depth Description Forest litter.

0-14" Very dark grayish brown (2.5Y 3/2) silt loam, granular, friable.

14-19" Light olive brown (2.5Y 5/4) silt loam, blocky, friable, redox.

19-30" Olive brown (2.5Y 4/4) silty clay loam, blocky, firm, redox.

30-50" Olive brown (2.5Y 4/3) stony fine sandy loam, massive, firm, redox.

50"+ Bedrock

Depth to Seasonal High Water Table: 14"

Observed water: 36" Depth to bedrock: 50"

Soil name: Boxford SPD variant

Test Pit Number: MC27

Depth Description

Forest litter

0-10" Very dark grayish brown (10YR 3/2) silt loam, granular, friable.

10-20" Yellowish brown (10YR 5/6) silt loam, blocky, friable.

20-30" Light olive brown (2.5Y 5/3) silty clay loam, massive, firm, redox.

30-50" Light olive brown (2.5Y 5/4) stony fine sandy loam, massive, firm, redox.

50"+ Bedrock.

Depth to Seasonal High Water Table: 20"

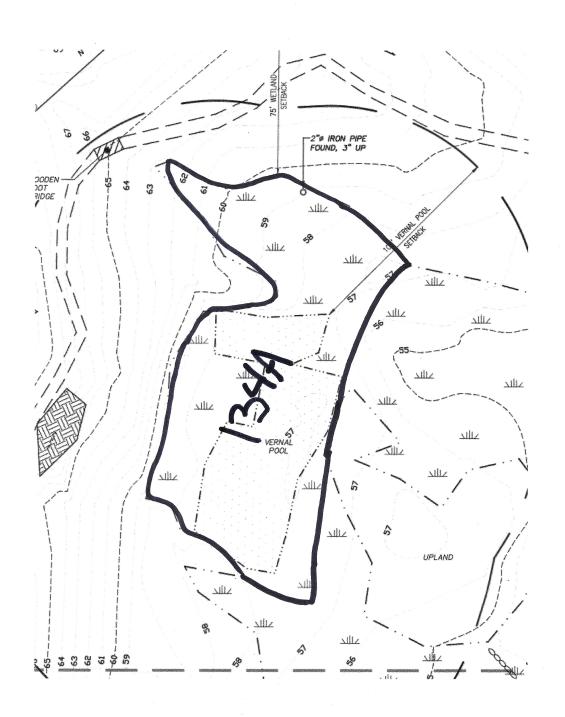
Observed water: none Depth to bedrock: 50"

Soil name: Boxford variant

```
Test Pit Number: MC28
Depth
             Description
1"
        Forest litter.
0-6"
        Very dark grayish brown (2.5Y 3/2) silt loam, granular,
6-8"
        Light olive brown (2.5Y 5/4) silt loam, blocky, friable.
8-11"
        Grayish brown (2.5Y 5/2) silt loam, blocky, friable, redox.
        Olive (5Y 4/3) silty clay loam, blocky, firm, redox.
Depth to Seasonal High Water Table: 8"
Observed water: 30"
Depth to bedrock: none
Soil name: Boxford SPD
Soil Observation A (with hand tools)
             Description
<u>Depth</u>
1"
        Forest litter.
0-10"
        Dark olive brown (2.5Y 3/3) silt loam, granular,
        friable, redox.
10-14"
        Light brownish gray (2.5Y 6/2) silt loam, blocky, friable,
14-19"
        Olive brown (2.5Y 4/3) silt loam, blocky, friable, redox.
19-40"
        Olive (5Y 4/3) silty clay loam, blocky, firm, redox.
Depth to Seasonal High Water Table: surface
Observed water: 12"
Depth to bedrock: none
Soil name: Scitico
Soil Observation B (with hand tools)
             Description
Depth
1 "
        Forest litter.
0-6"
        Black (2.5Y 2/1) silt loam, granular, friable, redox.
6-10"
        Light brownish gray (2.5Y 6/2) silt loam, blocky, friable,
        redox.
10-15"
        Dark grayish brown (2.5Y 4/2) silt loam, blocky, friable,
        redox.
15-20"
        Olive gray (5Y 5/2) silt loam, blocky, firm, redox.
        Olive (5Y 4/3) silty clay loam, blocky, firm, redox.
Depth to Seasonal High Water Table: surface
Observed water: 9"
Depth to bedrock: none
Soil name: Maybid
```



### THIS SHOWS THE CORRECT CONFIGURATION OF THIS MAP UNIT



### Michael Cuomo, Soil Scientist

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#### **TEST PIT DATA**

Client: Altus Engineering

Location: Stone Quarry Drive, Durham, NH

Date: 12 June 2025

#### **Test Pit Number: A1**

<u>Depth</u>	<u>Description</u>
0-9"	Dark brown (10YR 3/3) silt loam, granular, friable.
9-12"	Light olive brown (2.5Y 5/4) silt loam, blocky, friable.
12-19"	Light olive brown (2.5Y 5/3) silt loam, blocky, friable, redox.
19-75"	Olive (5Y 4/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 12"

Depth to Bedrock: none Observed Water: none

Estimated percolation rate: 60 min./inch

#### **Test Pit Number: A2**

<u>Depth</u>	<u>Description</u>
0-15"	Very dark grayish brown (10YR 3/2) very fine sandy loam, granular, friable.
15-17"	Reddish yellow (7.5YR 6/6) very fine sandy loam, blocky, friable.
17-25"	Light olive brown (2.5Y 5/4) very fine sandy loam, blocky, friable, redox.
25-80"	Olive (5Y 4/4) silt loam, massive, firm, redox.

Depth to Seasonal High Water Table: 17"

Depth to Bedrock: none Observed Water: 20"

Estimated percolation rate: 60 min./inch

<u>Depth</u>	<u>Description</u>
0-9"	Dark olive brown (2.5Y 3/3) silt loam, granular, friable.
9-14"	Light olive brown (2.5Y 5/4) silt loam, blocky, friable.
14-24"	Olive (5Y 4/4) silt loam, blocky, friable, redox.
24-60"	Olive (5Y 4/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 14"

Depth to Bedrock: none Observed Water: none

Estimated percolation rate: 60 min./inch

#### **Test Pit Number: A4**

<u>Depth</u>	<u>Description</u>
0-10"	Very dark grayish brown (2.5Y 3/2) silt loam fill, granular, friable.
10-14"	Light yellowish brown (2.5Y 6/4) loamy sand fill, massive, friable.
14-16"	Very dark grayish brown (2.5Y 3/2) silt loam, granular, friable, redox.
16-20"	Olive gray (5Y 5/2) silt loam, blocky, friable, redox.
20-66"	Olive (5Y 4/3) silty clay loam, massive, firm, redox.

Depth to Seasonal High Water Table: 14"

Depth to Bedrock: none Observed Water: 55"

Estimated percolation rate: 60 min./inch

#### **Test Pit Number: A5**

<u>Depth</u>	<u>Description</u>
0-8"	Very dark grayish brown (10YR 3/3) silt loam, granular, friable.
8-12"	Light olive brown (2.5Y 5/4) silt loam, blocky, friable.
12-19"	Light olive brown (2.5Y 5/3) silt loam, blocky, friable, redox.
19-48"	Olive (5Y 4/3) silty clay loam, massive, firm, redox.
48-72"	Olive brown (2.5Y 4/4) stony fine sandy loam, massive, friable, redox.
72-86"	Olive brown (2.5Y 4/4) stony loamy sand, massive, friable,
72 00	redox.

Depth to Seasonal High Water Table: 12"

Depth to Bedrock: none Observed Water: 60"

Estimated percolation rate: 60 min./inch

<u>Depth</u>	<u>Description</u>
0-9"	Very dark grayish brown (10YR 3/3) fine sandy loam, granular,
	friable.
9-16"	Brownish yellow (10YR 6/6) fine sandy loam, blocky, friable.
16-84"	Light yellowish brown (2.5Y 6/4) loamy sand, blocky, friable.
84-96"	Light olive brown (2.5Y 5/4) loamy sand, blocky, friable, redox.

