



## TOWN OF DURHAM STORMWATER MANAGEMENT PLAN

**REVISED: MARCH 2021** 

TOOMERFS, LLC 19 MAIN STREET and 21 MAIN STREET TAX MAP 5, LOTS 1-9, 1-10, 1-15, and 1-16 Durham, New Hampshire





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# TOWN OF DURHAM STORMWATER MANAGEMENT PLAN FOR TOOMERFS, LLC

19 MAIN STREET and 21 MAIN STREET TAX MAP 5, LOTS 1-9, 1-10, 1-15 and 1-16

**DURHAM, NEW HAMPSHIRE** 

OCTOBER 2020 REVISED MARCH 2021

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# **SECTION 1.0 PROJECT INFORMATION NARRATIVE**



#### 1.1.1 Project Summary

Toomerfs, LLC intents to develop a parking facility at 19 and 21 Main Street, in Durham, New Hampshire, on Tax Map 5, Lots 1-9, 1-10, 1-15, and 1-16. The parking facility will serve the apartments at the front of the site, as well as providing needed extra parking capacity for the Main Street area. Additionally, the driveway to the site will be reconstructed to improve clearances to the existing buildings.

The parking area will be constructed on a filled pad, supported by an engineered pre-cast retaining wall on the south end of the site. Fill and grading for subgrade preparation will be required to complete the pad improvements. The total disturbance for this work is 79,700 square feet. Stormwater from the parking area will be directed via sheet flow to grass swales leading to catchbasins feeding an underground ADS Stormtech MC4500 chamber system within the fill area. The chambers will allow infiltration into the fill area and to native ground. An overflow structure is provided to control flowrates for larger storm events.

The following table shows the 1-inch storm; 2, 10, 25, 50, and 100 year peak flow rate comparison at the discharge points.

Pre Pre Pre Post Post Post Pre Post Pre Post Pre Post 2 Yr 50 Yr 50 Yr Watershed 1 In 1 In 2 Yr 10 Yr 10 Yr 25 Yr 25 Yr 100 Yr 100 Yr Flow Flow Flow Flow Flow Flow Flow Flow Area Flow Flow Flow Flow Discharge Rate Point (cfs) DP-1 2.17 2.15 5.29 5.28 7.23 10.72 9.04 14.01 0.00 0.00 8.03 13.82 1.19 DP-2 0.13 0.10 0.66 0.56 1.07 0.92 1.38 1.68 1.45 2.03 1.76

Table 1.0 – 1 Inch; 2, 10, 25, 50, and 100 Year Comparison

Impacts to watershed water quality from grading within the watersheds would be likely to occur from uncontrolled discharge of site runoff during construction activities and stabilized post-project surfaces. To minimize the impacts to the watersheds, the site has been designed to cause no increase in runoff and erosion control methods have been sized in accordance with the Env-Wq 1500 and the *New Hampshire Stormwater Management Manual* (December, 2008).

#### 1.1.2 Existing Site Conditions

The proposed work is located on the south side of Main Street approximately 0.10 miles east of the intersection of Newmarket Road. The primary project site is located behind existing residential apartments.

The project site currently consists of forest sloping to the south down to College Brook. The upper portion of the site includes four residences, a garage, and 43 paved parking spaces.

There are existing no delineated wetlands located with the project disturbance area, and no wetland impacts are proposed as part of this project. Wetland exists in the extreme south of the property; buffer areas are to be maintained to the wetlands.

#### 1.1.3 Proposed Site Conditions & Disturbances

The project proposes the removal of an existing structure, reconstruction of the site's driveway, and construction of a 153-space parking lot. To create the relatively level area required for the parking lot, an engineered concrete block retaining wall will be constructed, and significant quantities of engineered fill will be imported to the site. An underground chamber system is proposed to detain and infiltrate stormwater from the site. In the immediate vicinity of the chamber system, the imported fill will be design to produce a hydraulic conductivity matching the underlying soils.

Approximately 79,700 square feet of earth disturbance will be required to construct the driveway improvements and parking lot, and associated utilities and drainage practices. An area of disturbance breakdown has been shown in **Table 1.1**.

Construction/Disturbance Activity

Grading and Site Disturbance

79,700

Total Impervious Area (within drainage area)

Total Undisturbed Area (within drainage area)

28,991

Area
(% EIC\*
% UDC\*

79,700

22.4%

Table 1.1 – Proposed Disturbance Area Breakdown

Total Drainage Area<sup>1</sup>

The total connected Effective Impervious Cover is 56.6% of the proposed disturbance area, and the total undisturbed area is 22.4% within the entire modeled drainage area.

129,549

The impacts to water quality during site development will be minimized using erosion control measures. Frequent site inspections during construction are required during or directly following rainfall events to ensure erosion control devices are working properly. A copy of the Stormwater Inspection and Maintenance Manual can be found in **Section 2.8** of this report.

<sup>\*</sup> EIC = Effective Impervious Cover

<sup>\*</sup> *UDC* = *Undisturbed Cover* 

#### 1.1.4 Rainfall Data

Using SCS TR-20, run under HydroCAD Version 10.0 with Type III-24 hour rainfall events, pre- and post-development cover types and drainage paths were modeled to generate peak discharge rates. Rainfall events modeled have intensities described by data provided by the Northeast Regional Climate Center for the geographic location of the project. These data are provided in full in section 2.13 of this report, and are summarized below in **Table 1.2**.

Table 1.2 - Type II, 24 Hour Rainfall Depths for Project Site (43.133°N, 70.923°W)

Rainfall Event	Depth*
1-Inch	1.00"
2-Year	3.14"
10-Year	4.76"
25-Year	6.03"
50-Year	7.22"
100-Year	8.64"

<sup>\*</sup> Rainfall depths from the Northeast Regional Climate Center Extreme Precipitation Tables, http://precip.eas.cornell.edu, accessed 20 October 2020, See section 2.13

#### 1.1.5 Peak Runoff Control Requirement

Town of Durham Site Design Standards require that measures be taken to control the post-development peak rate runoff so that it does not exceed pre-development runoff for the 2-year, 10-year, and 17-year\*, 24-hour storm events. Due to the post-project grading of the site and changes in land cover, stormwater devices were used to attenuate flow in order to meet these Peak Runoff Control requirements. **Table 1.3** summarizes the stormwater runoff peak flow rate for the 1 inch, 2, 10 and 25 year storm events. Additionally, for reference we are providing a comparison of the 50 and 100 year storm events in the table.

Table 1.3 – Reprint of Table 1.0 – 1 Inch; 2, 10, 25, 50, and 100 Year Comparison

	Pre	Post	Pre	Post								
Watershed	1 In	1 In	2 Yr	2 Yr	10 Yr	10 Yr	25 Yr	25 Yr	50 Yr	50 Yr	100 Yr	100 Yr
Area	Flow	Flow										
Discharge	Rate	Rate										
Point	(cfs)	(cfs)										
DP-1	0.00	0.00	2.17	2.15	5.29	5.28	8.03	7.23	10.72	9.04	14.01	13.82
DP-2	0.13	0.10	0.66	0.56	1.07	0.92	1.38	1.19	1.68	1.45	2.03	1.76

<sup>\*</sup>Understood to be a typo, and the 25-year event is intended.

#### 1.1.6 Runoff Volume Requirement

Town of Durham Site Design Standards require that measures be taken to control the post-development peak rate runoff so that it does not exceed pre-development runoff for the 2-year, 10-year, and 17-year\*, 24-hour storm events. Additionally, shown in the table for reference, are the 50 and 100 year storm events. Receiving waters and downstream wetland channels must be protected from erosion and sedimentation resulting from the project development. **Table 1.1** summarizes the flow volume data. While runoff volumes for larger events increase at Dp-1, overall volumes are reduced.

Table 1.4 – 1 Inch; 2, 10, 25, 50, and 100 Year Volume Comparison

	Pre	Post										
	1 In	1 In	2 Yr	2 Yr	10 Yr	10 Yr	25 Yr	25 Yr	50 Yr	50 Yr	100 Yr	100 Yr
Watershed Area	Volume											
Discharge Point	(af)											
DP-1	0.003	0.000	0.201	0.207	0.454	0.505	0.680	0.761	0.906	1.008	1.186	1.310
DP-2	0.009	0.007	0.050	0.042	0.082	0.070	0.109	0.093	0.133	0.114	0.162	0.140

#### 1.1.7 Infiltration Volume Requirement

Town of Durham Site Design Standards require that a portion of the stormwater runoff be infiltrated to protect groundwater resources. The amount of groundwater recharge required per soil group, as a ratio of the Water Quality Volume is summarized in **Table 1.5**. To provide stormwater management an infiltrating underground chamber system is proposed, providing 5,301 cubic feet of storage, equivalent to the full water quality volume for the area draining to the structure, for groundwater recharge through infiltration.

**Table 1.5 – Groundwater Recharge Volume Comparison** 

HSG	Total Area [sf]	Impervious Area [sf]	Percent Impervious [%]	Water Quality Volume [cf]	Ratio of Water Quality Volume	Required Volume [cf]
A	0	0	0	0	1.00	0
В	25,556	17,868	69.9	1,441	0.75	1,081
C	70,322	32,753	46.6	2,738	0.40	1,095
D	33,671	22,661	67.3	1,833	0.16	293
	2,469 cf					
	5,310 cf					

<sup>\*</sup>Understood to be a typo, and the 25-year event is intended.

# 1.2 NRCS Soils Information (Web Soils Survey Map)

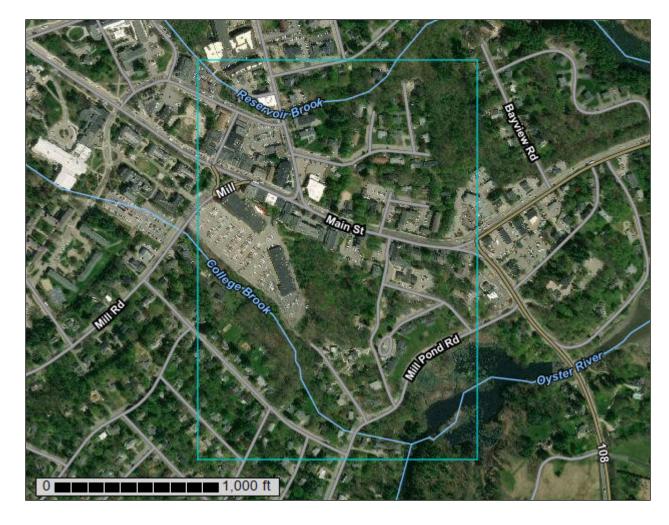


Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Strafford County, New Hampshire



#### **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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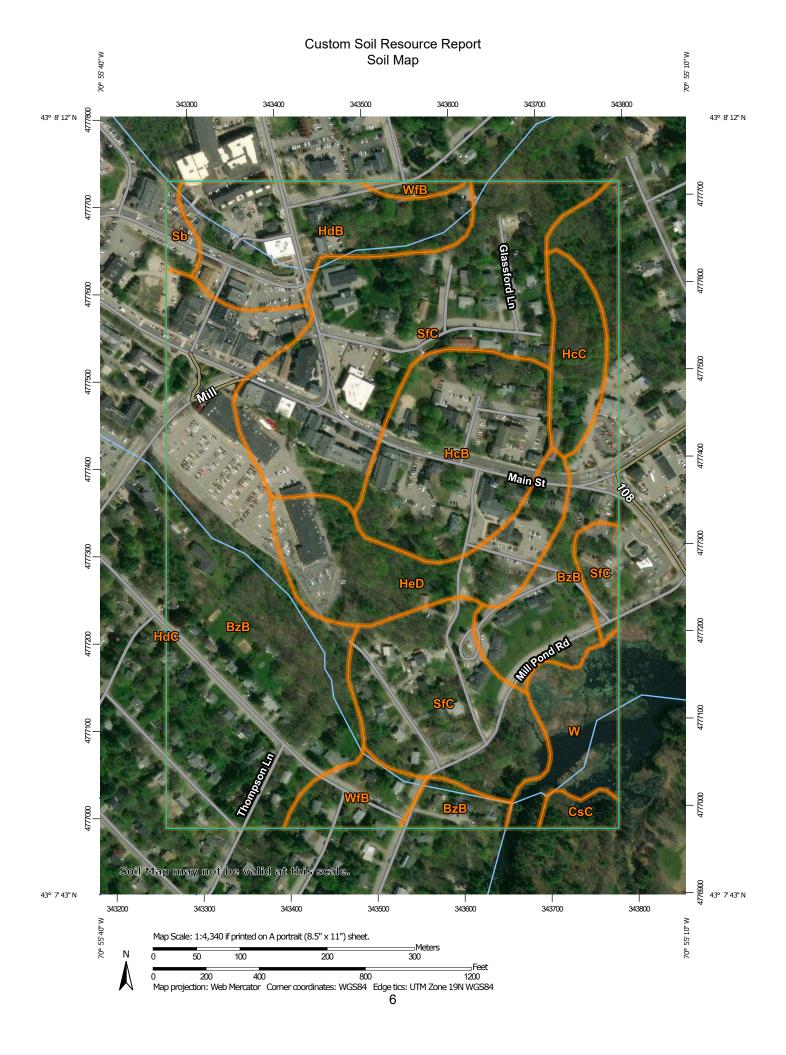
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# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons



Soil Map Unit Lines



Soil Map Unit Points

#### Special Point Features

pecia (©)

Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water
Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot

\_

Severely Eroded Spot

Λ

Sinkhole

Ø

Sodic Spot

Slide or Slip



Spoil Area Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

#### Water Features

\_

Streams and Canals

#### Transportation

ransp

Rails



Interstate Highways



US Routes



Major Roads



Local Roads

#### Background



Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Strafford County, New Hampshire Survey Area Data: Version 20, May 29, 2020

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Dec 31, 2009—Sep 9, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

#### Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BzB	Buxton silt loam, 3 to 8 percent slopes	31.7	33.2%
CsC	Charlton fine sandy loam, 8 to 15 percent slopes, very stony	0.8	0.9%
НсВ	Hollis-Charlton fine sandy loams, 3 to 8 percent slopes	10.0	10.5%
HcC	Hollis-Charlton fine sandy loams, 8 to 15 percent slopes	3.0	3.1%
HdB	Hollis-Charlton very rocky fine sandy loams, 3 to 8 percent slopes	8.2	8.5%
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	0.0	0.0%
HeD	Hollis-Charlton extremely rocky fine sandy loams, 8 to 25 percent slopes	7.5	7.8%
Sb	Saugatuck loamy sand	0.7	0.7%
SfC	Suffield silt loam, 8 to 15 percent slopes	26.9	28.1%
W	Water	4.1	4.3%
WfB	Windsor loamy fine sand, clay subsoil variant, 0 to 8 percent slopes	2.7	2.8%
Totals for Area of Interest		95.6	100.0%

#### **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion

of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### Strafford County, New Hampshire

#### BzB—Buxton silt loam, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d6p

Elevation: 0 to 260 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Buxton and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Buxton**

#### Setting

Parent material: Glaciomarine

#### **Typical profile**

H1 - 0 to 10 inches: silt loam H2 - 10 to 28 inches: silty clay loam H3 - 28 to 43 inches: silty clay

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 12 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 7.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C/D

Ecological site: F145XY006CT - Semi-Rich Moist Lake Plain

Hydric soil rating: No

#### **Minor Components**

#### **Elmwood**

Percent of map unit: 10 percent

Hydric soil rating: No

#### Not named

Percent of map unit: 5 percent

#### CsC—Charlton fine sandy loam, 8 to 15 percent slopes, very stony

#### **Map Unit Setting**

National map unit symbol: 2wh0p

Elevation: 0 to 1,570 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### Map Unit Composition

Charlton, very stony, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Charlton, Very Stony**

#### Setting

Landform: Hills, ground moraines, ridges

Landform position (two-dimensional): Backslope, shoulder, summit

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

#### Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water capacity: Moderate (about 8.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Sutton, very stony

Percent of map unit: 5 percent Landform: Hills, ground moraines

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Paxton, very stony

Percent of map unit: 5 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Linear, convex Across-slope shape: Convex Hydric soil rating: No

#### Chatfield, very stony

Percent of map unit: 3 percent

Landform: Hills, ridges

Landform position (two-dimensional): Summit, backslope, shoulder Landform position (three-dimensional): Crest, side slope, nose slope

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

#### Leicester, very stony

Percent of map unit: 2 percent

Landform: Drainageways, ground moraines, hills, depressions Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear, concave Across-slope shape: Concave Hydric soil rating: Yes

#### HcB—Hollis-Charlton fine sandy loams, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7j Elevation: 0 to 1,020 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Farmland of local importance

#### **Map Unit Composition**

Hollis and similar soils: 55 percent Charlton and similar soils: 35 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### **Typical profile**

H1 - 0 to 14 inches: fine sandy loam H2 - 14 to 18 inches: bedrock

#### Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

#### **Description of Charlton**

#### Setting

Parent material: Till

#### **Typical profile**

H1 - 0 to 13 inches: fine sandy loam
H2 - 13 to 36 inches: fine sandy loam
H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Not named

Percent of map unit: 5 percent

Hydric soil rating: No

#### **Buxton**

Percent of map unit: 5 percent

Hydric soil rating: No

#### HcC—Hollis-Charlton fine sandy loams, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7k

Elevation: 0 to 1,080 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Farmland of local importance

#### **Map Unit Composition**

Hollis and similar soils: 55 percent Charlton and similar soils: 35 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: fine sandy loam H2 - 14 to 18 inches: bedrock

#### **Properties and qualities**

Slope: 8 to 15 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of pondina: None

Available water capacity: Very low (about 2.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

#### **Description of Charlton**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 13 inches: fine sandy loam
H2 - 13 to 36 inches: fine sandy loam
H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Not named

Percent of map unit: 5 percent

Hydric soil rating: No

#### Buxton

Percent of map unit: 5 percent

#### HdB—Hollis-Charlton very rocky fine sandy loams, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7m

Elevation: 0 to 1,000 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hollis and similar soils: 40 percent Charlton and similar soils: 30 percent Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Settina

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: very stony fine sandy loam

H2 - 14 to 18 inches: bedrock

#### **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

#### **Description of Charlton**

#### Settina

Parent material: Till

#### Typical profile

H1 - 0 to 13 inches: very stony fine sandy loam

H2 - 13 to 36 inches: fine sandy loam H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Rock outcrop

Percent of map unit: 10 percent

Hydric soil rating: No

#### Not named

Percent of map unit: 5 percent

Hydric soil rating: No

#### Sutton

Percent of map unit: 5 percent

Hydric soil rating: No

#### **Buxton**

Percent of map unit: 5 percent

Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent Landform: Depressions

Hydric soil rating: Yes

# HdC—Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7n Elevation: 0 to 1,200 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hollis and similar soils: 40 percent Charlton and similar soils: 30 percent Minor components: 30 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: very stony fine sandy loam

H2 - 14 to 18 inches: bedrock

#### **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained

Runoff class: Very high Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

#### **Description of Charlton**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 13 inches: very stony fine sandy loam

H2 - 13 to 36 inches: fine sandy loam H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Rock outcrop

Percent of map unit: 10 percent

Hydric soil rating: No

#### Not named

Percent of map unit: 10 percent

Hydric soil rating: No

#### Woodbridge

Percent of map unit: 5 percent

Hydric soil rating: No

#### Sutton

Percent of map unit: 5 percent

# HeD—Hollis-Charlton extremely rocky fine sandy loams, 8 to 25 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7q Elevation: 0 to 1,180 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hollis and similar soils: 30 percent Charlton and similar soils: 25 percent Minor components: 45 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 14 inches: extremely stony fine sandy loam

H2 - 14 to 18 inches: bedrock

#### **Properties and qualities**

Slope: 8 to 25 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

#### **Description of Charlton**

#### Setting

Parent material: Till

#### Typical profile

H1 - 0 to 13 inches: extremely stony fine sandy loam

H2 - 13 to 36 inches: fine sandy loam
H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 8 to 25 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Rock outcrop

Percent of map unit: 25 percent

Hydric soil rating: No

#### Not named

Percent of map unit: 10 percent

Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent

Landform: Depressions Hydric soil rating: Yes

#### **Sutton**

Percent of map unit: 5 percent

#### Sb—Saugatuck loamy sand

#### Map Unit Setting

National map unit symbol: 9d8r Elevation: 300 to 1,000 feet

Mean annual precipitation: 27 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 125 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Saugatuck and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Saugatuck**

#### Setting

Landform: Outwash terraces
Parent material: Outwash

#### Typical profile

H1 - 0 to 4 inches: loamy sand H2 - 4 to 7 inches: sand

H3 - 7 to 26 inches: loamy sand H4 - 26 to 42 inches: sand

#### Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 10 to 16 inches to undefined

Drainage class: Poorly drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 1.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D Hydric soil rating: Yes

#### **Minor Components**

#### Not named wet

Percent of map unit: 15 percent

Landform: Outwash terraces Hydric soil rating: Yes

#### SfC—Suffield silt loam, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d8v

Elevation: 0 to 250 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Suffield and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Suffield**

#### **Typical profile**

H1 - 0 to 19 inches: silt loam H2 - 19 to 28 inches: silt loam H3 - 28 to 41 inches: silty clay

#### **Properties and qualities**

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

high (0.00 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 7.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hvdrologic Soil Group: C

Ecological site: F144AY017NH - Well Drained Lake Plain

Hydric soil rating: No

#### **Minor Components**

#### Not named

Percent of map unit: 9 percent

#### **Buxton**

Percent of map unit: 5 percent Hydric soil rating: No

#### **Rock outcrop**

Percent of map unit: 1 percent Hydric soil rating: No

#### W-Water

#### **Map Unit Composition**

Water (less than 40 acres): 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

## WfB—Windsor loamy fine sand, clay subsoil variant, 0 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 9d9b

Elevation: 0 to 280 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Windsor variant and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Windsor Variant**

#### Typical profile

H1 - 0 to 26 inches: loamy fine sand H2 - 26 to 30 inches: loamy sand H3 - 30 to 42 inches: silt loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20

to 0.60 in/hr)

Depth to water table: About 24 to 36 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 5.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Not named

Percent of map unit: 15 percent

## Soil Information for All Uses

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

#### Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

### **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

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Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:20.000. Area of Interest (AOI) C/D Soils D Warning: Soil Map may not be valid at this scale. Soil Rating Polygons Not rated or not available Α Enlargement of maps beyond the scale of mapping can cause **Water Features** A/D misunderstanding of the detail of mapping and accuracy of soil Streams and Canals line placement. The maps do not show the small areas of В contrasting soils that could have been shown at a more detailed Transportation scale. B/D Rails ---Interstate Highways Please rely on the bar scale on each map sheet for map C/D **US Routes** measurements. Major Roads Source of Map: Natural Resources Conservation Service Not rated or not available Local Roads Web Soil Survey URL: -Coordinate System: Web Mercator (EPSG:3857) Soil Rating Lines Background Aerial Photography Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Strafford County, New Hampshire Not rated or not available Survey Area Data: Version 20, May 29, 2020 **Soil Rating Points** Soil map units are labeled (as space allows) for map scales Α 1:50.000 or larger. A/D Date(s) aerial images were photographed: Dec 31, 2009—Sep 9. 2017 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

### Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
BzB	Buxton silt loam, 3 to 8 percent slopes	C/D	31.7	33.2%
CsC	Charlton fine sandy loam, 8 to 15 percent slopes, very stony	В	0.8	0.9%
HcB	Hollis-Charlton fine sandy loams, 3 to 8 percent slopes	D	10.0	10.5%
HcC	Hollis-Charlton fine sandy loams, 8 to 15 percent slopes	D	3.0	3.1%
HdB	Hollis-Charlton very rocky fine sandy loams, 3 to 8 percent slopes	D	8.2	8.5%
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	D	0.0	0.0%
HeD	Hollis-Charlton extremely rocky fine sandy loams, 8 to 25 percent slopes		7.5	7.8%
Sb	Saugatuck loamy sand	B/D	0.7	0.7%
SfC	Suffield silt loam, 8 to 15 percent slopes	С	26.9	28.1%
W	Water		4.1	4.3%
WfB	Windsor loamy fine sand, clay subsoil variant, 0 to 8 percent slopes	А	2.7	2.8%
Totals for Area of Inter	est		95.6	100.0%

#### Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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# 1.3 Extreme Precipitation Tables (Northeast Regional Climate Center)

## **Extreme Precipitation Tables**

#### **Northeast Regional Climate Center**

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing No

State New Hampshire

Location

**Longitude** 70.923 degrees West **Latitude** 43.133 degrees North

Elevation 0 feet

**Date/Time** Tue, 20 Oct 2020 14:53:49 -0400

#### **Extreme Precipitation Estimates**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.49	0.66	0.81	1.00	1yr	0.70	0.98	1.13	1.59	2.03	2.61	2.84	1yr	2.31	2.74	3.14	3.86	4.44	1yr
2yr	0.32	0.49	0.61	0.82	1.01	1.19	2yr	0.88	1.17	1.39	1.86	2.41	3.14	3.48	2yr	2.78	3.34	3.84	4.57	5.21	2yr
5yr	0.37	0.57	0.70	0.96	1.23	1.48	5yr	1.06	1.44	1.72	2.32	2.96	3.98	4.46	5yr	3.52	4.29	4.90	5.79	6.55	5yr
10yr	0.41	0.63	0.78	1.10	1.42	1.73	10yr	1.22	1.69	2.02	2.73	3.46	4.76	5.39	10yr	4.21	5.18	5.90	6.92	7.80	10yr
25yr	0.48	0.74	0.91	1.31	1.72	2.14	25yr	1.48	2.09	2.51	3.40	4.26	6.03	6.91	25yr	5.34	6.65	7.53	8.78	9.83	25yr
50yr	0.54	0.83	1.03	1.48	2.00	2.51	50yr	1.72	2.46	2.96	4.01	4.99	7.22	8.36	50yr	6.39	8.04	9.06	10.51	11.72	50yr
100yr	0.62	0.93	1.17	1.69	2.32	2.95	100yr	2.00	2.89	3.48	4.73	5.84	8.64	10.11	100yr	7.65	9.72	10.91	12.58	13.97	100yr
200yr	0.70	1.05	1.33	1.93	2.69	3.48	200yr	2.32	3.40	4.10	5.59	6.84	10.36	12.22	200yr	9.16	11.75	13.14	15.07	16.66	200yr
500yr	0.83	1.24	1.59	2.31	3.29	4.31	500yr	2.84	4.22	5.10	6.97	8.45	13.16	15.72	500yr	11.64	15.12	16.81	19.15	21.05	500yr

#### **Lower Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.24	0.37	0.45	0.60	0.74	0.90	1yr	0.64	0.88	0.91	1.26	1.56	2.02	2.52	1yr	1.79	2.42	2.93	3.27	4.01	1yr
2yr	0.31	0.49	0.60	0.81	1.00	1.18	2yr	0.86	1.16	1.37	1.83	2.36	3.04	3.39	2yr	2.69	3.26	3.74	4.46	5.05	2yr
5yr	0.35	0.54	0.67	0.92	1.16	1.40	5yr	1.01	1.37	1.62	2.15	2.78	3.72	4.14	5yr	3.29	3.98	4.59	5.43	6.14	5yr
10yr	0.38	0.59	0.73	1.02	1.32	1.60	10yr	1.14	1.57	1.82	2.45	3.13	4.30	4.82	10yr	3.80	4.63	5.34	6.30	7.08	10yr
25yr	0.44	0.67	0.83	1.18	1.56	1.91	25yr	1.35	1.87	2.11	2.85	3.66	5.03	5.87	25yr	4.45	5.65	6.54	7.68	8.56	25yr
50yr	0.48	0.74	0.92	1.32	1.77	2.19	50yr	1.53	2.14	2.36	3.20	4.11	5.77	6.81	50yr	5.11	6.55	7.63	8.92	9.87	50yr
100yr	0.54	0.82	1.02	1.48	2.03	2.51	100yr	1.75	2.45	2.64	3.59	4.60	6.60	7.89	100yr	5.84	7.59	8.91	10.35	11.35	100yr
200yr	0.60	0.90	1.15	1.66	2.31	2.87	200yr	2.00	2.80	2.94	4.01	5.14	7.55	9.15	200yr	6.68	8.80	10.41	12.02	13.08	200yr
500yr	0.70	1.05	1.34	1.95	2.78	3.45	500yr	2.40	3.37	3.42	4.65	5.98	8.99	11.12	500yr	7.95	10.69	12.80	14.67	15.72	500yr