Depth to Seasonal High Water Table: 84"

Depth to Bedrock: none Observed Water: none

Estimated percolation rate: 4 to 6 min./inch

## Section 7

## BMP and Riprap Sizing Calculations



## FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.08)

Type/Node Name: Bioretention Pond #1 (HydroCAD Node #17P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

			0/ )
X	_	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	8(a).
0.23	-	A = Area draining to the practice	
0.10	_	A <sub>I</sub> = Impervious area draining to the practice	
	decimal	I = Percent impervious area draining to the practice, in decimal form	
	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
	ac-in	WQV= 1" x Rv x A	
359	-	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
90	_	25% x WQV (check calc for sediment forebay volume)	
269		75% x WQV (check calc for surface sand filter volume)	
	В	Method of Pretreatment? (not required for clean or roof runoff)	. 250/14/01/
	cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	<u>&gt;</u> 25%WQV
Calculate ti		if system IS NOT underdrained:	
	sf -	A <sub>SA</sub> = Surface area of the practice	
	iph	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>	
	-	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	
-	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	< 72-hrs
Calculate ti	me to drair	if system IS underdrained:	
56.80	ft	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)	
0.01	cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)	
19.92	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	≤ 72-hrs
54.75	feet	E <sub>FC</sub> = Elevation of the bottom of the filter course material <sup>2</sup>	
53.75	- feet	E <sub>UD</sub> = Invert elevation of the underdrain (UD), if applicable	
57.00	- feet	$E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
51.75	- feet	$E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test	
1.00	feet	D <sub>FC to UD</sub> = Depth to UD from the bottom of the filter course	<u>≥</u> 1'
3.00	feet	D <sub>FC to ROCK</sub> = Depth to bedrock from the bottom of the filter course	<u>≥</u> 1'
(2.25)	_	D <sub>FC to SHWT</sub> = Depth to SHWT from the bottom of the filter course	<u>≥</u> 1'
58.50		Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
59.25		Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface	sand filter	or underground sand filter is proposed:	
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> 75%WQV
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
B	<del>-</del>	Note what sheet in the plan set contains the filter course specification.	
Sheet	•	Note what sheet in the plan set contains the litter course specification.	
Sheet	Yes/No	Access grate provided?	← yes

If a biore	etention area	is proposed:	
YES	ac	Drainage Area no larger than 5 ac?	← yes
1,05	54 cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> WQV
18	inches 3.0	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
She	eet C-15	Note what sheet in the plan set contains the filter course specification	
3	3.0 :1	Pond side slopes	<u>&gt; 3</u> :1
She	eet L1 & L2	Note what sheet in the plan set contains the planting plans and surface cover	
If porous	s pavement is	proposed:	
		Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres	A <sub>SA</sub> = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA
She	eet C-14	Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat<sub>design</sub> includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:		
System is lined, SHWT not relevant		

### Stage-Area-Storage for Pond 17P: Bio #1

Elevation	Surface	Wetted	Storage	
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)	
54.75	487	487	0	
54.85	487	495	2 5	
54.95	487	503	5	
55.05	487	510	7	
55.15	487	518	10	
55.25	487	526	12	
55.35	487	534	15	
55.45	487	542	17	
55.55	487	550	19	
55.65	487	557	22	
55.75	487	565	24	
55.85	487	573	27	
55.95	487	581	29	
56.05	487	589	32	
56.15	487	597	34	
56.25	487	604	37	
56.35	521	640	87	
56.45	557	676	141	
56.55	594	714	198	
56.65	632	753	260	
56.75	671	793	325	
56.85	711	835	394	WQV = 359 cf
56.95	753	877	467	Ewqv = 56.80
57.05	795	920	544	EWQV = 30.00
57.15	837	964	626	
57.25	880	1,008	712	
57.35	924	1,054	802	Available
57.45	970	1,100	897	WQV=1,054cf
57.55	1,016	1,148	996	VVQV=1,03401
57.65	1,064	1,197	1,100	
57.75	1,113	1,247	1,209	
57.85	1,162	1,298	1,323	
57.95	1,213	1,351	1,441	
58.05	1,264	1,403	1,565	
58.15	1,316	1,457	1,694	
58.25	1,369	1,511	1,829	
58.35	1,423	1,566	1,968	
58.45	1,477	1,623	2,113	
58.55	1,533	1,680	2,264	
58.65	1,590	1,739	2,420	
58.75	1,648	1,798	2,582	
58.85	1,707	1,859	2,749	
58.95	1,767	1,921	2,749	
59.05	1,827	1,983	3,103	
59.05 59.15	1,888	2,046	3,103	
59.15 59.25			3,480	
08.20	1,950	2,110	3,400	

### Stage-Discharge for Pond 17P: Bio #1

Elevation	Primary	Elevation	Primary
(feet)	(cfs)	(feet)	(cfs)
54.75	0.00	57.40	0.03
54.80	0.00	57.45	0.05
54.85	0.00	57.50	0.08
54.90 54.95	0.00 0.00	57.55 57.60	0.11 0.15
54.95 55.00	0.00	57.65 57.65	0.15
55.05	0.00	57.70	0.19
55.10	0.00	57.75	0.24
55.15	0.00	57.80	0.26
55.20	0.00	57.85	0.28
55.25	0.00	57.90	0.30
55.30	0.00	57.95	0.32
55.35	0.00	58.00	0.34
55.40 55.45	0.00 0.00	58.05 58.10	0.35 0.37
55.50	0.00	58.15	0.38
55.55	0.00	58.20	0.40
55.60	0.00	58.25	0.41
55.65	0.00	58.30	0.43
55.70	0.00	58.35	0.44
55.75	0.00	58.40	0.45
55.80	0.00	58.45	0.46
55.85	0.00	58.50	0.48
55.90 55.95	0.00 0.00	58.55 58.60	0.49 0.50
56.00	0.00	58.65	0.51
56.05	0.00	58.70	0.52
56.10	0.00	58.75	0.54
56.15	0.00	58.80	0.84
56.20	0.00	58.85	1.39
56.25	0.00	58.90	2.09
56.30	0.00	58.95	2.92
56.35 56.40	0.00 0.00	59.00 59.05	3.86 4.90
56.45	0.00	59.10	6.03
56.50	0.01	59.15	7.24
56.55	0.01	59.20	8.53
56.60	0.01	59.25	9.89
56.65	0.01		
56.70	0.01		
56.75 56.80	0.01 0.01		
56.85	0.01	Qwqv =	= 0.01cfs
56.90	0.01		
56.95	0.02		
57.00	0.02		
57.05	0.02		
57.10	0.02		
57.15	0.02		
57.20 57.25	0.02 0.02		
57.25 57.30	0.02		
57.35	0.02		

## FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.08)

Type/Node Name: Bioretention Pond #2 (HydroCAD Node #22P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		201
X 2.26	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	08(a).
0.36 ac	A = Area draining to the practice	
0.27 ac	A <sub>I</sub> = Impervious area draining to the practice	
0.75 decimal	I = Percent impervious area draining to the practice, in decimal form	
0.73 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.26 ac-in	WQV= 1" x Rv x A	
947 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
237 cf	25% x WQV (check calc for sediment forebay volume)	
711 cf	75% x WQV (check calc for surface sand filter volume)	
СВ	Method of Pretreatment? (not required for clean or roof runoff)	
cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	<u>&gt;</u> 25%WQV
Calculate time to dra	in if system IS NOT underdrained:	
sf	A <sub>SA</sub> = Surface area of the practice	
iph	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>	
	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
Yes/No	(Use the calculations below)	
- hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	< 72-hrs
Calculate time to dra	in if system IS underdrained:	
	•	
58.45 ft	E <sub>WOV</sub> = Elevation of WQV (attach stage-storage table)	
	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)  O <sub>WQV</sub> = Discharge at the E <sub>WQV</sub> (attach stage-discharge table)	
0.02 cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)	< 72-hrs
0.02 cfs 26.32 hours	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$	< 72-hrs
0.02 cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup>	< 72-hrs
0.02 cfs 26.32 hours	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$	< 72-hrs
0.02 cfs 26.32 hours 56.25 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup>	
0.02 cfs 26.32 hours 56.25 feet 55.25 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $^2$ $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable	pit)
0.02 cfs  26.32 hours  56.25 feet  55.25 feet  55.08 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test)	pit)
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Depth to UD from the bottom of the filter course	pit) t pit)
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $^2$ $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } NOCK}$ = Depth to bedrock from the bottom of the filter course	oit) t pit) <b>&gt; 1'</b>
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test particles are Elevation of bedrock (if none found, enter the lowest elevation of the test particles are Depth to UD from the bottom of the filter course $D_{FC \text{ to } ROCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course	oit) t pit) ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test particles are the elevation of bedrock (if none found, enter the lowest elevation of the test particles are the	oit) t pit) ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $^2$ $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Depth to UD from the bottom of the filter course $D_{FC \text{ to } NOCK}$ = Depth to bedrock from the bottom of the filter course $D_{FC \text{ to } SHWT}$ = Depth to SHWT from the bottom of the filter course  Peak elevation of the 50-year storm event (infiltration can be used in analysis)  Elevation of the top of the practice	pit) t pit) ≥ 1' ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft 60.00 ft	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test particles are the elevation of bedrock (if none found, enter the lowest elevation of the test particles are the	oit) t pit) ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft 60.00 ft	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test processes $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test processes $E_{ROCK}$ = Depth to UD from the bottom of the filter course $E_{FC to ROCK}$ = Depth to bedrock from the bottom of the filter course $E_{FC to SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course $E_{ROCK}$ = Depth to SHWT from the bottom of the filter course	pit) t pit) ≥ 1' ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft 60.00 ft YES If a surface sand filter	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup> $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test $E_{ROCK}$ = Depth to UD from the bottom of the filter course $E_{FC \ to \ NOCK}$ = Depth to bedrock from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course $E_{FC \ to \ SHWT}$ = Depth to SHWT from the bottom of the filter course	oit) t pit) ≥ 1' ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft 60.00 ft YES If a surface sand filte YES ac cf	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $^2$ $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test particles are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the lowest elevation can be used in analysis) are lowest elevation of the top of the practice are the lowest elevation of the lowest elevation can be used in analysis). Elevation of the top of the practice are the lowest elevation of the lowest elevation can be used in analysis). Elevation of the top of the practice are the lowest elevation of the lowe	oit) t pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1'
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft 60.00 ft YES If a surface sand filte YES ac cf inches	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $^2$ $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test processes and the filter course elevation of bedrock (if none found, enter the lowest elevation of the test processes are processed in the filter course elevation of the bottom of the filter course elevation elevation of the bottom of the filter course elevation of the SHWT from the bottom of the filter course elevation of the 50-year storm event (infiltration can be used in analysis) elevation of the top of the practice elevation elevation elevation elevation of the top of the practice elevation eleva	pit) t pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1'   ✓ yes  < 10 ac ≥ 75%WQV
0.02 cfs 26.32 hours 56.25 feet 55.25 feet 55.08 feet 50.75 feet 1.00 feet 5.50 feet 1.17 feet 59.65 ft 60.00 ft YES If a surface sand filte YES ac cf	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table) $T_{DRAIN}$ = Drain time = $2WQV/Q_{WQV}$ $E_{FC}$ = Elevation of the bottom of the filter course material $^2$ $E_{UD}$ = Invert elevation of the underdrain (UD), if applicable $E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test particles are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the top of the practice are the lowest elevation of the lowest elevation can be used in analysis) are lowest elevation of the top of the practice are the lowest elevation of the lowest elevation can be used in analysis). Elevation of the top of the practice are the lowest elevation of the lowest elevation can be used in analysis). Elevation of the top of the practice are the lowest elevation of the lowe	oit) t pit) ≥ 1' ≥ 1' ≥ 1' ≥ 1'