### **Upper Confidence Limits**

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.43	0.53	0.71	0.87	1.08	1yr	0.75	1.05	1.24	1.75	2.22	2.84	3.03	1yr	2.51	2.91	3.38	4.18	4.78	1yr
2yr	0.33	0.51	0.62	0.84	1.04	1.25	2yr	0.90	1.22	1.48	1.95	2.50	3.26	3.58	2yr	2.88	3.44	3.95	4.71	5.40	2yr
5yr	0.39	0.60	0.75	1.03	1.31	1.58	5yr	1.13	1.55	1.85	2.50	3.19	4.23	4.77	5yr	3.74	4.59	5.22	6.16	6.93	5yr
10yr	0.46	0.70	0.87	1.21	1.57	1.92	10yr	1.35	1.88	2.23	3.04	3.84	5.21	5.94	10yr	4.61	5.71	6.48	7.56	8.45	10yr
25yr	0.55	0.84	1.05	1.50	1.97	2.48	25yr	1.70	2.42	2.87	3.96	4.93	7.05	7.95	25yr	6.24	7.65	8.59	9.94	11.01	25yr
50yr	0.64	0.97	1.21	1.74	2.34	2.99	50yr	2.02	2.92	3.48	4.83	5.99	8.73	9.93	50yr	7.73	9.55	10.65	12.21	13.47	50yr
100yr	0.74	1.12	1.41	2.03	2.79	3.61	100yr	2.40	3.53	4.23	5.91	7.27	10.81	12.40	100yr	9.57	11.92	13.19	15.02	16.48	100yr
200yr	0.86	1.29	1.64	2.37	3.31	4.38	200yr	2.86	4.28	5.14	7.23	8.81	13.43	15.50	200yr	11.88	14.91	16.34	18.47	20.19	200yr
500yr	1.05	1.56	2.01	2.92	4.15	5.63	500yr	3.58	5.50	6.63	9.47	11.40	17.92	20.82	500yr	15.86	20.02	21.69	24.30	26.43	500yr



# SECTION 2.0 - DRAINAGE CALCULATIONS, ANALYSIS & DESIGN

2.1 BMP Worksheets	for all Treatment Sys	stems

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## Stage-Area-Storage for Pond MC45: MC-4500 Chambers

Elevation	Horizontal	Storage	Elevation	Horizontal	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
52.50	3,293	0	53.54	3,293	1,430
52.52	3,293	26	53.56	3,293	1,486
52.54	3,293	53	53.58	3,293	1,543
52.56	3,293	79	53.60	3,293	1,599
52.58	3,293	105	53.62	3,293	1,655
52.60 52.62	3,293 3,293	132 158	53.64 53.66	3,293 3,293	1,712 1,768
52.64	3,293	184	53.68	3,293	1,824
52.66	3,293	211	53.70	3,293	1,881
52.68	3,293	237	53.72	3,293	1,937
52.70	3,293	263	53.74	3,293	1,993
52.72	3,293	290	53.76	3,293	2,049
52.74	3,293	316	53.78	3,293	2,105
52.76	3,293	342	53.80	3,293	2,161
52.78	3,293	369	53.82	3,293	2,217
52.80	3,293	395	53.84	3,293	2,273
52.82	3,293	421	53.86	3,293	2,329
52.84	3,293	448	53.88	3,293	2,385
52.86	3,293	474	53.90	3,293	2,441
52.88	3,293	501	53.92	3,293	2,497
52.90	3,293	527	53.94	3,293	2,553
52.92	3,293	553	53.96	3,293	2,609
52.94	3,293	580	53.98	3,293	2,665
52.96 52.98	3,293 3,293	606 632	54.00 54.02	3,293 3,293	2,721 2,776
53.00	3,293	659	54.04	3,293	2,832
53.02	3,293	685	54.06	3,293	2,888
53.04	3,293	711	54.08	3,293	2,943
53.06	3,293	738	54.10	3,293	2,999
53.08	3,293	764	54.12	3,293	3,055
53.10	3,293	790	54.14	3,293	3,110
53.12	3,293	817	54.16	3,293	3,166
53.14	3,293	843	54.18	3,293	3,221
53.16	3,293	869	54.20	3,293	3,277
53.18	3,293	896	54.22	3,293	3,332
53.20	3,293	922	54.24	3,293	3,388
53.22	3,293	948	54.26	3,293	3,443
53.24	3,293	975	54.28	3,293	3,498
53.26	3,293	1,001	54.30 54.33	3,293	3,554
53.28 53.30	3,293 3,293	1,027 1,054	54.32 54.34	3,293 3,293	3,609 3,664
53.32	3,293	1,080	54.36	3,293	3,719
53.34	3,293	1,106	54.38	3,293	3,774
53.36	3,293	1,133	54.40	3,293	3,830
53.38	3,293	1,159	54.42	3,293	3,885
53.40	3,293	1,185	54.44	3,293	3,940
53.42	3,293	1,212	54.46	3,293	3,995
53.44	3,293	1,238	54.48	3,293	4,050
53.46	3,293	1,264	54.50	3,293	4,105
53.48	3,293	1,291	54.52	3,293	4,159
53.50	3,293	1,317	54.54	3,293	4,214
53.52	3,293	1,374	54.56	3,293	4,269

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#### Stage-Area-Storage for Pond MC45: MC-4500 Chambers (continued)

Elevation (feet)	Horizontal (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Horizontal (sq-ft)	Storage (cubic-feet)
54.58	3,293	4,324	55.62	3,293	7,099
54.60	3,293	4,379	55.64	3,293	7,099 7,151
54.62	3,293	4,433	55.66	3,293	7,101
54.64	3,293	4,488	55.68	3,293	7,254
54.66	3,293	4,542	55.70	3,293	7,305
54.68	3,293	4,597	55.72	3,293	7,357
54.70	3,293	4,651	55.74	3,293	7,408
54.72	3,293	4,706	55.76	3,293	7,459
54.74	3,293	4,760	55.78	3,293	7,511
54.76	3,293	4,814	55.80	3,293	7,562
54.78	3,293	4,869	55.82	3,293	7,613
54.80	3,293	4,923	55.84	3,293	7,664
54.82	3,293	4,977	55.86	3,293	7,715
54.84	3,293	5,031	55.88	3,293	7,765
54.86	3,293	5,085	55.90	3,293	7,816
54.88	3,293	5,139	55.92	3,293	7,867
54.90	3,293	5,193	55.94	3,293	7,917
54.92 54.04	3,293	5,247	55.96	3,293	7,968
54.94 54.96	3,293 3,293	5,301 5,355	55.98 56.00	3,293 3,293	8,018 8,060
54.98	3,293 3,293	5,355 5,409	56.02	3,293 3,293	8,069 8,119
55.00	3,293	5,463	56.04	3,293	8,169
55.02	3,293	5,516	56.06	3,293	8,219
55.04	3,293	5,570	56.08	3,293	8,269
55.06	3,293	5,624	56.10	3,293	8,319
55.08	3,293	5,677	56.12	3,293	8,369
55.10	3,293	5,731	56.14	3,293	8,418
55.12	3,293	5,784	56.16	3,293	8,468
55.14	3,293	5,837	56.18	3,293	8,518
55.16	3,293	5,891	56.20	3,293	8,567
55.18	3,293	5,944	56.22	3,293	8,616
55.20	3,293	5,997	56.24	3,293	8,666
55.22	3,293	6,050	56.26	3,293	8,715
55.24	3,293	6,103	56.28	3,293	8,764
55.26	3,293	6,156	56.30	3,293	8,813
55.28	3,293	6,209	56.32	3,293	8,862
55.30 55.32	3,293 3,293	6,262	56.34 56.36	3,293 3,293	8,910
		6,315 6,367			8,959 9,008
55.34 55.36	3,293 3,293	6,367 6,420	56.38 56.40	3,293 3,293	9,056
55.38	3,293	6,473	56.42	3,293	9,104
55.40	3,293	6,525	56.44	3,293	9,153
55.42	3,293	6,578	56.46	3,293	9,201
55.44	3,293	6,630	56.48	3,293	9,249
55.46	3,293	6,683	56.50	3,293	9,297
55.48	3,293	6,735	56.52	3,293	9,345
55.50	3,293	6,787	56.54	3,293	9,392
55.52	3,293	6,839	56.56	3,293	9,440
55.54	3,293	6,891	56.58	3,293	9,487
55.56	3,293	6,943	56.60	3,293	9,535
55.58	3,293	6,995	56.62	3,293	9,582
55.60	3,293	7,047	56.64	3,293	9,629

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#### Stage-Area-Storage for Pond MC45: MC-4500 Chambers (continued)

Elevation (feet)	Horizontal (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Horizontal (sq-ft)	Storage (cubic-feet)
56.66	3,293	9,676	57.70	3,293	11,923
56.68	3,293	9,723	57.70 57.72	3,293	11,923
56.70	3,293	9,770	57.72 57.74	3,293	11,999
56.72	3,293	9,817	57.7 <del>4</del> 57.76	3,293	12,037
56.74	3,293	9,863	57.78	3,293	12,037
56.76	3,293	9,910	57.76 57.80	3,293	12,074
56.78	3,293	9,956	57.82	3,293	12,111
56.80	3,293	10,002	57.84	3,293	12,145
56.82	3,293	10,048	57.86	3,293	12,221
56.84	3,293	10,094	57.88	3,293	12,257
56.86	3,293	10,140	57.90	3,293	12,292
56.88	3,293	10,186	57.92	3,293	12,328
56.90	3,293	10,231	57.94	3,293	12,362
56.92	3,293	10,277	57.96	3,293	12,397
56.94	3,293	10,322	57.98	3,293	12,430
56.96	3,293	10,367	58.00	3,293	12,464
56.98	3,293	10,412	58.02	3,293	12,496
57.00	3,293	10,457	58.04	3,293	12,528
57.02	3,293	10,502	58.06	3,293	12,560
57.04	3,293	10,546	58.08	3,293	12,591
57.06	3,293	10,591	58.10	3,293	12,621
57.08	3,293	10,635	58.12	3,293	12,652
57.10	3,293	10,679	58.14	3,293	12,681
57.12	3,293	10,723	58.16	3,293	12,711
57.14	3,293	10,767	58.18	3,293	12,740
57.16	3,293	10,811	58.20	3,293	12,769
57.18	3,293	10,854	58.22	3,293	12,798
57.20	3,293	10,897	58.24	3,293	12,827
57.22	3,293	10,941	58.26	3,293	12,855
57.24	3,293	10,984	58.28	3,293	12,884
57.26	3,293	11,027	58.30	3,293	12,912
57.28	3,293	11,069	58.32	3,293	12,940
57.30	3,293	11,112	58.34	3,293	12,968
57.32	3,293	11,154	58.36	3,293	12,996
57.34	3,293	11,196	58.38	3,293	13,024
57.36	3,293	11,238	58.40	3,293	13,051
57.38	3,293	11,280	58.42	3,293	13,079
57.40	3,293	11,322	58.44	3,293	13,106
57.42	3,293	11,363	58.46	3,293	13,133
57.44	3,293	11,405	58.48	3,293	13,159
57.46	3,293	11,446	58.50	3,293	13,186
57.48	3,293	11,487	58.52	3,293	13,212
57.50	3,293	11,528	58.54	3,293	13,239
57.52	3,293	11,568	58.56	3,293	13,265
57.54	3,293	11,608	58.58	3,293	13,291
57.56	3,293	11,648	58.60	3,293	13,318
57.58 57.60	3,293	11,688	58.62	3,293	13,344
57.60 57.62	3,293	11,728 11,767	58.64	3,293 3,293	13,370
57.62 57.64	3,293 3,293	11,767	58.66 58.68	3,293 3,293	13,397 13,423
57.66	3,293 3,293	11,846	58.70	3,293 3,293	13,449
57.68	3,293	11,884	58.72	3,293	13,449
07.00	0,200	11,004	50.72	5,255	10,470
			1		

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#### Stage-Area-Storage for Pond MC45: MC-4500 Chambers (continued)

Elevation (feet)	Horizontal (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Horizontal (sq-ft)	Storage (cubic-feet)
58.74	3,293	13,502	59.78	3,293	14,503
58.76	3,293	13,528	59.80	3,293	14,503
58.78	3,293	13,555	59.82	3,293	14,503
58.80	3,293	13,581	59.84	3,293	14,503
58.82	3,293	13,607	59.86	3,293	14,503
58.84	3,293	13,634	59.88	3,293	14,503
58.86	3,293	13,660	59.90	3,293	14,503
58.88	3,293	13,686	59.92	3,293	14,503
58.90	3,293	13,713			
58.92	3,293	13,739			
58.94	3,293	13,765			
58.96	3,293	13,792			
58.98	3,293	13,818			
59.00	3,293	13,845			
59.02	3,293	13,871			
59.04	3,293	13,897			
59.06	3,293	13,924			
59.08	3,293	13,950			
59.10	3,293	13,976			
59.12	3,293	14,003			
59.14	3,293	14,029			
59.16	3,293	14,055			
59.18	3,293	14,082			
59.20	3,293	14,108			
59.22	3,293	14,134			
59.24	3,293	14,161			
59.26	3,293	14,187			
59.28	3,293	14,213			
59.30	3,293	14,240			
59.32	3,293	14,266			
59.34	3,293	14,292			
59.36	3,293	14,319			
59.38	3,293	14,345			
59.40	3,293	14,371			
59.42	3,293	14,398			
59.44 59.44	3,293	14,424			
59.46	3,293	14,450			
59.48	3,293	14,477			
59.50	3,293	<b>14,503</b>			
59.52	3,293	14,503			
59.54	3,293	14,503			
59.56	3,293	14,503			
59.58	3,293	14,503			
59.60	3,293	14,503			
59.62	3,293	14,503			
59.64	3,293	14,503			
59.66	3,293	14,503			
59.68	3,293	14,503			
59.70	3,293	14,503			
59.72	3,293	14,503			
59.74	3,293	14,503			
59.76	3,293	14,503			



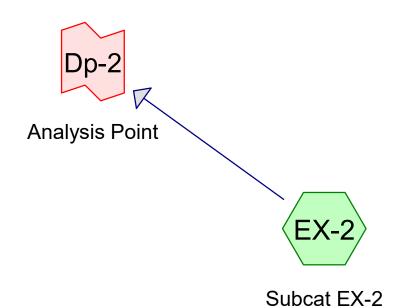
#### 2.2 Pre-development Analysis

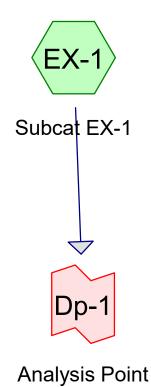
A pre-development analysis covering 128,764 square feet which includes the area to be disturbed by the proposed project. The site has been divided into two pre-development subcatchment area., Subcatchments EX-1 and EX-2 representing the areas draining directly to Drainage Point 1 (Dp-1) and Drainage Point 2 (Dp-2) respectively. EX-1 models area at the front of the site which drains to a point on Main Street, and consists primarily of the existing developed areas at the front of the project site. Drainage Point 2 is in the south of the site, and represents flow toward college brook. EX-2 represents the area draining to Dp-2, and consists primarily of forested slope, but includes a portion of the existing developed area at the north end of the project site.

For more detailed information on the pre-developed area, including watershed areas and drainage paths, see attached drainage plans found in **Section 3** and the HydroCAD area listing found in **Section 2.3.1**. A pre- versus post- development comparison flow rate table for the 1 inch; 2, 10, 25, 50, and 100 year storm events can be found in **Table 1.0** in **Section 1.1.1**.

A High Intensity Soil Survey (HISS) within the work area was completed by Joseph W. Noel, Certified Soil Scientist #017, on October 16, 2020. This information can be found included on the Existing Conditions Plan.

# 2.2.1 Pre Development Diagram, Area Listing, Soil Listing













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#### **Area Listing (selected nodes)**

Area (sq-ft)	CN	Description (subcatchment-numbers)
6,205	61	>75% Grass cover, Good, HSG B (EX-1)
1,321	74	>75% Grass cover, Good, HSG C (EX-1, EX-2)
9,052	80	>75% Grass cover, Good, HSG D (EX-1, EX-2)
508	98	Existing Concrete Pads, HSG C (EX-2)
223	98	Existing Concrete Pads, HSG D (EX-1, EX-2)
25	98	Existing Decks and Steps, HSG B (EX-1)
6	98	Existing Decks and Steps, HSG C (EX-2)
493	98	Existing Decks and Steps, HSG D (EX-1, EX-2)
227	98	Paved parking, HSG B (EX-1)
2,767	98	Paved parking, HSG C (EX-2)
17,991	98	Paved parking, HSG D (EX-1, EX-2)
767	98	Roofs, HSG B (EX-1)
3,732	98	Roofs, HSG D (EX-1, EX-2)
18,332	55	Woods, Good, HSG B (EX-1)
65,194	70	Woods, Good, HSG C (EX-1)
1,919	77	Woods, Good, HSG D (EX-1)

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#### Soil Listing (selected nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
0	HSG A	
25,556	HSG B	EX-1
69,797	HSG C	EX-1, EX-2
33,411	HSG D	EX-1, EX-2
0	Other	

## 2.2.2 Pre-Development Node Listing for the 2, 10, 25, 50, and 100 Year Storm Events

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=0.01"

Flow Length=653' Tc=11.0 min CN=72 Runoff=0.00 cfs 118 cf

Subcatchment EX-2: Subcat EX-2 Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=0.45"

Flow Length=154' Tc=6.0 min CN=93 Runoff=0.13 cfs 408 cf

Link Dp-1: Analysis Point Inflow=0.00 cfs 118 cf

Primary=0.00 cfs 118 cf

Link Dp-2: Analysis Point Inflow=0.13 cfs 408 cf

Primary=0.13 cfs 408 cf

Total Runoff Area = 128,764 sf Runoff Volume = 526 cf Average Runoff Depth = 0.05" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=0.89"

Flow Length=653' Tc=11.0 min CN=72 Runoff=2.17 cfs 8,769 cf

Subcatchment EX-2: Subcat EX-2 Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=2.39"

Flow Length=154' Tc=6.0 min CN=93 Runoff=0.66 cfs 2,166 cf

Link Dp-1: Analysis Point Inflow=2.17 cfs 8,769 cf

Primary=2.17 cfs 8,769 cf

Link Dp-2: Analysis Point Inflow=0.66 cfs 2,166 cf

Primary=0.66 cfs 2,166 cf

Total Runoff Area = 128,764 sf Runoff Volume = 10,935 cf Average Runoff Depth = 1.02" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=2.01"

Flow Length=653' Tc=11.0 min CN=72 Runoff=5.29 cfs 19,792 cf

Subcatchment EX-2: Subcat EX-2 Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=3.96"

Flow Length=154' Tc=6.0 min CN=93 Runoff=1.07 cfs 3,593 cf

Link Dp-1: Analysis Point Inflow=5.29 cfs 19,792 cf

Primary=5.29 cfs 19,792 cf

Link Dp-2: Analysis Point Inflow=1.07 cfs 3,593 cf

Primary=1.07 cfs 3,593 cf

Total Runoff Area = 128,764 sf Runoff Volume = 23,385 cf Average Runoff Depth = 2.18" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=3.02"

Flow Length=653' Tc=11.0 min CN=72 Runoff=8.03 cfs 29,645 cf

Subcatchment EX-2: Subcat EX-2 Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=5.21"

Flow Length=154' Tc=6.0 min CN=93 Runoff=1.38 cfs 4,727 cf

Link Dp-1: Analysis Point Inflow=8.03 cfs 29,645 cf

Primary=8.03 cfs 29,645 cf

Link Dp-2: Analysis Point Inflow=1.38 cfs 4,727 cf Primary=1.38 cfs 4,727 cf

> Total Runoff Area = 128,764 sf Runoff Volume = 34,372 cf Average Runoff Depth = 3.20" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=4.02"

Flow Length=653' Tc=11.0 min CN=72 Runoff=10.72 cfs 39,463 cf

**Subcatchment EX-2: Subcat EX-2** Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=6.39"

Flow Length=154' Tc=6.0 min CN=93 Runoff=1.68 cfs 5,794 cf

Link Dp-1: Analysis Point Inflow=10.72 cfs 39,463 cf

Primary=10.72 cfs 39,463 cf

Link Dp-2: Analysis Point Inflow=1.68 cfs 5,794 cf Primary=1.68 cfs 5,794 cf

> Total Runoff Area = 128,764 sf Runoff Volume = 45,257 cf Average Runoff Depth = 4.22" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=5.26"

Flow Length=653' Tc=11.0 min CN=72 Runoff=14.01 cfs 51,675 cf

Subcatchment EX-2: Subcat EX-2 Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=7.80"

Flow Length=154' Tc=6.0 min CN=93 Runoff=2.03 cfs 7,072 cf

Link Dp-1: Analysis Point Inflow=14.01 cfs 51,675 cf

Primary=14.01 cfs 51,675 cf

Link Dp-2: Analysis Point Inflow=2.03 cfs 7,072 cf Primary=2.03 cfs 7,072 cf

> Total Runoff Area = 128,764 sf Runoff Volume = 58,746 cf Average Runoff Depth = 5.47" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf

# 2.2.3 Pre-Development Full Summary 10 - Year Storm Event

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX-1: Subcat EX-1 Runoff Area=117,882 sf 15.74% Impervious Runoff Depth=2.01"

Flow Length=653' Tc=11.0 min CN=72 Runoff=5.29 cfs 19,792 cf

Subcatchment EX-2: Subcat EX-2 Runoff Area=10,882 sf 75.28% Impervious Runoff Depth=3.96"

Flow Length=154' Tc=6.0 min CN=93 Runoff=1.07 cfs 3,593 cf

Link Dp-1: Analysis Point Inflow=5.29 cfs 19,792 cf

Primary=5.29 cfs 19,792 cf

Link Dp-2: Analysis Point Inflow=1.07 cfs 3,593 cf

Primary=1.07 cfs 3,593 cf

Total Runoff Area = 128,764 sf Runoff Volume = 23,385 cf Average Runoff Depth = 2.18" 79.23% Pervious = 102,024 sf 20.77% Impervious = 26,741 sf Prepared by Horizons Engineering, Inc.

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#### **Summary for Subcatchment EX-1: Subcat EX-1**

Runoff = 5.29 cfs @ 12.16 hrs, Volume= 19,792 cf, Depth= 2.01"

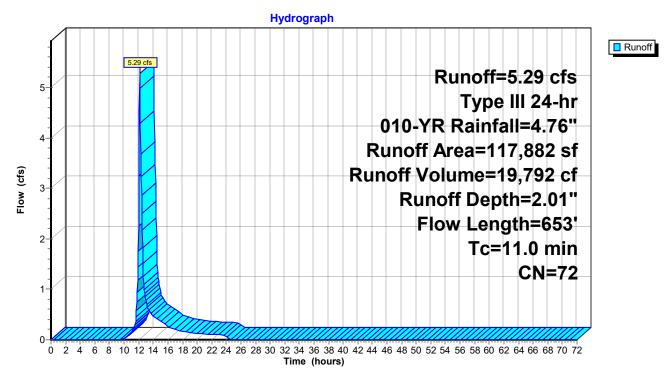
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 010-YR Rainfall=4.76"

A	rea (sf)	CN [	Description								
	6,205	61 >	>75% Gras	s cover, Go	ood, HSG B						
	378	74 >	>75% Gras	s cover, Go	ood, HSG C						
	7,305			5% Grass cover, Good, HSG D							
	193			ncrete Pad							
	25				eps, HSG B						
	395				eps, HSG D						
	227			aved parking, HSG B							
	14,494			ing, HSG D							
	767		Roofs, HSC								
	2,447		Roofs, HSC								
	18,332			od, HSG B							
	65,194			od, HSG C							
	1,919			od, HSG D							
	17,882		Neighted A	•							
	99,333	-		rvious Area							
	18,549	•	15.74% Imp	pervious Ar	ea						
<b>-</b>	1	01	\	0	December 6						
Tc	Length	Slope			Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
5.1	64	0.0435	0.21		Sheet Flow, 1A						
0.5	0.5	0.0004	4.00		Grass: Short n= 0.150 P2= 3.14"						
0.5	35	0.0291	1.28		Sheet Flow, 1B						
0.0	00	0.0500	4.00		Smooth surfaces n= 0.011 P2= 3.14"						
0.3	96	0.0528	4.66		Shallow Concentrated Flow, 2A						
<b>-</b> 4	450	0.0070	4 40		Paved Kv= 20.3 fps						
5.1	458	0.0879	1.48		Shallow Concentrated Flow, 2B						
	050	<b>T</b>			Woodland Kv= 5.0 fps						
11.0	653	Total									

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#### **Subcatchment EX-1: Subcat EX-1**



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#### **Summary for Subcatchment EX-2: Subcat EX-2**

Runoff = 1.07 cfs @ 12.09 hrs, Volume= 3,593 cf, Depth= 3.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 010-YR Rainfall=4.76"

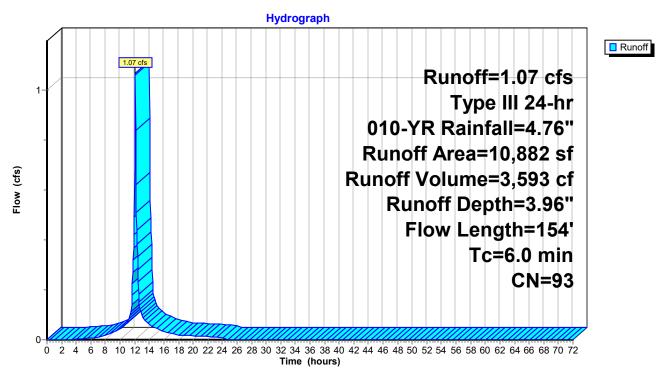
A	rea (sf)	CN [	Description			
	943	74 >75% Grass cover, Good, HSG C				
	1,747	80 >75% Grass cover, Good, HSG D				
	508 98 Existing Concrete Pads, HSG C				s, HSG C	
	30	98 E	98 Existing Concrete Pads, HSG D			
	6	98 E	98 Existing Decks and Steps, HSG C			
	97	98 Existing Decks and Steps, HSG D				
	2,767	98 Paved parking, HSG C				
	3,498		1 0,			
	1,285	98 Roofs, HSG D				
	10,882	882 93 Weighted Average				
	2,690 24.72% Pervious Area					
	8,192	7	'5.28% lmp	pervious Ar	ea	
Tc	Length	Slope	•		Description	
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)		
8.0	14	0.2021	0.29		Sheet Flow, 1A	
					Grass: Short n= 0.150 P2= 3.14"	
0.6	140	0.0374	3.93		Shallow Concentrated Flow, 2A	
					Paved Kv= 20.3 fps	
4.6					Direct Entry, CORRECT TO TR-55 MIN.	
6.0	154	Total				

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#### **Subcatchment EX-2: Subcat EX-2**