If a b	iorete	ntion area i	is proposed:	
Υ	'ES	ac	Drainage Area no larger than 5 ac?	← yes
	1,000	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> WQV
	18.0	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
	Sheet	C-15	Note what sheet in the plan set contains the filter course specification	
	3.0	:1	Pond side slopes	<u>&gt; 3</u> :1
	Sheet	L1 & L2	Note what sheet in the plan set contains the planting plans and surface cover	
If po	rous p	avement is	proposed:	
			Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
		acres	A <sub>SA</sub> = Surface area of the pervious pavement	
		:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
		inches	D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA
	Sheet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat<sub>design</sub> includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:					
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·		·		·	

### Stage-Area-Storage for Pond 22P: Bio #2

Elevation	Surface	Wetted	Storage	
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)	
56.25	1,027	1,027	0	
56.35	1,027	1,038	5	
56.45	1,027	1,050	10	
56.55	1,027	1,061	15	
56.65	1,027	1,072	21	
56.75	1,027	1,084	26	
56.85	1,027	1,095	31	
56.95	1,027	1,107	36	
57.05	1,027	1,118	41	
57.15	1,027	1,129	46	
57.25	1,027	1,141	51	
57.35	1,027	1,152	56	
57.45	1,027	1,163	62	
57.55	1,027	1,175	67	
57.65	1,027	1,186	72	
57.75	1,027	1,197	77	
57.85	1,085	1,257	183	
57.95	1,145	1,317	294	
58.05	1,203	1,377	412	
58.15	1,261	1,437	535	
58.25	1,321	1,497	664	WQV = 947 cf
58.35	1,381	1,559	799	I I
58.45	1,443	1,623	940	Ewqv = 58.45
58.55	1,507	1,688	1,088	Lowest Outlet = 58.50
58.65	1,572	1,754	1,242	Available WQV = 1,000 cf
58.75	1,638	1,822	1,402	Available VVQV = 1,000 cl
58.85	1,705	1,891	1,569	
58.95	1,774	1,961	1,743	
59.05	1,841	2,030	1,924	
59.15	1,907	2,097	2,111	
59.25	1,974	2,166	2,305	
59.35	2,042	2,236	2,506	
59.45	2,111	2,307	2,714	
59.55	2,181	2,379	2,928	
59.65	2,252	2,452	3,150	
59.75	2,325	2,526	3,379	
59.85	2,398	2,602	3,615	
59.95	2,473	2,679	3,859	

Prepared by Altus Engineering, Inc.

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### Stage-Discharge for Pond 22P: Bio #2

Elevation	Primary	Elevation	Primary	Elevation	Primary	Elevation	Primary
(feet)	(cfs)	(feet)	(cfs)	(feet)	(cfs)	(feet)	(cfs)
56.25	0.00	57.31	0.00	58.37	0.02	59.43	0.43
56.27	0.00	57.33	0.00	58.39	0.02	59.45	0.44
56.29	0.00	57.35	0.00	58.41	0.02	59.47	0.44
56.31	0.00	57.37	0.00	58.43	0.02	59.49	0.45
56.33	0.00	57.39	0.00	58.45	0.02	$\longrightarrow$ Qwqv = (	0.02 cfs
56.35	0.00	57.41	0.00	58.47	0.03	50.55	0.70
56.37	0.00	57.43	0.00	58.49	0.03	59.55	0.76
56.39	0.00	57.45	0.00	58.51	0.03	59.57	0.95
56.41	0.00	57.47	0.00	58.53	0.03	59.59	1.18
56.43	0.00	57.49	0.00	58.55 58.57	0.03	59.61	1.43
56.45	0.00	57.51	0.00	58.57	0.04	59.63	1.71
56.47	0.00	57.53	0.00	58.59	0.05	59.65	2.01
56.49	0.00	57.55	0.00	58.61	0.06	59.67	2.33
56.51	0.00	57.57	0.00	58.63	0.07	59.69	2.67
56.53	0.00	57.59	0.00	58.65	0.08	59.71	3.02
56.55 56.53	0.00	57.61	0.00	58.67	0.10	59.73	3.39
56.57	0.00	57.63	0.00	58.69	0.11	59.75	3.78
56.59	0.00	57.65	0.00	58.71	0.12	59.77	4.19
56.61	0.00	57.67	0.00	58.73	0.14	59.79	4.61
56.63	0.00	57.69	0.00	58.75	0.16	59.81	5.04
56.65	0.00	57.71	0.00	58.77	0.17	59.83	5.49
56.67	0.00	57.73	0.00	58.79	0.19	59.85	5.96
56.69	0.00	57.75	0.00	58.81	0.20	59.87	6.43
56.71	0.00	57.77	0.00	58.83	0.21	59.89	6.92
56.73	0.00	57.79	0.00	58.85	0.22	59.91	7.42
56.75	0.00	57.81	0.00	58.87	0.23	59.93	7.93
56.77	0.00	57.83	0.00	58.89	0.24	59.95	8.46
56.79 56.81	0.00	57.85 57.87	0.00 0.00	58.91	0.25 0.26	59.97	9.00
56.83	0.00 0.00		0.00	58.93	0.26	59.99	9.54
		57.89		58.95			
56.85 56.87	0.00 0.00	57.91	0.01 0.01	58.97 58.99	0.28 0.28		
56.89	0.00	57.93 57.95	0.01	59.01	0.28		
56.91	0.00	57.95 57.97	0.01	59.01	0.29		
56.93	0.00	57.97 57.99	0.01	59.05 59.05	0.30		
56.95	0.00	57.99 58.01	0.01	59.05 59.07	0.31		
56.97	0.00	58.03	0.01	59.07 59.09	0.32		
56.99	0.00	58.05	0.01	59.09 59.11	0.32		
57.01	0.00	58.07	0.01	59.11	0.33		
57.01 57.03	0.00	58.09	0.01	59.15 59.15	0.34		
57.05	0.00	58.11	0.01	59.17	0.35		
57.03 57.07	0.00	58.13	0.01	59.17 59.19	0.36		
57.09	0.00	58.15	0.01	59.21	0.36		
57.11	0.00	58.17	0.01	59.23	0.37		
57.13	0.00	58.19	0.02	59.25	0.38		
57.15	0.00	58.21	0.02	59.27	0.38		
57.17	0.00	58.23	0.02	59.29	0.39		
57.17 57.19	0.00	58.25	0.02	59.31	0.40		
57.21	0.00	58.27	0.02	59.33	0.40		
57.23	0.00	58.29	0.02	59.35	0.41		
57.25	0.00	58.31	0.02	59.37	0.41		
57.27	0.00	58.33	0.02	59.39	0.42		
57.29	0.00	58.35	0.02	59.41	0.42		
2 <b>_2</b>	2.00			]	3 <u> </u>		

## FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.08)

Type/Node Name: Bioretention Pond #3 (HydroCAD Node #69P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		Charlest various at the restrictions on unlined systems authord in Fau Wa 1500.0	0/0)
1.65	_	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	8(a).
	-	A = Area draining to the practice	
1.05	_	A <sub>1</sub> = Impervious area draining to the practice	
	decimal	I = Percent impervious area draining to the practice, in decimal form	
	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)  WQV= 1" x Rv x A	
3,729	ac-in	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
932	_	25% x WQV (check calc for sediment forebay volume)	
2,797	_	75% x WQV (check calc for surface sand filter volume)	
	CB	Method of Pretreatment? (not required for clean or roof runoff)	
	cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate ti		if system IS NOT underdrained:	
Carcalate ti	sf	A <sub>SA</sub> = Surface area of the practice	
	_		
	iph -	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>	
	v. (b)	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	. 70 L
	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
		if system IS underdrained:	
49.64	_ft _	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)	
0.06	cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)	
34.53	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	<u>&lt;</u> 72-hrs
46.50	feet	$E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup>	
45.50	feet	E <sub>UD</sub> = Invert elevation of the underdrain (UD), if applicable	
49.50	feet	$E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
48.50	feet	$E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)
1.00	feet	$D_{FC \text{ to UD}}$ = Depth to UD from the bottom of the filter course	<u>≥</u> 1'
(2.00)	feet	$D_{FC \text{ to ROCK}}$ = Depth to bedrock from the bottom of the filter course	<u>≥</u> 1'
(3.00)	_	D <sub>FC to SHWT</sub> = Depth to SHWT from the bottom of the filter course	<u>≥</u> 1'
52.55		Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
53.00	_	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface	sand filter	or underground sand filter is proposed:	
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> 75%WQV
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sheet	<b>-</b> : :	Note what sheet in the plan set contains the filter course specification.	
1		-	← yes
	Yes/No	Access grate provided?	\ yes

If a bior	retentior	n area i	s proposed:	
YES	ac		Drainage Area no larger than 5 ac?	← yes
4,7	799_cf		V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> WQV
18	inch 8.0	es	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sh	neet	C-15	Note what sheet in the plan set contains the filter course specification	
	3.0 :1		Pond side slopes	<u>&gt; 3</u> :1
Sh	neet L1	L & L2	Note what sheet in the plan set contains the planting plans and surface cover	
If porou	us pavem	nent is	proposed:	
			Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acre	·S	A <sub>SA</sub> = Surface area of the pervious pavement	
	:1		Ratio of the contributing area to the pervious surface area	≤ 5:1
	inch	es	D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA
Sh	neet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat<sub>design</sub> includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:					
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### Stage-Area-Storage for Pond 69P: Bio #3

Elevation	Surface	Wetted	Storage	
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)	
46.50	1,678	1,678	0	
46.70	1,678	1,707	17	
46.90	1,678	1,736	34	
47.10	1,678	1,765	50	
47.30	1,678	1,794	67	
47.50	1,678	1,823	84	
47.70	1,678	1,852	101	
47.90	1,678	1,881	117	
48.10	1,737	1,957	297	
48.30	1,859	2,082	656	
48.50	1,985	2,212	1,040	
48.70	2,114	2,345	1,450	
48.90	2,248	2,483	1,887	
49.10	2,387	2,626	2,350	
49.30	2,531	2,775	2,842	
49.50	2,679	2,927	3,363	WQV = 3,729  cf
49.70	2,832	3,084	3,914	Ewgv = 49.64
49.90	2,988	3,245	4,496	
50.10	3,150	3,411	5,109	Lowest Outlet = 50.00
50.30	3,317	3,583	5,756	Available WQV = 4,799 cf
50.50	3,488	3,759	6,436	
50.70	3,664	3,940	7,151	
50.90	3,843	4,125	7,902	
51.10	4,028	4,315	8,689	
51.30	4,218	4,510	9,514	
51.50	4,413	4,710	10,377	
51.70	4,612	4,915	11,279	
51.90	4,815	5,124	12,222	
52.10	5,023	5,338	13,205	
52.30	5,237	5,557	14,231	
52.50	5,455	5,781	15,300	
52.70	5,677	6,010	16,413	
52.90	5,904	6,243	17,572	

### Stage-Discharge for Pond 69P: Bio #3

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
46.50	0.00	48.62	0.02	50.74	0.80	52.86	16.48
46.54	0.00	48.66	0.02	50.74	0.85	52.90	18.49
46.58	0.00	48.70	0.02	50.76	0.03	52.94	20.60
46.62	0.00	48.74	0.02	50.86	0.98	52.98	<b>22.07</b>
46.66	0.00	48.78	0.03	50.90	1.04	32.30	22.07
46.70	0.00	48.82	0.03	50.94	1.10		
46.74	0.00	48.86	0.03	50.98	1.17		
46.78	0.00	48.90	0.03	51.02	1.23		
46.82	0.00	48.94	0.03	51.06	1.30		
46.86	0.00	48.98	0.04	51.10	1.37		
46.90	0.00	49.02	0.04	51.14	1.44		
46.94	0.00	49.06	0.04	51.18	1.51		
46.98	0.00	49.10	0.04	51.22	1.58		
47.02	0.00	49.14	0.04	51.26	1.66		
47.06	0.00	49.18	0.04	51.30	1.73		
47.10	0.00	49.22	0.05	51.34	1.81		
47.14	0.00	49.26	0.05	51.38	1.88		
47.18	0.00	49.30	0.05	51.42	1.96		
47.22	0.00	49.34	0.05	51.46	2.04		
47.26	0.00	49.38	0.05	51.50	2.12		
47.30	0.00	49.42	0.05	51.54	2.20		
47.34	0.00	49.46	0.06	51.58	2.29		
47.38	0.00	49.50	0.06	51.62	2.37		
47.42	0.00	49.54	0.06	51.66	2.45		
47.46	0.00	49.58	0.06	51.70	2.54		
47.50	0.00	49.62	0.06	Qwqv = 0.06	cfs 2.63		
47.54	0.00	49.66	0.06	<del>                                   </del>	<b></b> 2./1		
47.58	0.00	49.70	0.07	51.82	2.80		
47.62	0.00	49.74	0.07	51.86	2.89		
47.66	0.00	49.78	0.07	51.90	2.98		
47.70	0.00	49.82	0.07	51.94	3.07		
47.74	0.00	49.86	0.07	51.98	3.17		
47.78	0.00	49.90	0.07	52.02	3.26		
47.82	0.00	49.94	0.08	52.06	3.35		
47.86	0.00	49.98	0.08	52.10	3.45		
47.90	0.00	50.02	0.08	52.14	3.54		
47.94	0.00	50.06	0.10	52.18	3.64		
47.98	0.00	50.10	0.12 0.14	52.22	3.74 3.84		
48.02 48.06	0.00 0.00	50.14 50.18	0.14	52.26	3.64 3.94		
48.10	0.00	50.16	0.17	52.30 52.34	3.94 4.04		
48.14	0.00	50.26	0.20	52.38	4.04		
48.18	0.00	50.30	0.23	52.42	4.14		
48.22	0.01	50.34	0.27	52.46	4.34		
48.26	0.01	50.38	0.35	52.50	4.45		
48.30	0.01	50.42	0.39	52.54	4.96		
48.34	0.01	50.46	0.44	52.58	5.81		
48.38	0.01	50.50	0.48	52.62	6.89		
48.42	0.01	50.54	0.53	52.66	8.15		
48.46	0.02	50.58	0.58	52.70	9.56		
48.50	0.02	50.62	0.63	52.74	11.11		
48.54	0.02	50.66	0.69	52.78	12.79		
48.58	0.02	50.70	0.74	52.82	14.58		
		l		l			

## FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.08)

Type/Node Name: Bioretention Pond #4 (HydroCAD Node #83P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		Charlest various at the restrictions on unlined systems authord in Fau Wa 1500.0	0/0)
0.33	-	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	δ(a).
	_	A = Area draining to the practice	
0.24	_	A <sub>1</sub> = Impervious area draining to the practice	
	decimal	I = Percent impervious area draining to the practice, in decimal form	
	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)  WQV= 1" x Rv x A	
844	ac-in	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
211	_	25% x WQV (check calc for sediment forebay volume)	
633	_	75% x WQV (check calc for surface sand filter volume)	
	CB	Method of Pretreatment? (not required for clean or roof runoff)	
	cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate ti		if system IS NOT underdrained:	
Carcalate ti	sf	A <sub>SA</sub> = Surface area of the practice	
	_		
	iph -	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>	
	v. (b)	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	. 70 L
	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
		if system IS underdrained:	
47.00	_ft _	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)	
0.03	cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)	
15.63	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	<u>&lt;</u> 72-hrs
44.00	feet	$E_{FC}$ = Elevation of the bottom of the filter course material <sup>2</sup>	
43.00	feet	E <sub>UD</sub> = Invert elevation of the underdrain (UD), if applicable	
43.75	feet	$E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
37.58	feet	$E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)
1.00	feet	$D_{FC \text{ to UD}}$ = Depth to UD from the bottom of the filter course	<u>≥</u> 1'
6.42	feet	$D_{FC \text{ to ROCK}}$ = Depth to bedrock from the bottom of the filter course	<u>≥</u> 1'
0.25	feet	D <sub>FC to SHWT</sub> = Depth to SHWT from the bottom of the filter course	<u>≥</u> 1'
48.63		Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
49.00	_	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface	sand filter	or underground sand filter is proposed:	
YES	ac	Drainage Area check.	< 10 ac
833	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> 75%WQV
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sheet	<del>-</del> :	Note what sheet in the plan set contains the filter course specification.	
1		-	•
	Yes/No	Access grate provided?	← yes