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Inflow
□ Primary

#### **Summary for Link Dp-1: Analysis Point**

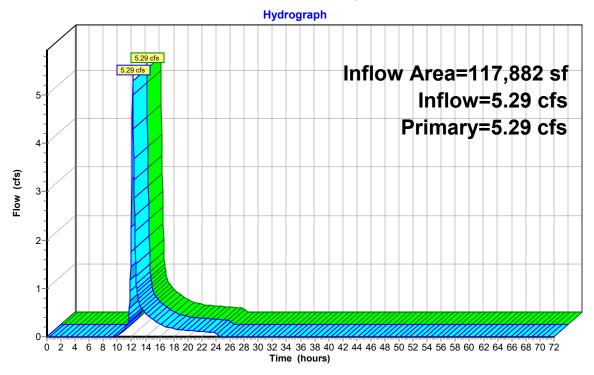
Inflow Area = 117,882 sf, 15.74% Impervious, Inflow Depth = 2.01" for 010-YR event

Inflow = 5.29 cfs @ 12.16 hrs, Volume= 19,792 cf

Primary = 5.29 cfs @ 12.16 hrs, Volume= 19,792 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

#### **Link Dp-1: Analysis Point**



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Inflow
□ Primary

#### **Summary for Link Dp-2: Analysis Point**

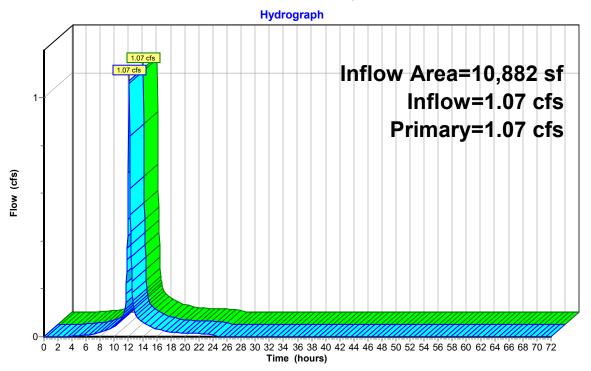
Inflow Area = 10,882 sf, 75.28% Impervious, Inflow Depth = 3.96" for 010-YR event

Inflow = 1.07 cfs @ 12.09 hrs, Volume= 3,593 cf

Primary = 1.07 cfs @ 12.09 hrs, Volume= 3,593 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

#### **Link Dp-2: Analysis Point**



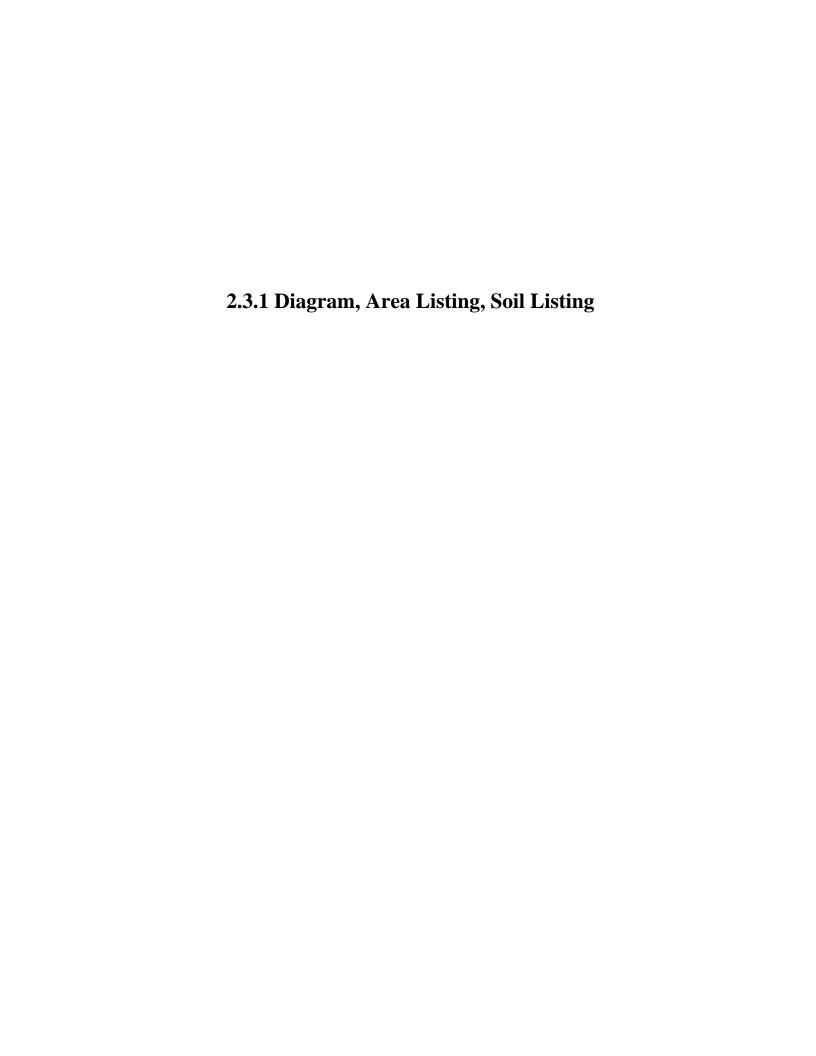


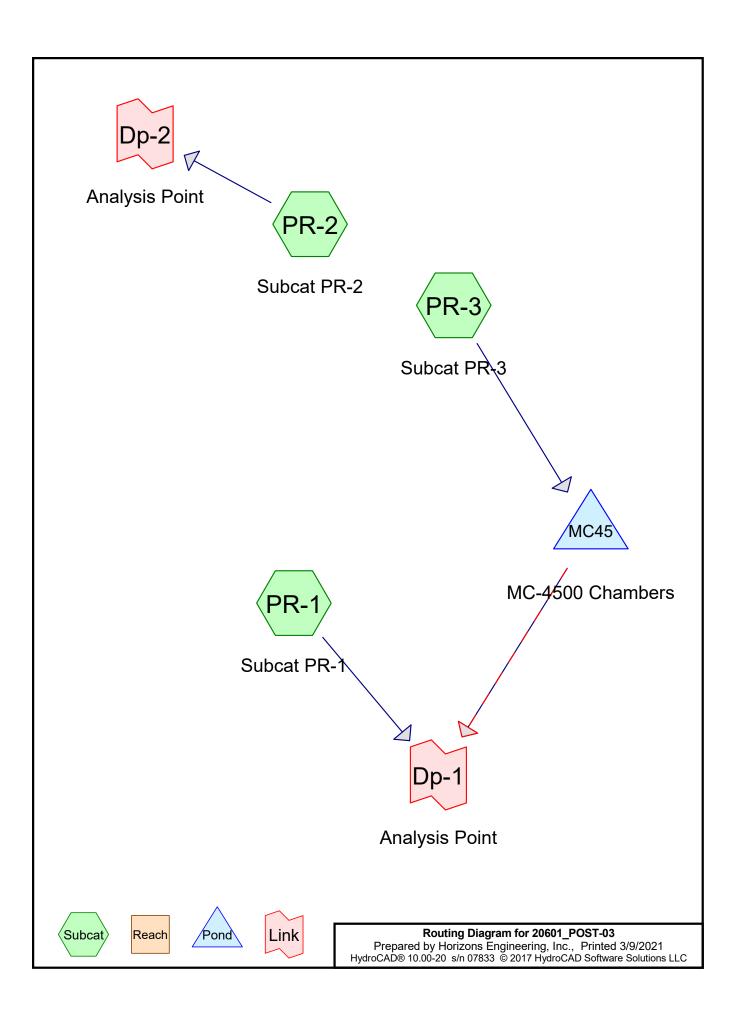
#### 2.3 Post-Development Analysis

A post-development analysis covering 129,767 square feet includes the 79,700 square feet of disturbed area within the proposed project site as well as previously developed areas and undisturbed areas. The site has been divided into three post-development subcatchment area., Subcatchments PR-1 and PR-2 representing the areas draining directly to Drainage Point 1 (Dp-1) and Drainage Point 2 (Dp-2) respectively. PR-1 is modified from the pre-development condition by the reconstruction of the site driveway, resulting in a smaller area draining to Dp-1. PR-2 is smaller than the pre-development equivalent, EX-2, due to the exclusion of areas draining to an underground chamber system. A third subcatchment, PR-3, represents this flow contributing to the underground chamber system, and consists primarily of parking lot areas.

Stormwater from the proposed parking area will be conveyed via sheet flow to grass swale islands which lead to catch basins. These catchbasins then direct stormwater into the isolator row of an underground chamber system under the parking lot. The chamber system has been designed to detain a volume greater than the water quality volume. An overflow structure has been designed to maintain water levels within the profile of the chamber system during events up to the 100-year storm event. Orifices within the overflow structure additionally manage peak flow rates out of the system during storm events.

For more detailed information on the post-developed area, see attached drainage plans found in **Section 4** and the HydroCAD area listing found in **Section 3.4.1**. A pre- versus post-development comparison flow rate table for the 1 inch; 2, 10, 25, 50, and 100 year storm events can be found in **Table 1.0** in **Section 1.1.1**.





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## **Area Listing (selected nodes)**

Area (sq-ft)	CN	Description (subcatchment-numbers)
6,263	61	>75% Grass cover, Good, HSG B (PR-1, PR-3)
10,566	74	>75% Grass cover, Good, HSG C (PR-1, PR-2, PR-3)
10,834	80	>75% Grass cover, Good, HSG D (PR-1, PR-2, PR-3)
40	98	Existing Concrete Pads, HSG B (PR-3)
584	98	Existing Concrete Pads, HSG C (PR-2)
3,050	98	Existing Concrete Pads, HSG D (PR-2, PR-3)
6	98	Existing Decks and Steps, HSG C (PR-2)
492	98	Existing Decks and Steps, HSG D (PR-2, PR-3)
17,828	98	Paved parking, HSG B (PR-3)
32,163	98	Paved parking, HSG C (PR-2, PR-3)
15,386	98	Paved parking, HSG D (PR-2, PR-3)
3,732	98	Roofs, HSG D (PR-2, PR-3)
1,424	55	Woods, Good, HSG B (PR-1, PR-3)
27,003	70	Woods, Good, HSG C (PR-1)
175	77	Woods, Good, HSG D (PR-1, PR-3)
129,547	86	TOTAL AREA

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## Soil Listing (selected nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
0	HSG A	_
25,555	HSG B	PR-1, PR-3
70,323	HSG C	PR-1, PR-2, PR-3
33,670	HSG D	PR-1, PR-2, PR-3
0	Other	
129,547		<b>TOTAL AREA</b>

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## **Ground Covers (selected nodes)**

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
0	6,263	10,566	10,834	0	27,663	>75% Grass cover, Good
0	40	584	3,050	0	3,675	Existing Concrete Pads
0	0	6	492	0	499	Existing Decks and Steps
0	17,828	32,163	15,386	0	65,377	Paved parking
0	0	0	3,732	0	3,732	Roofs
0	1,424	27,003	175	0	28,602	Woods, Good
0	25,555	70,323	33,670	0	129,547	<b>TOTAL AREA</b>

## 2.3.2 Post-Development Node Listing for the 2, 10, 25, 50, and 100 Year Storm Events

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PR-1: Subcat PR-1 Runoff Area=38,120 sf 0.00% Impervious Runoff Depth=0.79"

Flow Length=237' Tc=6.0 min CN=70 Runoff=0.71 cfs 2,520 cf

Subcatchment PR-2: Subcat PR-2 Runoff Area=9,503 sf 71.13% Impervious Runoff Depth=2.29"

Flow Length=154' Tc=6.0 min CN=92 Runoff=0.56 cfs 1,816 cf

Subcatchment PR-3: Subcat PR-3 Runoff Area=81,924 sf 81.20% Impervious Runoff Depth=2.49"

Tc=6.0 min CN=94 Runoff=5.14 cfs 16,970 cf

Pond MC45: MC-4500 Chambers Peak Elev=55.56' Storage=6,952 cf Inflow=5.14 cfs 16,970 cf

Discarded=0.11 cfs 10,478 cf Primary=1.78 cfs 6,492 cf Outflow=1.89 cfs 16,970 cf

Link Dp-1: Analysis Point Inflow=2.15 cfs 9,012 cf

Primary=2.15 cfs 9,012 cf

Link Dp-2: Analysis Point Inflow=0.56 cfs 1,816 cf

Primary=0.56 cfs 1,816 cf

Total Runoff Area = 129,547 sf Runoff Volume = 21,306 cf Average Runoff Depth = 1.97" 43.43% Pervious = 56,265 sf 56.57% Impervious = 73,282 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PR-1: Subcat PR-1 Runoff Area=38,120 sf 0.00% Impervious Runoff Depth=1.86"

Flow Length=237' Tc=6.0 min CN=70 Runoff=1.83 cfs 5,909 cf

Subcatchment PR-2: Subcat PR-2 Runoff Area=9,503 sf 71.13% Impervious Runoff Depth=3.86"

Flow Length=154' Tc=6.0 min CN=92 Runoff=0.92 cfs 3,053 cf

Subcatchment PR-3: Subcat PR-3 Runoff Area=81,924 sf 81.20% Impervious Runoff Depth=4.07"

Tc=6.0 min CN=94 Runoff=8.18 cfs 27,795 cf

Pond MC45: MC-4500 Chambers Peak Elev=56.67' Storage=9,701 cf Inflow=8.18 cfs 27,795 cf

Discarded=0.13 cfs 11,702 cf Primary=3.97 cfs 16,093 cf Outflow=4.10 cfs 27,795 cf

Link Dp-1: Analysis Point Inflow=5.28 cfs 22,002 cf

Primary=5.28 cfs 22,002 cf

Link Dp-2: Analysis Point Inflow=0.92 cfs 3,053 cf

Primary=0.92 cfs 3,053 cf

Total Runoff Area = 129,547 sf Runoff Volume = 36,757 cf Average Runoff Depth = 3.40" 43.43% Pervious = 56,265 sf 56.57% Impervious = 73,282 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PR-1: Subcat PR-1 Runoff Area=38,120 sf 0.00% Impervious Runoff Depth=2.83"

Flow Length=237' Tc=6.0 min CN=70 Runoff=2.83 cfs 8,987 cf

Subcatchment PR-2: Subcat PR-2 Runoff Area=9,503 sf 71.13% Impervious Runoff Depth=5.10"

Flow Length=154' Tc=6.0 min CN=92 Runoff=1.19 cfs 4,038 cf

Subcatchment PR-3: Subcat PR-3 Runoff Area=81,924 sf 81.20% Impervious Runoff Depth=5.33"

Tc=6.0 min CN=94 Runoff=10.54 cfs 36,363 cf

Pond MC45: MC-4500 Chambers Peak Elev=57.51' Storage=11,546 cf Inflow=10.54 cfs 36,363 cf

Discarded=0.15 cfs 12,240 cf Primary=5.11 cfs 24,123 cf Outflow=5.26 cfs 36,363 cf

Link Dp-1: Analysis Point Inflow=7.23 cfs 33,109 cf

Primary=7.23 cfs 33,109 cf

Link Dp-2: Analysis Point Inflow=1.19 cfs 4,038 cf

Primary=1.19 cfs 4,038 cf

Total Runoff Area = 129,547 sf Runoff Volume = 49,388 cf Average Runoff Depth = 4.57" 43.43% Pervious = 56,265 sf 56.57% Impervious = 73,282 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PR-1: Subcat PR-1 Runoff Area=38,120 sf 0.00% Impervious Runoff Depth=3.80"

Flow Length=237' Tc=6.0 min CN=70 Runoff=3.82 cfs 12,078 cf

Subcatchment PR-2: Subcat PR-2 Runoff Area=9,503 sf 71.13% Impervious Runoff Depth=6.27"

Flow Length=154' Tc=6.0 min CN=92 Runoff=1.45 cfs 4,967 cf

Subcatchment PR-3: Subcat PR-3 Runoff Area=81,924 sf 81.20% Impervious Runoff Depth=6.51"

Tc=6.0 min CN=94 Runoff=12.73 cfs 44,422 cf

Pond MC45: MC-4500 Chambers Peak Elev=58.43' Storage=13,093 cf Inflow=12.73 cfs 44,422 cf

Discarded=0.16 cfs 12,593 cf Primary=6.11 cfs 31,828 cf Outflow=6.27 cfs 44,422 cf

Link Dp-1: Analysis Point Inflow=9.04 cfs 43,906 cf

Primary=9.04 cfs 43,906 cf

Link Dp-2: Analysis Point Inflow=1.45 cfs 4,967 cf

Primary=1.45 cfs 4,967 cf

Total Runoff Area = 129,547 sf Runoff Volume = 61,466 cf Average Runoff Depth = 5.69" 43.43% Pervious = 56,265 sf 56.57% Impervious = 73,282 sf

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PR-1: Subcat PR-1 Runoff Area=38,120 sf 0.00% Impervious Runoff Depth=5.02"

Flow Length=237' Tc=6.0 min CN=70 Runoff=5.04 cfs 15,944 cf

Subcatchment PR-2: Subcat PR-2 Runoff Area=9,503 sf 71.13% Impervious Runoff Depth=7.68"

Flow Length=154' Tc=6.0 min CN=92 Runoff=1.76 cfs 6,080 cf

Subcatchment PR-3: Subcat PR-3 Runoff Area=81,924 sf 81.20% Impervious Runoff Depth=7.92"

Tc=6.0 min CN=94 Runoff=15.34 cfs 54,060 cf

Pond MC45: MC-4500 Chambers Peak Elev=59.16' Storage=14,055 cf Inflow=15.34 cfs 54,060 cf

Discarded=0.17 cfs 12,930 cf Primary=10.41 cfs 41,130 cf Outflow=10.58 cfs 54,060 cf

Link Dp-1: Analysis Point Inflow=13.82 cfs 57,074 cf

Primary=13.82 cfs 57,074 cf

Link Dp-2: Analysis Point Inflow=1.76 cfs 6,080 cf Primary=1.76 cfs 6,080 cf

> Total Runoff Area = 129,547 sf Runoff Volume = 76,084 cf Average Runoff Depth = 7.05" 43.43% Pervious = 56,265 sf 56.57% Impervious = 73,282 sf

## 2.3.3 Post-Development Full Summary 10 - Year Storm Event

## 20601\_POST-03

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## Pipe Listing (selected nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Diam/Width	Height	Inside-Fill
	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)
1	MC45	53.60	48.50	72.0	0.0708	0.013	24.0	0.0	0.0
2	MC45	58.50	58.92	21.1	-0.0199	0.013	18.0	0.0	0.0

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## **Notes Listing (selected nodes)**

Line#	Node Number	Notes
1	MC45	ADS Stormtech MC4500 chamber system.
2		Exfiltration rate based on published Ksat value (23.2833um/s) for Hollis-Charlton fine sandy loam, converted to in/hr with a 4X factor of safety applied via discharge multiplier.
3		Note: Due to program limitations, 80 chambers are included in this model. 81 chambers are depicted on the project plan. This should make the hydraulic model more conservative.

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PR-1: Subcat PR-1 Runoff Area=38,120 sf 0.00% Impervious Runoff Depth=1.86"

Flow Length=237' Tc=6.0 min CN=70 Runoff=1.83 cfs 5,909 cf

Subcatchment PR-2: Subcat PR-2 Runoff Area=9,503 sf 71.13% Impervious Runoff Depth=3.86"

Flow Length=154' Tc=6.0 min CN=92 Runoff=0.92 cfs 3,053 cf

Subcatchment PR-3: Subcat PR-3 Runoff Area=81,924 sf 81.20% Impervious Runoff Depth=4.07"

Tc=6.0 min CN=94 Runoff=8.18 cfs 27,795 cf

Pond MC45: MC-4500 Chambers Peak Elev=56.67' Storage=9,701 cf Inflow=8.18 cfs 27,795 cf

Discarded=0.13 cfs 11,702 cf Primary=3.97 cfs 16,093 cf Outflow=4.10 cfs 27,795 cf

Link Dp-1: Analysis Point Inflow=5.28 cfs 22,002 cf

Primary=5.28 cfs 22,002 cf

Link Dp-2: Analysis Point Inflow=0.92 cfs 3,053 cf

Primary=0.92 cfs 3,053 cf

Total Runoff Area = 129,547 sf Runoff Volume = 36,757 cf Average Runoff Depth = 3.40" 43.43% Pervious = 56,265 sf 56.57% Impervious = 73,282 sf

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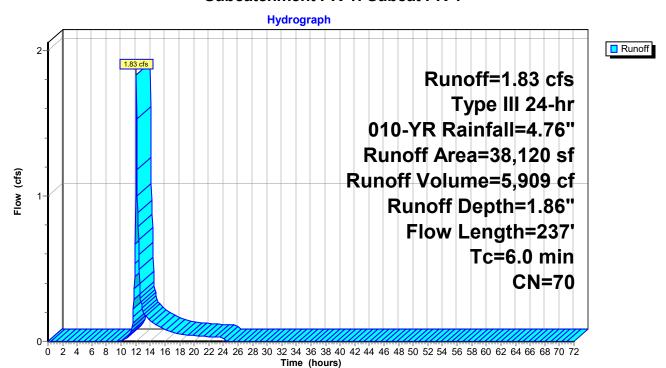
## **Summary for Subcatchment PR-1: Subcat PR-1**

Runoff = 1.83 cfs @ 12.10 hrs, Volume= 5,909 cf, Depth= 1.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 010-YR Rainfall=4.76"

A	rea (sf)	CN [	Description		
	3,221	61 >	75% Gras	s cover, Go	ood, HSG B
	4,620	74 >	75% Gras	s cover, Go	ood, HSG C
	1,709			,	ood, HSG D
	1,416	55 \	Voods, Go	od, HSG B	
	27,003		Voods, Go	,	
	151	77 \	Voods, Go	od, HSG D	
	38,120	70 \	Veighted A	verage	
	38,120	•	100.00% Pe	ervious Are	ea
_				_	
Tc	Length	Slope		Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
2.7	36	0.0479	0.22		Sheet Flow, 1A
					Range n= 0.130 P2= 3.14"
1.8	201	0.1312	1.81		Shallow Concentrated Flow, 2A
					Woodland Kv= 5.0 fps
1.5					Direct Entry, CORRECT TO TR-55 MIN.
6.0	237	Total			

#### **Subcatchment PR-1: Subcat PR-1**



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## **Summary for Subcatchment PR-2: Subcat PR-2**

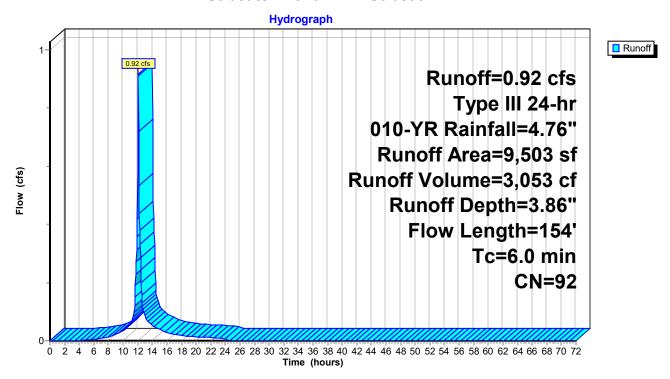
Runoff = 0.92 cfs @ 12.09 hrs, Volume= 3,053 cf, Depth= 3.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 010-YR Rainfall=4.76"

A	rea (sf)	CN [	Description		
	875	74 >	>75% Gras	s cover, Go	ood, HSG C
	1,869	80 >	>75% Gras	s cover, Go	ood, HSG D
	584	98 E	Existing Co	ncrete Pad	s, HSG C
	1,089	98 E	Existing Co	ncrete Pad	s, HSG D
	6				eps, HSG C
	97		_		eps, HSG D
	2,759		•	ing, HSG C	
	1,235		•	ing, HSG D	
	988	98 F	Roofs, HSC	<u> 5 D</u>	
	9,503	92 \	Neighted A	verage	
	2,744	2	28.87% Per	rvious Area	
	6,759	7	71.13% lmp	pervious Ar	ea
_					
Tc	Length	Slope	•	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.8	14	0.2021	0.29		Sheet Flow, 1A
					Grass: Short n= 0.150 P2= 3.14"
0.6	140	0.0374	3.93		Shallow Concentrated Flow, 2A
					Paved Kv= 20.3 fps
4.6					Direct Entry, CORRECT TO TR-55 MIN.
6.0	154	Total			

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#### **Subcatchment PR-2: Subcat PR-2**



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## **Summary for Subcatchment PR-3: Subcat PR-3**

Runoff = 8.18 cfs @ 12.09 hrs, Volume= 27,795 cf, Depth= 4.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 010-YR Rainfall=4.76"

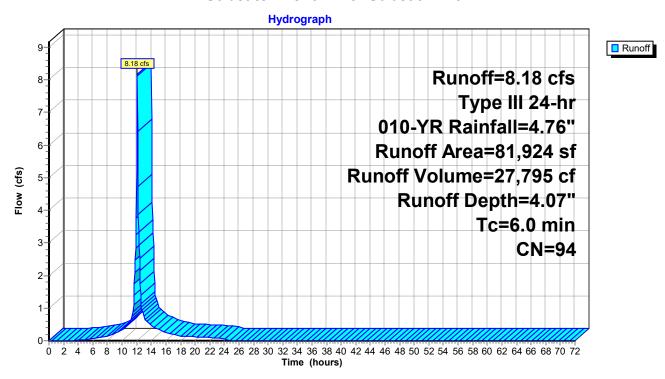
Area	(sf) CN	Description			
3,	042 6	>75% Grass cover, Good, HSG B			
5,	071 74	>75% Grass cover, Good, HSG C			
7,	256 80	>75% Grass cover, Good, HSG D			
	40 98	Existing Concrete Pads, HSG B			
	0 98	Existing Concrete Pads, HSG C			
1,	961 98	Existing Concrete Pads, HSG D			
	395 98	Existing Decks and Steps, HSG D			
17,	828 98	Paved parking, HSG B			
29,	404 98	Paved parking, HSG C			
14,	151 98	Paved parking, HSG D			
2,	744 98	Roofs, HSG D			
	8 5	Woods, Good, HSG B			
	24 7	Woods, Good, HSG D			
81	924 94	Weighted Average			
15.	401	18.80% Pervious Area			
66	523	81.20% Impervious Area			
Tc Le	ength S	pe Velocity Capacity Description			
(min)	(feet) (	(ft) (ft/sec) (cfs)			

6.0

**Direct Entry, TR-55 MINIMUM** 

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#### **Subcatchment PR-3: Subcat PR-3**



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### **Summary for Pond MC45: MC-4500 Chambers**

ADS Stormtech MC4500 chamber system.

Exfiltration rate based on published Ksat value (23.2833um/s) for Hollis-Charlton fine sandy loam, converted to in/hr with a 4X factor of safety applied via discharge multiplier.

Note: Due to program limitations, 80 chambers are included in this model. 81 chambers are depicted on the project plan. This should make the hydraulic model more conservative.