If a biorete	ention area	is proposed:	
YES	ac	Drainage Area no larger than 5 ac?	← yes
873	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> WQV
18.0	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA
Sheet	C-15	Note what sheet in the plan set contains the filter course specification	
3.0	<u>:</u> 1	Pond side slopes	<u>&gt; 3</u> :1
Sheet	: L1 & L2	Note what sheet in the plan set contains the planting plans and surface cover	
If porous p	avement is	proposed:	
		Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres	A <sub>SA</sub> = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA
Sheet	-	Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat<sub>design</sub> includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:					
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·		·		·	

### Stage-Area-Storage for Pond 83P: Bio #4

Elevation	Surface	Storage	Elevation	Surface	Storage	
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	
44.00	315	0	46.65	668	579	
44.05	315	1	46.70	685	613	
44.10	315	2	46.75	702	647	
44.15	315	2	46.80	718	683	
44.20	315	3	46.85	735	719	
44.25	315	4	46.90	752	756	
44.30	315	5	46.95	768	794	MOV - 044 of
44.35	315	6	47.00	785	833	WQV = 844 cf
44.40	315	6	47.05	806	873	Ewqv = 47.00
44.45	315	7	47.10	826	914	Laviant Outlat
44.50	315	8	47.15	847	956	Lowest Outlet =
44.55	315	9	47.20	868	998	<b>└</b>  47.05
44.60	315	9	47.25	889	1,042	Available WQV =
44.65	315	10	47.30	909	1,087	873 cf
44.70	315	11	47.35	930	1,133	0/3 CI
44.75	315	12	47.40	951	1,180	
44.80	315	13	47.45	971	1,228	
44.85	315	13	47.50	992	1,277	
44.90	315	14	47.55	1,013	1,327	
44.95	315	15	47.60	1,033	1,379	
45.00	315	16	47.65	1,054	1,431	
45.05	315	17	47.70	1,075	1,484	
45.10	315	17	47.75	1,096	1,538	
45.15	315	18	47.80	1,116	1,594	
45.20	315	19	47.85	1,137	1,650	
45.25	315	20	47.90	1,158	1,707	
45.30	315	20	47.95	1,178	1,766	
45.35	315	21	48.00	1,199	1,825	
45.40	315	22	48.05	1,224	1,886	
45.45	315	23	48.10	1,248	1,947	
45.50	315	24	48.15	1,273 1,297	2,011	
45.55 45.60	329 342	40 56	48.20 48.25		2,075	
45.60 45.65	342 356	74	48.30	1,322	2,140 2,207	
45.65 45.70	369	92	48.35	1,347 1,371	2,207 2,275	
45.75	383	111	48.40	1,396	2,344	
45.80	397	130	48.45	1,420	2,344 2,414	
45.85	410	151	48.50	1,445	2,486	
45.90	424	171	48.55	1,470		
45.95	437	193	48.60	1,494	2,559 2,633	
46.00	451	215	48.65	1,519	2,708	
46.05	468	238	48.70	1,543	2,785	
46.10	484	262	48.75	1,568	2,863	
46.15	501	287	48.80	1,593	2,942	
46.20	518	312	48.85	1,617	3,022	
46.25	535	338	48.90	1,642	3,103	
46.30	551	365	48.95	1,666	3,186	
46.35	568	393	49.00	1,691	3,270	
46.40	585	422	10.00	.,	J, 21 U	
46.45	601	452				
46.50	618	482				
46.55	635	514				
46.60	651	546				
	•••					

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### Stage-Discharge for Pond 83P: Bio #4

Elevation	Primary	Elevation	Primary	
(feet)	(cfs)	(feet)	(cfs)	
44.00	0.00	46.65 46.70	0.02	
44.05 44.10	0.00 0.00	46.70 46.75	0.02 0.02	
44.10 44.15	0.00	46.80	0.02	
44.13	0.00	46.85	0.02	
44.25	0.00	46.90	0.02	
44.30	0.00	46.95	0.03	
44.35	0.00	47.00	0.03	O
44.40	0.00	47.05	0.03	Qwqv = 0.03 cfs
44.45	0.00	47.10	0.04	
44.50	0.00	47.15	0.05	
44.55	0.00	47.20	0.08	
44.60	0.00	47.25	0.12	
44.65	0.00	47.30	0.15	
44.70	0.00	47.35	0.19	
44.75	0.00	47.40 47.45	0.22	
44.80 44.85	0.00 0.00	47.45 47.50	0.24 0.26	
44.83	0.00	47.55	0.28	
44.95	0.00	47.60	0.20	
45.00	0.00	47.65	0.32	
45.05	0.00	47.70	0.34	
45.10	0.00	47.75	0.35	
45.15	0.00	47.80	0.37	
45.20	0.00	47.85	0.38	
45.25	0.00	47.90	0.40	
45.30	0.00	47.95	0.41	
45.35	0.00	48.00	0.42	
45.40	0.00	48.05	0.44	
45.45	0.00	48.10	0.45	
45.50	0.00	48.15	0.46	
45.55 45.60	0.00 0.00	48.20 48.25	0.47 0.49	
45.65	0.00	48.30	0.49	
45.70	0.00	48.35	0.51	
45.75	0.00	48.40	0.52	
45.80	0.00	48.45	0.53	
45.85	0.01	48.50	0.54	
45.90	0.01	48.55	0.84	
45.95	0.01	48.60	1.39	
46.00	0.01	48.65	2.09	
46.05	0.01	48.70	2.92	
46.10	0.01	48.75	3.86	
46.15	0.01	48.80	4.90	
46.20 46.25	0.01 0.01	48.85 48.90	6.03 7.24	
46.25 46.30	0.01	48.95	7.24 8.53	
46.35	0.01	49.00	9.89	
46.40	0.01	10.00	0.00	
46.45	0.02			
46.50	0.02			
46.55	0.02			
46.60	0.02			
	ı			

### **Stage-Area-Storage for Pond 10P: Porous Pavement**

E	0 (	\A/ (( 1	01
Elevation	Surface	Wetted	Storage
(feet)	(sq-ft)	(sq-ft)	(cubic-feet)
0.00	2,761	2,761	0
0.10	2,761	2,780	110
0.20	2,761	2,798	221
0.30	2,761	2,817	331
0.40	2,761	2,836	442
0.50	2,761	2,854	552
0.60	2,761	2,873	663
0.70	2,761	2,891	773
0.80	2,761	2,910	884
0.90	2,761	2,929	994
1.00	2,761	2,947	1,104
1.10	2,761	2,966	1,215
1.20	2,761	2,985	1,325
1.30	2,761	3,003	1,436
1.40	2,761	3,022	1,546
1.50	2,761	3,040	1,657
1.60	2,761	3,059	1,670
1.70	2,761	3,078	1,684
1.80	2,761	3,096	1,698
1.90	2,761	3,115	1,712
2.00	2,761	3,134	1,726
2.10	2,761	3,152	1,739
2.20	2,761	3,171	1,753
2.30	2,761	3,189	1,767
2.40	2,761	3,208	1,781
2.50	2,761	3,227	1,795
2.60	2,761	3,245	1,905
2.70	2,761	3,264	2,016
2.80	2,761	3,283	2,126
2.90	2,761	3,301	2,236
3.00	2,761	3,320	2,347
3.10	2,761	3,338	2,457
3.20	2,761	3,357	2,559
3.30	2,761	3,376	2,642
3.40	2,761	3,394	2,725
3.50	2,761	3,413	2,808

## FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.08)

Type/Node Name: Porous Pavement (HydroCAD Node #10P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

			.0( )				
X 0.22	-	Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	18(a).				
0.23	-	A = Area draining to the practice					
0.23	_	A <sub>I</sub> = Impervious area draining to the practice					
	decimal	I = Percent impervious area draining to the practice, in decimal form					
	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)					
	ac-in	WQV= 1" x Rv x A					
800	_	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")					
200	_	25% x WQV (check calc for sediment forebay volume)					
600		75% x WQV (check calc for surface sand filter volume)					
	В	_ Method of Pretreatment? (not required for clean or roof runoff)	> 250/14/01/				
	cf	V <sub>SED</sub> = Sediment forebay volume, if used for pretreatment	<u>&gt;</u> 25%WQV				
		n if system IS NOT underdrained:					
2,761	sf_	A <sub>SA</sub> = Surface area of the practice					
0.50	iph	Ksat <sub>DESIGN</sub> = Design infiltration rate <sup>1</sup>					
	-	If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?					
	Yes/No	(Use the calculations below)					
7.0	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	< 72-hrs				
Calculate ti	me to drain	n if system IS underdrained:					
	ft	E <sub>WQV</sub> = Elevation of WQV (attach stage-storage table)					
	cfs	$Q_{WQV}$ = Discharge at the $E_{WQV}$ (attach stage-discharge table)					
-	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	<u>&lt;</u> 72-hrs				
	feet	E <sub>FC</sub> = Elevation of the bottom of the filter course material <sup>2</sup>					
	feet	E <sub>UD</sub> = Invert elevation of the underdrain (UD), if applicable					
	feet	$E_{SHWT}$ = Elevation of SHWT (if none found, enter the lowest elevation of the test p	oit)				
	feet	$E_{ROCK}$ = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)				
-	feet	$D_{FC \text{ to UD}}$ = Depth to UD from the bottom of the filter course	<u>≥</u> 1'				
-	feet	$D_{FC \text{ to ROCK}}$ = Depth to bedrock from the bottom of the filter course	<u>≥</u> 1'				
-	feet	$D_{FC \text{ to SHWT}}$ = Depth to SHWT from the bottom of the filter course	<u>≥</u> 1'				
	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)					
	ft	Elevation of the top of the practice					
-		50 peak elevation $\leq$ Elevation of the top of the practice	← yes				
If a surface	If a surface sand filter or underground sand filter is proposed:						
YES	ac	Drainage Area check.	< 10 ac				
	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> 75%WQV				
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA				
Sheet	<del>-</del>	Note what sheet in the plan set contains the filter course specification.					
	Yes/No	Access grate provided?	← yes				
-							

If a biorete	If a bioretention area is proposed:						
YES	ac	Drainage Area no larger than 5 ac?	← yes				
	cf	V = Volume of storage <sup>3</sup> (attach a stage-storage table)	<u>&gt;</u> WQV				
	inches	D <sub>FC</sub> = Filter course thickness	18", or 24" if within GPA				
Shee	t	Note what sheet in the plan set contains the filter course specification					
	:1	Pond side slopes	<u>&gt; 3</u> :1				
Shee	t	Note what sheet in the plan set contains the planting plans and surface cover					
If porous p	avement is	proposed:					
Ası	ohalt	Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)					
0.1	acres	A <sub>SA</sub> = Surface area of the pervious pavement					
3.9	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1				
12.0	inches –	D <sub>FC</sub> = Filter course thickness	12", or 18" if within GPA				
Shee	t C-15	Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)				

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat<sub>design</sub> includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:		
2,808 cf storage provided		

# GROUNDWATER RECHARGE VOLUME (GRV) (Env-Wq 1504.12)

	ac	Area of HSG A soil that was replaced by impervious cover	0.40"	
0.11	ac	Area of HSG B soil that was replaced by impervious cover	0.25"	
1.68	ac	Area of HSG C soil that was replaced by impervious cover	0.10"	
0.01	ac	Area of HSG D soil or impervious cover that was replaced by impervious cover	0.0"	
0.11	inches	Rd = Weighted groundwater recharge depth		
0.1965	ac-in	GRV = AI * Rd		
713	cf	GRV conversion (ac-in x 43,560 sf/ac x 1ft/12")		
	Υ	Is a stage-storage table attached showing that the GRV can be stored below the low	vest	
	invert of the outlet structure (if applicable)? Multiple stormwater control measures may be			
		used to meet the GRV requirements.		

Provide calculations/discussion below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):

2,808 cf provided in porous pavement (Town requires 2,757 cf)

# **Water Quaity Volume Calculations**

Town of Durham, New Hampshire

Project #: 5540 Date: 5/8/2025

HSG	Area (ac)	Ratio	WQV		
Α	0.00	1	0.000	in	GRV
В	0.11	0.75	0.085	in	GRV
С	1.68	0.4	0.673	in	GRV
D	0.01	0.16	0.002	in	GRV
			0.760	ac-in	Total GRV = AI*Rd
			2757.93	cf	GRV Conversion (ac-in x 43560sf/ac x 1'/12")
			0.063	af	

2,808 cf (0.064 cf) storage provided in porous pavement



# Location: Bio #1, 15" Culvert (HydroCAD Pond #17P)

Project: 5440 Date: 6/25/2025 By: EBS

La	Apron Length, Ft.	Calculated
Tw	Tailwater, Ft.	0.2
Q	Flow, 10 Yr Storm, CFS	0.73
D50	Median Stone Dia., Ft.	Calculated
D	Depth of Stone, In	Calculated
Do	Pipe Diameter, Ft	1.25
W1	Width @ Start, Ft.	Calculated
W2	Width @ End, Ft	Calculated
W	Width of Channel	4

W1:

3(Do)= 3.75 Ft.

Width @ Start: 4 Ft.

D50:  $0.02(Q)^{4/3}$  D50= 0.05 Ft.

or 0.6 In.

Median Stone Size: 6 In.

D: 2.25\*D50 **Depth of Riprap: 14 In.** 

La: If  $Tw \le Do/2$ : Do/2 = 0.625 Ft.

 $La=1.8Q/Do^{3/2}+7Do \qquad \qquad Tw= \qquad 0.2 \ \text{Ft.}$  and  $W2=width \ of \ channel$ 

W2=width of channel or

If Tw>Do/2:

 $La=3Q/Do^{3/2} + 7Do$ 

W2=3Do+La

and W2=width of channel

or

Length of Apron:	10 Ft.
Width @ End:	4 Ft.



# Location: Bio #2, 15" Culvert (HydroCAD Pond #22P)

Project: 5440 Date: 6/25/2025 By: EBS

La	Apron Length, Ft.	Calculated
Tw	Tailwater, Ft.	0.1
Q	Flow, 10 Yr Storm, CFS	0.37
D50	Median Stone Dia., Ft.	Calculated
D	Depth of Stone, In	Calculated
Do	Pipe Diameter, Ft	1.25
W1	Width @ Start, Ft.	Calculated
W2	Width @ End, Ft	Calculated
W	Width of Channel	4

W1:

3(Do)= 3.75 Ft.

Width @ Start: 4 Ft.

D50:  $0.02(Q)^{4/3}$  D50= 0.09 Ft.

or 1.0 In.

Median Stone Size: 6 In.

D: 2.25\*D50 **Depth of Riprap: 14 In.** 

La: If  $Tw \le Do/2$ : Do/2 = 0.625 Ft.

 $La=1.8Q/Do^{3/2} + 7Do$  Tw= 0.05 Ft.

and W2=width of channel or

W2=3Do+La

If Tw>Do/2:  $La=3Q/Do^{3/2} + 7Do$ 

and W2=width of channel

01

Length of Apron:	10 Ft.
Width @ End:	4 Ft.



# Location: DMH #12, 15" Culvert (HydroCAD Pond #50P)

By: EBS Project: 5440 Date: 6/25/2025

La	Apron Length, Ft.	Calculated
Tw	Tailwater, Ft.	3.2
Q	Flow, 10 Yr Storm, CFS	3.11
D50	Median Stone Dia., Ft.	Calculated
D	Depth of Stone, In	Calculated
Do	Pipe Diameter, Ft	1.25
W1	Width @ Start, Ft.	Calculated
W2	Width @ End, Ft	Calculated
W	Width of Channel	4

W1:

3(Do)=3.75 Ft.

Width @ Start: 4 Ft.

D50: D50= 0.02 Ft.

> 0.3 In. or

> > **Median Stone Size:** 6 In.

Depth of Riprap: 14 In. D: 2.25\*D50

La: If  $Tw \le Do/2$ : Do/2=0.625 Ft.

 $La=1.8Q/Do^{3/2} + 7Do$ Tw=3.15 Ft.

W2=width of channel and or

W2=3Do+La

If Tw>Do/2:  $La=3Q/Do^{3/2} + 7Do$ 

W2=width of channel

and

Length of Apron:	16 Ft.
Width @ End:	4 Ft.



# Location: Bio #3, 18" Culvert (HydroCAD Pond #69P)

Project: 5440 Date: 6/25/2025 By: EBS

La	Apron Length, Ft.	Calculated
Tw	Tailwater, Ft.	0.1
Q	Flow, 10 Yr Storm, CFS	2.47
D50	Median Stone Dia., Ft.	Calculated
D	Depth of Stone, In	Calculated
Do	Pipe Diameter, Ft	1.50
W1	Width @ Start, Ft.	Calculated
W2	Width @ End, Ft	Calculated
W	Width of Channel	4

W1:

3(Do)= 4.5 Ft.

Width @ Start: 5 Ft.

D50:  $0.02(Q)^{4/3}$  D50= 0.44 Ft.

or 5.3 In.