Inflow Area =	81,924 sf, 81.20% Impervious, I	nflow Depth = 4.07" for 010-YR event
Inflow =	8.18 cfs @ 12.09 hrs, Volume=	27,795 cf
Outflow =	4.10 cfs @ 12.24 hrs, Volume=	27,795 cf, Atten= 50%, Lag= 9.2 min
Discarded =	0.13 cfs @ 12.24 hrs, Volume=	11,702 cf
Primary =	3.97 cfs @ 12.24 hrs, Volume=	16,093 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 56.67' @ 12.24 hrs Surf.Area= 3,293 sf Storage= 9,701 cf

Plug-Flow detention time= 257.2 min calculated for 27,795 cf (100% of inflow) Center-of-Mass det. time= 257.0 min (1,031.9 - 774.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	52.50'	5,698 cf	37.58'W x 87.62'L x 7.00'H Field A
			23,050 cf Overall - 8,805 cf Embedded = 14,246 cf x 40.0% Voids
#2A	53.50'	8,805 cf	ADS_StormTech MC-4500 +Cap x 80 Inside #1
			Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf
			Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap
			4 Rows of 20 Chambers
			Cap Storage= +35.7 cf x 2 x 4 rows = 285.6 cf
		14,503 cf	Total Available Storage

#### Storage Group A created with Chamber Wizard

<u>Device</u>	Routing	Invert	Outlet Devices
#1	Discarded	52.50'	3.300 in/hr Exfiltration X 0.25 over Horizontal area
			Conductivity to Groundwater Elevation = 48.67' Phase-In= 0.05'
#2	Device 5	54.95'	20.0" W x 4.0" H Vert. Low Orifice 4"HX20"W C= 0.600
#3	Device 5	55.95'	12.0" W x 2.0" H Vert. Medium Flow 2"Hx12"W C= 0.600
#4	Device 5	58.85'	6.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#5	Primary	53.60'	24.0" Round 24" HDPE outlet
			L= 72.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 53.60' / 48.50' S= 0.0708 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
#6	Device 5	58.92'	18.0" Round 18" BYPASS from CB-100
			L= 21.1' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 58.50' / 58.92' S= -0.0199 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf

#### 20601 POST-03

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**Discarded OutFlow** Max=0.13 cfs @ 12.24 hrs HW=56.67' (Free Discharge) 1=Exfiltration (Controls 0.13 cfs)

Primary OutFlow Max=3.97 cfs @ 12.24 hrs HW=56.67' (Free Discharge)

**-5=24" HDPE outlet** (Passes 3.97 cfs of 21.75 cfs potential flow)

**2=Low Orifice 4"HX20"W** (Orifice Controls 3.33 cfs @ 5.99 fps)

—3=Medium Flow 2"Hx12"W (Orifice Controls 0.64 cfs @ 3.83 fps)

-4=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

**-6=18" BYPASS from CB-100** ( Controls 0.00 cfs)

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#### Pond MC45: MC-4500 Chambers - Chamber Wizard Field A

#### Chamber Model = ADS\_StormTech MC-4500 +Cap (ADS StormTech® MC-4500 with cap volume)

Effective Size= 90.4"W x 60.0"H => 26.46 sf x 4.03'L = 106.5 cf Overall Size= 100.0"W x 60.0"H x 4.33'L with 0.31' Overlap Cap Storage= +35.7 cf x 2 x 4 rows = 285.6 cf

100.0" Wide + 9.0" Spacing = 109.0" C-C Row Spacing

20 Chambers/Row x 4.02' Long +2.56' Cap Length x 2 = 85.62' Row Length +12.0" End Stone x 2 = 87.62' Base Length

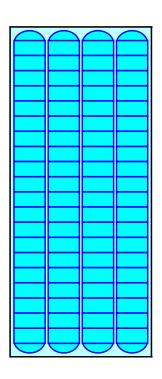
4 Rows x 100.0" Wide + 9.0" Spacing x 3 + 12.0" Side Stone x 2 = 37.58' Base Width 12.0" Base + 60.0" Chamber Height + 12.0" Cover = 7.00' Field Height

80 Chambers x 106.5 cf + 35.7 cf Cap Volume x 2 x 4 Rows = 8,804.8 cf Chamber Storage

23,050.5 cf Field - 8,804.8 cf Chambers = 14,245.7 cf Stone x 40.0% Voids = 5,698.3 cf Stone Storage

Chamber Storage + Stone Storage = 14,503.1 cf = 0.333 af Overall Storage Efficiency = 62.9% Overall System Size = 87.62' x 37.58' x 7.00'

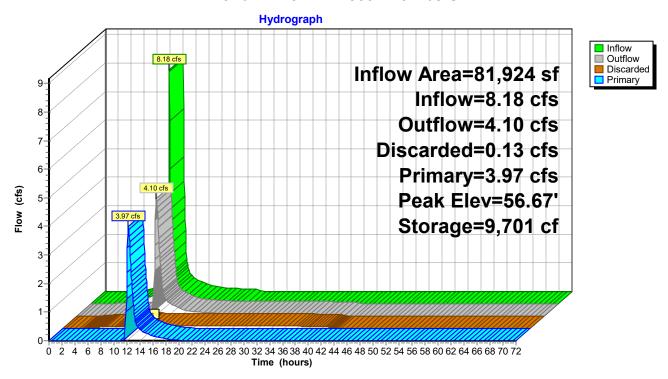
80 Chambers 853.7 cy Field 527.6 cy Stone





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#### Pond MC45: MC-4500 Chambers



Inflow
□ Primary

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## **Summary for Link Dp-1: Analysis Point**

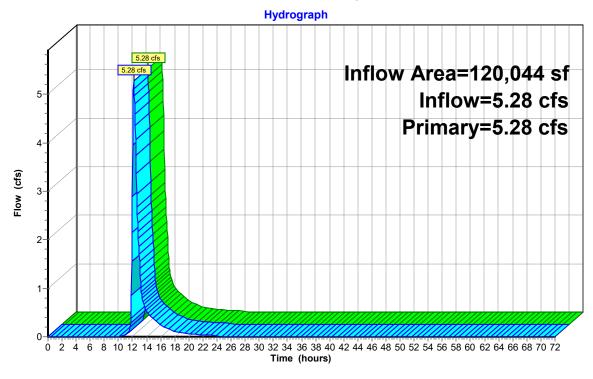
Inflow Area = 120,044 sf, 55.42% Impervious, Inflow Depth = 2.20" for 010-YR event

Inflow = 5.28 cfs @ 12.15 hrs, Volume= 22,002 cf

Primary = 5.28 cfs @ 12.15 hrs, Volume= 22,002 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

## **Link Dp-1: Analysis Point**



Inflow
Primary

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## **Summary for Link Dp-2: Analysis Point**

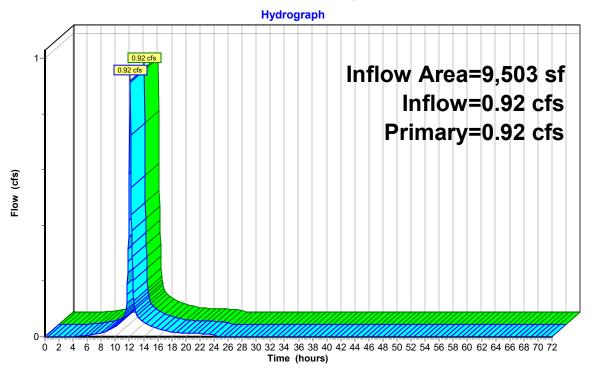
Inflow Area = 9,503 sf, 71.13% Impervious, Inflow Depth = 3.86" for 010-YR event

Inflow = 0.92 cfs @ 12.09 hrs, Volume= 3,053 cf

Primary = 0.92 cfs @ 12.09 hrs, Volume= 3,053 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

#### **Link Dp-2: Analysis Point**



# 2.4 Stone Riprap Calculations (Energy Dissipation – Stability Calculations)

## P-300

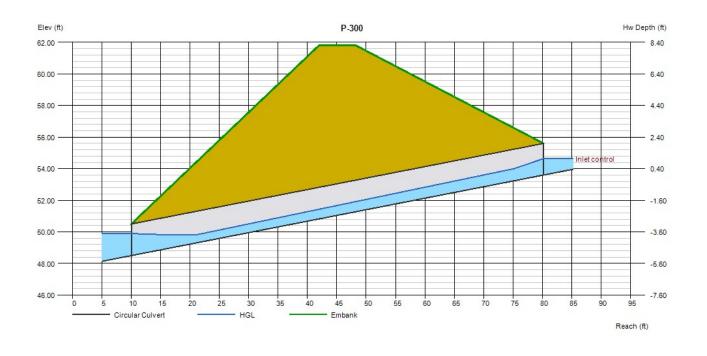
Invert Elev Dn (ft)	= 48.50
Pipe Length (ft)	= 70.20
Slope (%)	= 7.26
Invert Elev Up (ft)	= 53.60
Rise (in)	= 24.0
Shape	= Circular
Span (in)	= 24.0
No. Barrels	= 1
n-Value	= 0.012
Culvert Type	<ul><li>= Circular Concrete</li></ul>
Culvert Entrance	= Square edge w/headwall (C)
Coeff. K,M,c,Y,k	= 0.0098, 2, 0.0398, 0.67, 0.5
Endon di contra	

#### **Embankment**

Top Elevation (ft) = 61.80Top Width (ft) = 6.30Crest Width (ft) = 10.00

Calculations Qmin (cfs)	= 5.06
Qmax (cfs)	= 5.06
Tailwater Elev (ft)	= (dc+D)/2
Highlighted	
Qtotal (cfs)	= 5.06
Qpipe (cfs)	= 5.06
Qovertop (cfs)	= 0.00
Veloc Dn (ft/s)	= 2.16
Veloc Up (ft/s)	= 4.37
HGL Dn (ft)	= 49.90
HGL Up (ft)	= 54.39
Hw Elev (ft)	= 54.64
Hw/D (ft)	= 0.52
Flow Regime	= Inlet Control

DEPTH = HGLdn - INVdn DEPTH = 49.90 - 48.50 DEPTH = 1.40 FT



## **Calculations 25 year storm**

Project: 19 & 21 Main Street

Performed By: CJH

Checked By: 10/28/2020

Apron Length

use **Eq 1**: La = 
$$\frac{1.8 \times Q}{D^{3/2}}$$
 + 7 x D

When Tail water depth at pipe outlet is **greater (>)** than 1/2 the dia. pipe use **Eq 2**: La = 
$$\frac{3 \times Q}{D^{3/2}}$$
 + 7 x D

 $\frac{\text{Apron Width at Outlet}}{\text{Downstream Apron Width}} = 3 \times D \quad \text{Eq3} \text{ or channel bottom width, when there is a well defined channel at pipe outlet}$ 

and the Tailwater Depth is less (<) than the elevation of the center of the pipe use Eq 4

W=3D+La

or if the Tailwater Depth is greater (>) than the elevation of the center of the pipe use Eq 5

W=3D+0.4xLa

Where D= pipe Diameter La= apron length W= apron width

Q=Discharge from pipe CFS Tw=Tailwater

**OUTFALL** Outlet Protection

Channel

CFS Feet Feet (Y or N)

Data: Q=5.06

D=2

Tw=1.4

n

1) Apron Width at Outlet

2) Apron Length

3) Downstream Apron Width

4) Stone Size 
$$d50 = \frac{0.02 \times Q}{Tw \times D}$$

0.06 Feet

#### **Use NHDOT Class C Stone Fill**

## 2.5 Site Specific Soil Survey

Soils included on Existing Conditions plan sheet

2.6 Inspection and Mai	intenance Manual	

## Inspection and Maintenance Plan Toomerfs, LLC – 19 and 21 Main Street Durham, NH

#### **Introduction**

This document is intended to provide a unified procedure for the party (ies) responsible for inspecting and maintaining the stormwater management device(s) that are located within the site development (see Design Plan for the device locations).

## **Responsible Parties**

The ultimate responsibility for complying with this plan rests with the owners of the Property.

Owner's Name: Toomerfs, LLC

Prior to transfer of ownership to another entity the existing owner shall notify DES in writing of such transfer.

Parties assigned to complete inspection and maintenance tasks are presented in the following table:

DEVICE	TASK	PARTY			
22,162	212022	RESPONSIBLE			
Structural Stormwater Devices					
MC-4500 Chamber System	Inspection	OWNER			
	Maintenance	OWNER			
	Reporting	OWNER			
Riprap/Stone Outlet Protections	Inspection	OWNER			
	Maintenance	OWNER			
	Reporting	OWNER			
Grass Lined Swales	Inspection	OWNER			
	Maintenance	OWNER			
	Reporting	OWNER			
Catchbasins and Manholes	Inspection	OWNER			
Catchousins and Mannoles	Maintenance	OWNER			
	Reporting	OWNER			

#### **Frequency of Activities**

The best time to perform inspections is during the onset of rain. To the extent practicable inspections should be timed to coincide with moderate storms that do not have the potential for severe (thunderstorms, etc.) precipitation. The frequency of inspection and maintenance will vary by intensity of use; however the recommended inspection frequency for each feature has been described in the protocol sheets to follow.

Maintenance frequencies will be determined based upon the results of the inspections and if specific maintenance thresholds are observed to have been crossed during inspections.

#### Records

A record of inspection and maintenance activities shall be recorded on the Inspection and Maintenance Log presented following. Records of Inspection and Maintenance Logs shall be made available upon request.

#### **Control of Invasive Plants**

Invasive plants are introduced, alien, or non-native plants, which have been moved by people from their native habitat to a new area. Some exotic plants are imported for human use such as landscaping, erosion control, or food crops. They also can arrive as "hitchhikers" among shipments of other plants, seeds, packing materials, or fresh produce. Some exotic plants become invasive and cause harm by:

- becoming weedy and overgrown;
- killing established shade trees;
- obstructing pipes and drainage systems;
- forming dense beds in water;
- lowering water levels in lakes, streams, and wetlands;
- destroying natural communities;
- promoting erosion on stream banks and hillsides; and
- resisting control except by hazardous chemical.

During maintenance activities, check for the presence of invasive plants and remove in a safe manner as described on the following pages. They should be controlled as described on the following pages.

Year	

## Stormwater BMP Inspection and Maintenance Log

## Toomerfs, LLC – 19 and 21 Main Street Durham, NH

	INSPECTION		FOLLOW UP ACTIVITY	
DEVICE/		Insp.		
LOCATION	Date	Name	Date	Notes/Action Taken
		-		
		<u> </u>		
	<u> </u>	<u>i                                      </u>		

### **CB-** CATCH BASINS

(To include trench drains, drain manholes, and double catchbasins, and drop inlets)



#### Inspection Frequency:

Inspect 2 times per year (spring and fall-after leaf drop) unless otherwise described-maintain features as described below.