Median Stone Size: 6 In.

D: 2.25\*D50 **Depth of Riprap: 14 In.** 

La: If  $Tw \le Do/2$ : Do/2= 0.75 Ft.

 $La=1.8Q/Do^{3/2}+7Do \qquad \qquad Tw= \qquad \qquad 0.1 \ \ Ft.$  and  $W2=width \ of \ channel$ 

or

If Tw>Do/2:

 $La=3Q/Do^{3/2}+7Do$  and  $W2=width\ of\ channel$ 

W2=3Do+La

0

Length of Apron:	13 Ft.
Width @ End:	4 Ft.



# Location: Bio #4, 15" Culvert (HydroCAD Pond #83P)

Project: 5440 Date: 6/25/2025 By: EBS

La	Apron Length, Ft.	Calculated
Tw	Tailwater, Ft.	0.1
Q	Flow, 10 Yr Storm, CFS	0.46
D50	Median Stone Dia., Ft.	Calculated
D	Depth of Stone, In	Calculated
Do	Pipe Diameter, Ft	1.25
W1	Width @ Start, Ft.	Calculated
W2	Width @ End, Ft	Calculated
W	Width of Channel	4

W1:

3(Do)= 3.75 Ft.

Width @ Start: 4 Ft.

D50:  $0.02(Q)^{4/3}$  D50= 0.06 Ft.

or 0.7 In.

Median Stone Size: 6 In.

D: 2.25\*D50 **Depth of Riprap: 14 In.** 

La: If  $Tw \le Do/2$ : Do/2 = 0.625 Ft.

 $La=1.8Q/Do^{3/2} + 7Do$  Tw= 0.1 Ft.

and W2=width of channel or

W2=3Do+La

If Tw>Do/2:

 $La=3Q/Do^{3/2} + 7Do$ 

and W2=width of channel

or

Length of Apron:	10 Ft.
Width @ End:	4 Ft.



# **LEVEL SPREADER CALCULATIONS**

Location: Bio #3 Outfall (Reach #70R)					
Project:	5440	Date: 6/25/2025	By: EBS		
Based on I	Maine Volume III	BMP's Technical Desig	n Manual		
Level Spre	eader Length base	d on 10-Year 24-Hour st	form at 0.25 cfs per foot	i.	
10-Year Po	eak Rate:	2.47 cfs			
Required	Length:	9.88 feet			



# **LEVEL SPREADER CALCULATIONS**

Location: Bio #4 Outfall (Reach #83R)								
Project:	5440	Date: 6/25/2025	By: EBS					
Based on Maine Volume III BMP's Technical Design Manual								
Level Spreader Length based on 10-Year 24-Hour storm at 0.25 cfs per foot.								
10-Year P	eak Rate:	0.49 cfs						
Required	Length:	1.96 feet						



# Section 8

Stormwater Operations & Maintenance Plan Inspection Form Stormwater Management Plan



## STORMWATER INSPECTION AND MAINTENANCE MANUAL

# RiverWoods Phase II Assessor's Map 209, Lot 33

## OWNER:

RiverWoods Company at Durham 14 Stone Quarry Drive Durham, NH 03824

Proper inspection, maintenance, and repair are key elements in maintaining a successful stormwater management program on a developed property. Routine inspections ensure permit compliance and reduce the potential for deterioration of infrastructure or reduced water quality. The following responsible parties shall be in charge of managing the stormwater facilities:

## **RESPONSIBLE PARTIES:**

Owner:	RiverWoods Durham	(603) 590-4001	
	Name	Company	Phone
Inspection:	RiverWoods Durham		(603) 590-4001
·	Name	Company	Phone
Maintenance	e: RiverWoods Durham		(603) 590-4001
	Name	Company	Phone

## **NOTES:**

Written inspection forms and maintenance logs shall be completed yearly by a qualified inspector retained the owner or assigns on or before January 31<sup>st</sup> of each year and a copy retained at the site's business office.

Photographs of each stormwater BMP are to be taken at each inspection and submitted with the annual inspection reports.

Inspection and maintenance responsibilities shall transfer to any future property owner(s).

This manual shall be updated as needed to reflect any changes related to any transfer of ownership and/or any delegation of inspection and maintenance responsibilities to another entity



## **BIORETENTION PONDS (AKA RAINGARDENS)**

*Function* – Bioretention ponds provide treatment to runoff prior to directing it to stormwater systems by filtering sediment and suspended solids, trapping them in the bottom of the garden and in the filter media itself. Additional treatment is provided by the native water-tolerant vegetation which removes nutrients and other pollutants through bio-uptake. Stormwater detention and infiltration can also be provided as the filtering process slows runoff, decreases the peak rate of discharge and promotes groundwater recharge.

Bioretention ponds shall be managed (Per AGR 3800 and RSA 430:53) to: prevent and control the spread of invasive plant, insect, and fungal species; minimize the adverse environmental and economic effects invasive species cause to agriculture, forests, wetlands, wildlife, and other natural resources of the state; and protect the public from potential health problems attributed to certain invasive species.

#### Maintenance

- Inspect annually and after significant rainfall events.
- If a raingarden does not completely drain within 72-hours following a rainfall event, then a qualified professional shall be retained to assess the condition of the facility to determine measures required to restore its filtration and/or infiltration function(s), including but not limited to removal of accumulated sediments and/or replacement or reconstruction of the filter media. Filter media shall be replaced with material matching the specification on the design drawings or the NHDES Stormwater Manual.
- Replace any riprap dislodged from spillways, inlets and outlets.
- Remove any obstructions, litter and accumulated sediment or debris as warranted but no less than once a year.
- Mowing of any grassed area in or adjacent to a raingarden, including its berm, shall be performed at least twice per year (when areas are not inundated) to keep the vegetation in vigorous condition. The cut grass shall be removed to prevent the decaying organic litter from clogging the filter media or choking other vegetation.
- Select vegetation should be maintained in healthy condition. This may include pruning, removal and replacement of dead or diseased vegetation.
- Remove any invasive species, Per AGR 3800 and RSA 430:53.
- Remove any hard wood growth from raingardens.

#### **CULVERTS AND DRAINAGE PIPES**

*Function* – Culverts and drainage pipes convey stormwater away from buildings, walkways, and parking areas and to surface waters or closed drainage systems.

#### Maintenance

- Culverts and drainage pipes shall be inspected semi-annually, or more often as needed, for accumulation of debris and structural integrity. Leaves and other debris shall be removed from the inlet and outlet to insure the functionality of drainage structures. Debris shall be disposed of on site where it will not concentrate back at the drainage structures or at a solid waste disposal facility.
- Riprap Areas Culvert outlets and inlets shall be inspected during annual maintenance and operations for erosion and scour. If scour or creek erosion is identified, the outlet owner shall take appropriate means to prevent further erosion. Increased lengths of riprap may require a NHDES Permit and/or local permit.

### **DEEP SUMP CATCH BASINS**

Function – Catch basins collect stormwater, primarily from paved surfaces and roofs. Stormwater from paved areas often contains sediment and contaminants. Catch basin sumps serve to trap sediment, trace metals, nutrients and debris. Hooded catch basins trap hydrocarbons and floating debris.

## Maintenance

- Remove leaves and debris from structure grates on an as-needed basis.
- Sumps shall be inspected and cleaned annually and any removed sediment and debris shall be disposed of at a solid waste disposal facility.

## RIP RAP OUTLETS, SWALES, LEVEL SPREADERS AND BUFFERS

*Function* – Rip rap outlets slow the velocity of runoff, minimizing erosion and maximizing the treatment capabilities of associated buffers. Vegetated buffers, either forested or meadow, slow runoff which promotes and reduces peak rates of runoff. The reduced velocities and the presence of vegetation encourage the filtration of sediment and the limited bio-uptake of nutrients.

#### Maintenance

- Inspect riprap, level spreaders and buffers at least annually for signs of erosion, sediment buildup, or vegetation loss.
- Inspect level for signs of condensed flows. Level spreader and rip rap shall be maintained to disperse flows evenly over level spreader.
- If a meadow buffer, provide periodic mowing as needed to maintain a healthy stand of herbaceous vegetation.
- If a forested buffer, then the buffer should be maintained in an undisturbed condition, unless erosion occurs.
- If erosion of the buffer (forested or meadow) occurs, eroded areas should be repaired and replanted with vegetation similar to the remaining buffer. Corrective action should include eliminating the source of the erosion problem and may require retrofit or reconstruction of the level spreader.
- Remove debris and accumulated sediment and dispose of properly.

### LANDSCAPED AREAS - FERTILIZER MANAGEMENT

*Function* – Fertilizer management involves controlling the rate, timing and method of fertilizer application so that the nutrients are taken up by the plants thereby reducing the chance of polluting the surface and ground waters. Fertilizer management can be effective in reducing the amounts of phosphorus and nitrogen in runoff from landscaped areas, particularly lawns.

## Maintenance

- Have the soil tested by your landscaper or local Soil Conservation Service for nutrient requirements and follow the recommendations.
- Do not apply fertilizer to frozen ground.
- Clean up any fertilizer spills.
- Do not allow fertilizer to be broadcast into water bodies.
- When fertilizing a lawn, water thoroughly, but do not create a situation where water runs off the surface of the lawn.

### LANDSCAPED AREAS - LITTER CONTROL

*Function* – Landscaped areas tend to filter debris and contaminates that may block drainage systems and pollute the surface and ground waters.

### Maintenance

- Litter Control and lawn maintenance involves removing litter such as trash, leaves, lawn clippings, pet wastes, oil and chemicals from streets, parking lots, and lawns before materials are transported into surface waters.
- Litter control shall be implemented as part of the grounds maintenance program.

## **VEGETATIVE SWALES**

*Function* – Vegetative swales filter sediment from stormwater, promote infiltration, and the uptake of contaminates. They are designed to treat runoff and dispose of it safely into the natural drainage system.

#### Maintenance

- Timely maintenance is important to keep a swale in good working condition. Mowing of grassed swales shall be monthly to keep the vegetation in vigorous condition. The cut vegetation shall be removed to prevent the decaying organic litter from adding pollutants to the discharge from the swale.
- Fertilizing shall be bi-annual or as recommended from soil testing.
- Inspect swales following significant rainfall events.
- Woody vegetation shall not be allowed to become established in the swales or rock riprap outlet protection and if present shall be removed.
- Accumulated debris disrupts flow and leads to clogging and erosion. Remove debris and litter as necessary.
- Inspect for eroded areas. Determine cause of erosion and correct deficiency as required. Monitor repaired areas.

## **POROUS PAVEMENT**

*Function* – Porous pavement is designed to capture rainwater runoff containing suspended solids, nutrients and pollutants. Proper maintenance of porous pavement is crucial for ensuring its longevity and functionality to infiltrate runoff.

#### Maintenance

- Signs shall be installed indicating the location of porous pavement and the special maintenance required.
- New porous pavement shall be inspected several times in the first month after construction and at least annually thereafter. Inspections shall be conducted after major storms to check for surface ponding that might indicate possible clogging.
- Inspect annually for pavement deterioration or spalling.
- Vacuum sweeping shall be performed 2-4 times a year. Power washing may be required prior to vacuum sweeping to dislodge trapped particles.
- Sand and abrasives shall not be used for winter maintenance, as they will clog the pores; deicing materials shall be used instead.
- Never reseal or repave with impermeable materials. If the porous pavement is damaged, it can be repaired using conventional, non-porous patching mixes as long as the cumulative area repaired does not exceed 10 percent of the paved area.

#### CONTROL OF INVASIVE PLANTS

*Function* – Invasive plants are introduced, alien, or non-native plants, which have been moved by people from their native habitat to a new area. Some exotic plants are imported for human use such as landscaping, erosion control, or food crops. They also can arrive as "hitchhikers" among shipments of other plants, seeds, packing materials, or fresh produce. Some exotic plants become invasive and cause harm by:

- becoming weedy and overgrown;
- killing established shade trees;
- obstructing pipes and drainage systems;
- forming dense beds in water;
- lowering water levels in lakes, streams, and wetlands;
- destroying natural communities;
- promoting erosion on stream banks and hillsides; and
- resisting control except by hazardous chemical.

#### Maintenance

During maintenance activities, check for the presence of invasive plants and remove in a safe manner as described in the attached "Methods for Disposing Non-Native Invasive Plants" prepared by the UNH Cooperative Extension.

## STREET/PARKING LOT SWEEPING (NON-POROUS PAVEMENT)

*Function* – Parking lots accumulate sand and debris. Street sweeping removes the sand and debris, which lowers transport of sediment and pollutants the stormwater systems and into the environment.

#### Maintenance

• A regular periodic cleaning schedule is recommended. The more frequent, the greater the sediment and pollutant removal. Regular cleaning of paved areas reduces the frequency of cleaning catch basins and drainage systems. It is recommended that the parking lots and access ways shall be swept at least once a month during winter months.

### **GENERAL CLEAN UP**

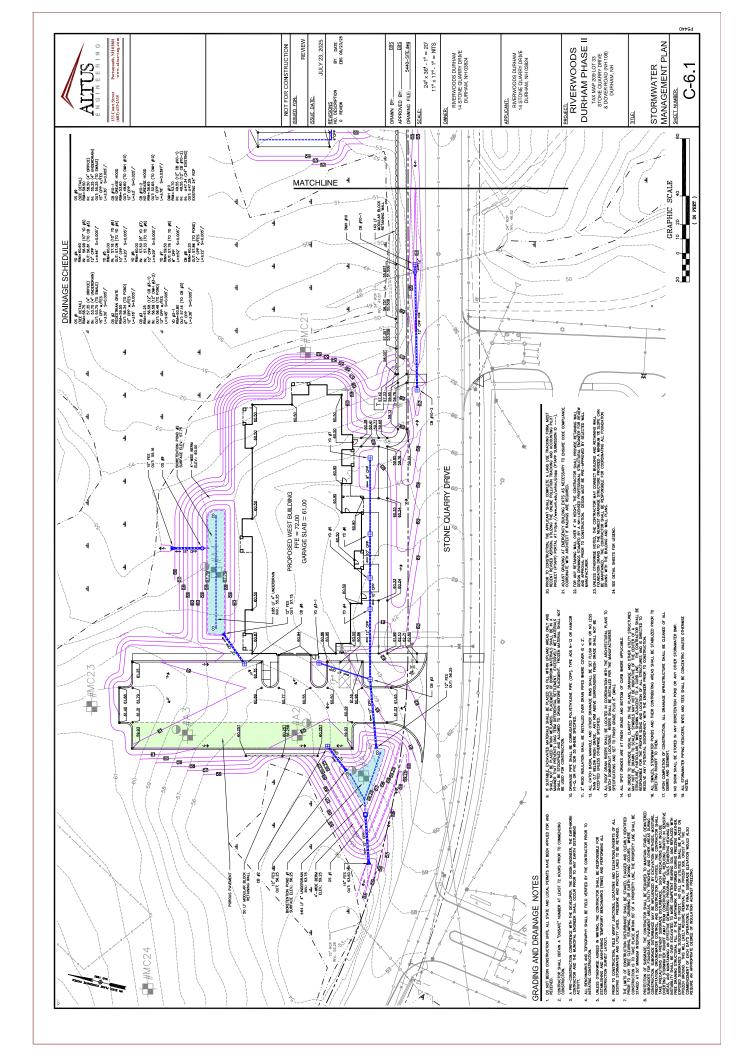
- Upon completion of the project, the contractor shall remove all temporary stormwater structures (i.e., temporary stone check dams, silt fence, temporary diversion swales, catch basin inlet filter, etc.). Any sediment deposits remaining in place after the silt fence or filter barrier is no longer required shall be dressed to conform to the existing grade, prepared, and seeded. Remove any sediment in catch basins and clean drain pipes that may have accumulated during construction.
- Once in operation, all paved areas of the site should be swept at least once annually at the end of winter/early spring prior to significant spring rains.

# **APPPENDIX**

- A. Stormwater System Operations and Maintenance ReportB. Site Grading and Drainage Plan

# STORM WATER SYSTEM OPERATION AND MAINTENANCE REPORT

General Information								
Project Name								
Owner								
Inspector's Name(s)								
Inspector's Contact Information								
Date of Inspection			Start Time:	End Time:				
Type of Inspection: Annual Report Due to a discharge of significant amounts of sediment								
Notes:								
	General Site Qu	estions and Dis	charges of Significant Amounts of Sedin	nent				
Sub	ject	Status	Notes					
			ndicated by (but is not limited to) observations	of the following.				
Note	e whether any are observed during	g this inspection:						
			Notes/ Action taken:					
1	Do the current site conditions ref the attached site plan?	□No						
2	Is the site permanently stabilized							
	temporary erosion and sediment	□No						
	controls are removed, and stormy							
	discharges from construction acti are eliminated?							
3	Is there evidence of the discharge							
	significant amounts of sediment							
	surface waters, or conveyance sy	stems						
	leading to surface waters?							
		Permit	Coverage and Plans					
ш	DMD/E 2124			Data Carrantal				
#	BMP/Facility	Inspected	Corrective Action Needed and Notes	Date Corrected				
	Catch Basins and Yard Drains	□Yes						
		□No						
	Drainage Pipes	□Yes						
		□No □Yes						
	Porous Pavement							
Riprap Aprons		□No □Yes						
Tupiup Apions		□No						
Site Vegetation		□Yes						
Bioretention Ponds		□No □Yes						
		□No						
		□Yes						
		□No						
		□Yes □No						





# Section 9

# Watershed Plans

Pre-Development Drainage Plan
Pre-Development Soils Plan
Post-Development Drainage Plan
Post-Development Soils Plan