- Remove debris from inlets grates.
- If an oily sheen or hydrocarbons are present on the water surface contact your supervisor
  - Skimming/absorbants should be used to remove to the material and disposed of in accordance with state and federal regulations.
- Remove accumulated sediment in sump if sediment has accumulated to ½ sump depth or is within 1 foot below invert out of basin.
  - If sediment has accumulated to pipe invert out, check discharge end of pipe for sediment accumulations and remove sediment from pipe.
  - Note such conditions and increase inspection frequency if it is determined that the loads of sediment to the basin are consistently high.
  - Address source of sediment if possible.
- For drop inlets with no sump sediments will typically only accumulate if there is an obstruction in the downstream culvert and/or culvert outlet. Therefore where sediments are present in structure:
  - Inspect culvert and culvert outlet and remove debris and sediments.
- Do not dispose of catch basin cleanings in wetland areas or within 40 feet of wetland areas- refer to Appendix b; pages B-2 and B-4 in NH DES guidance document <a href="http://des.nh.gov/organization/divisions/water/stormwater/documents/nh\_idde\_sop.pdf">http://des.nh.gov/organization/divisions/water/stormwater/documents/nh\_idde\_sop.pdf</a> to determine where catchbasin cleanings and street sweepings may be disposed of.

## **GS**-GRASS SWALES (Includes grass ditches, grass Pre-Treatment Swales, and grass Treatment Swales)



### Inspection Frequency:

Inspect once per year unless otherwise described.

Grassed channels should be inspected for sediment accumulation, vegetation loss, and presence of invasive species. Maintain features as described below.

- Repairs, including vegetation replacement, should be made based on inspection.
  - Grass Treatment Swales require a relatively flat swale floor (both laterally (side to side), and longitudinally (along their length)) to spread water across the swale floor and slow flows down to enable sediments to settle in the swale. This may create areas of standing water and associated dead spots in the grass.
    - Reseed such areas by scratching in seed and applying mulch matting for areas that exceed 4 ft. in diameter.
    - If reseeding does not work or water is seen ponding for more than 48 hours turf aeration of the swale floor may rejuvenate it.
      - Re-seed and rake out plugs created by aeration activities.
- Remove sediment and debris annually, or more frequently as warranted by inspection.
  - Leaves should be raked from swales to avoid smothering grass.
- Mow vegetated channels at least once a year to control establishment of woody vegetation.
  - It is recommended to cut grass no shorter than 4 inches.
  - Rake/collect grass clippings from swales.

### RR- RIP RAP OUTLET APRONS (To include Rip Rap Channels/Swales)



### <u>Inspection Frequency:</u>

Inspect once per year unless otherwise indicated or if apron is inlet to a stormwater Detention/treatment Pond or Bioretention Area (if so, see DP and BR, respectively). Maintain features as described below.

- Remove debris accumulations if they redirect flow off of the apron or otherwise restrict flow or cause any backflow into the culvert outlet.
- Repair and replace gaps in stone coverage with stone of similar or larger size stone.
  - Refer to design plans for apron dimensions, stone size and any required geotextile underlayment.
  - Be careful not to extend apron into jurisdictional wetland areas or local wetland buffers.
- Ensure that any flared end sections are level to help spread water out onto apron. Relevel if needed.
- Ensure concrete or masonry headwalls are not undermined or have evidence of piping/voids; evidence that flow has bypassed culvert. If voids are found:
  - Check again during storms to determine what has caused voids and contact an engineer if water is flowing around/bypassing culvert.

### **ST**- STORMTECH INFILTRATION CHAMBERS (*To include stormtech isolator rows*)



Photo Credit: Stormtech

### <u>Inspection Frequency:</u>

Isolator Rows shall be inspected immediately after completion of the site construction and cleaned out if necessary. The typical inspection schedule after construction for the Isolator Rows is a minimum of twice a year (spring & fall) - maintain features as described below.

Inspection of the Isolator Row shall involve a visual check using either the inspection ports or the access manholes

- If upon visual inspection of the Isolator Row, it is found that sediment has accumulated to an average depth exceeding 3 inches throughout the length of the Isolator Row, cleanout is required.
- Cleanout of the accumulated material in the Isolator Row should be accomplished by vacuum pumping.
- Cleanout should be performed during dry weather and care should be taken to avoid tearing the fabric in the Isolator Rows.
- A site maintenance log will be kept. This log will record the dates when maintenance tasks were completed, the person who completed the task, and any observations of malfunctions in components of the stormwater management system. Call 1-888-892-2694 to speak with a Technical representative or visit www.stormtech.com.

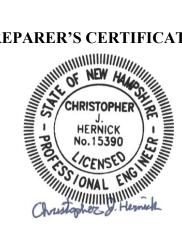
2.7 References
Preparer's Certification
Reviewer's Certification

#### REFERENCES

- Mays, Larry. Stormwater Collection Systems Design Handbook. McGraw-Hill. New York, NY. 2001
- McCarthy, David. Essentials of Soil Mechanics and Foundations: Sixth Edition. Prentice Hall. Columbus, Ohio. 2002.
- NHDES. New Hampshire Stormwater Manual. New Hampshire Department of Environmental Services, 2008.
- NHDES. New Hampshire Homeowner's Guide to Stormwater Management. New Hampshire Department of Environmental Services. 2012
- The UNH Stormwater Center, The LID Stormwater Management Systems Demonstrate LID Stormwater Management Systems Demonstrate Superior Cold Climate Performance than Superior Cold Climate Performance than Conventional Stormwater Management Systems,

UNH Stormwater Center, NEIWPCC 2007 NPS Conference, Newport, RI, May 2007

### PREPARER'S CERTIFICATION



Prepared by Chris Hernick, P.E.



### 3.1 Design Plans

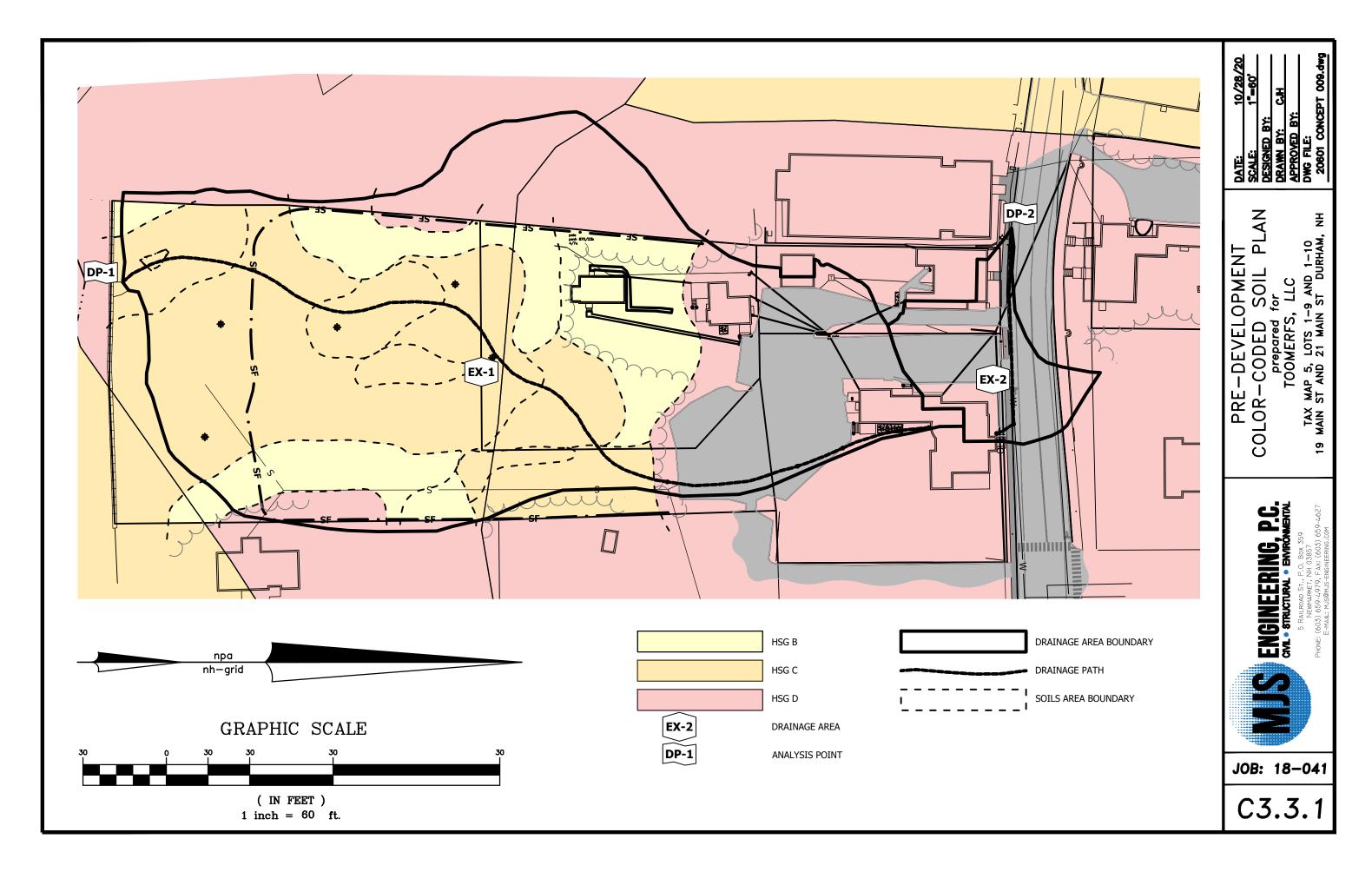
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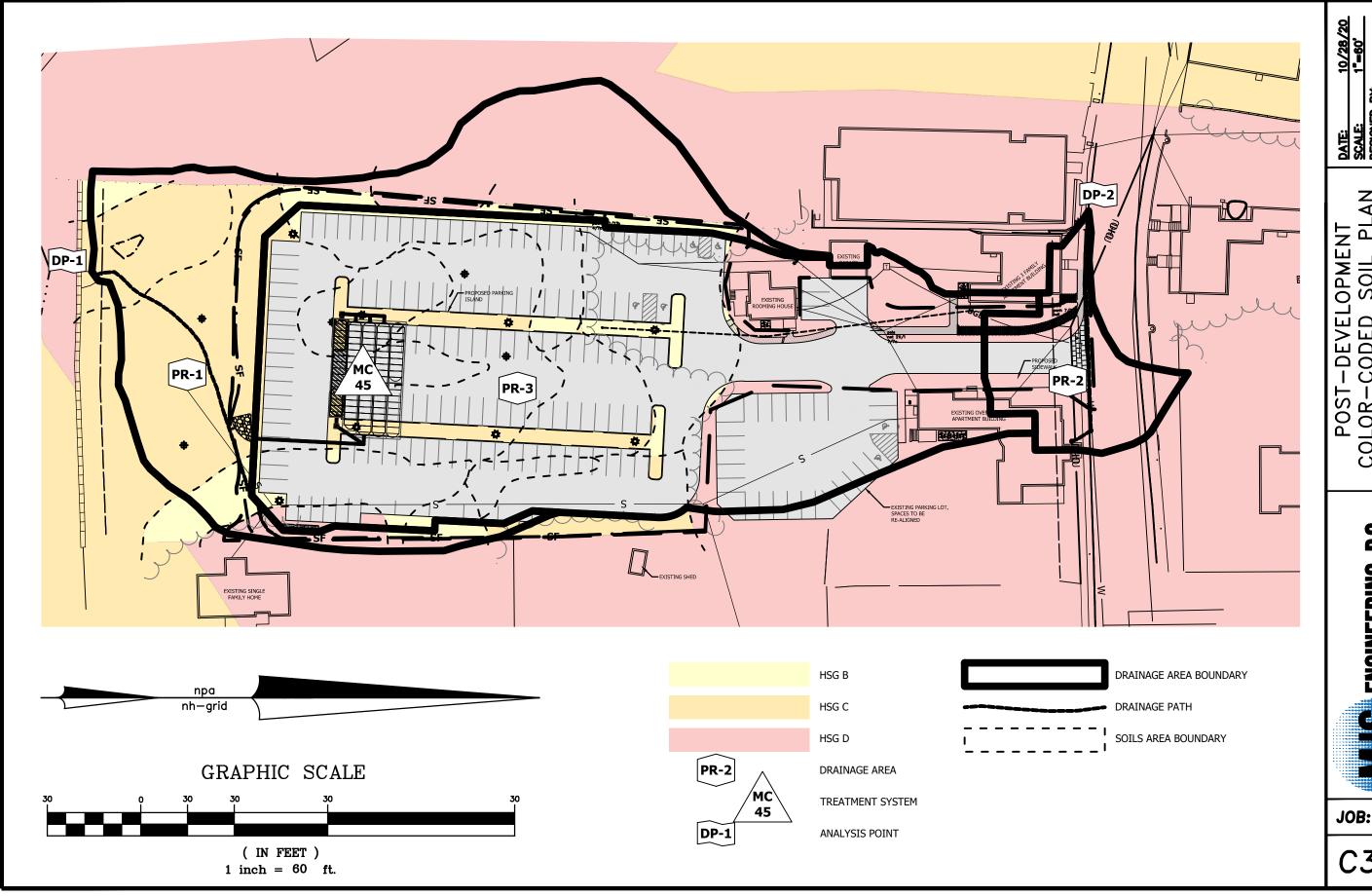
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Wetlands included on Existing Conditions plan sheet

3.3 Color Coded Hydrologic	c Soils Group Plans	





POST-DEVELOPMENT
COLOR-CODED SOIL PLAN
prepared for
TOOMERFS, LLC

TAX MAP 5, LOTS 1-9 AND 1-10 MAIN ST AND 21 MAIN ST DURHAM,

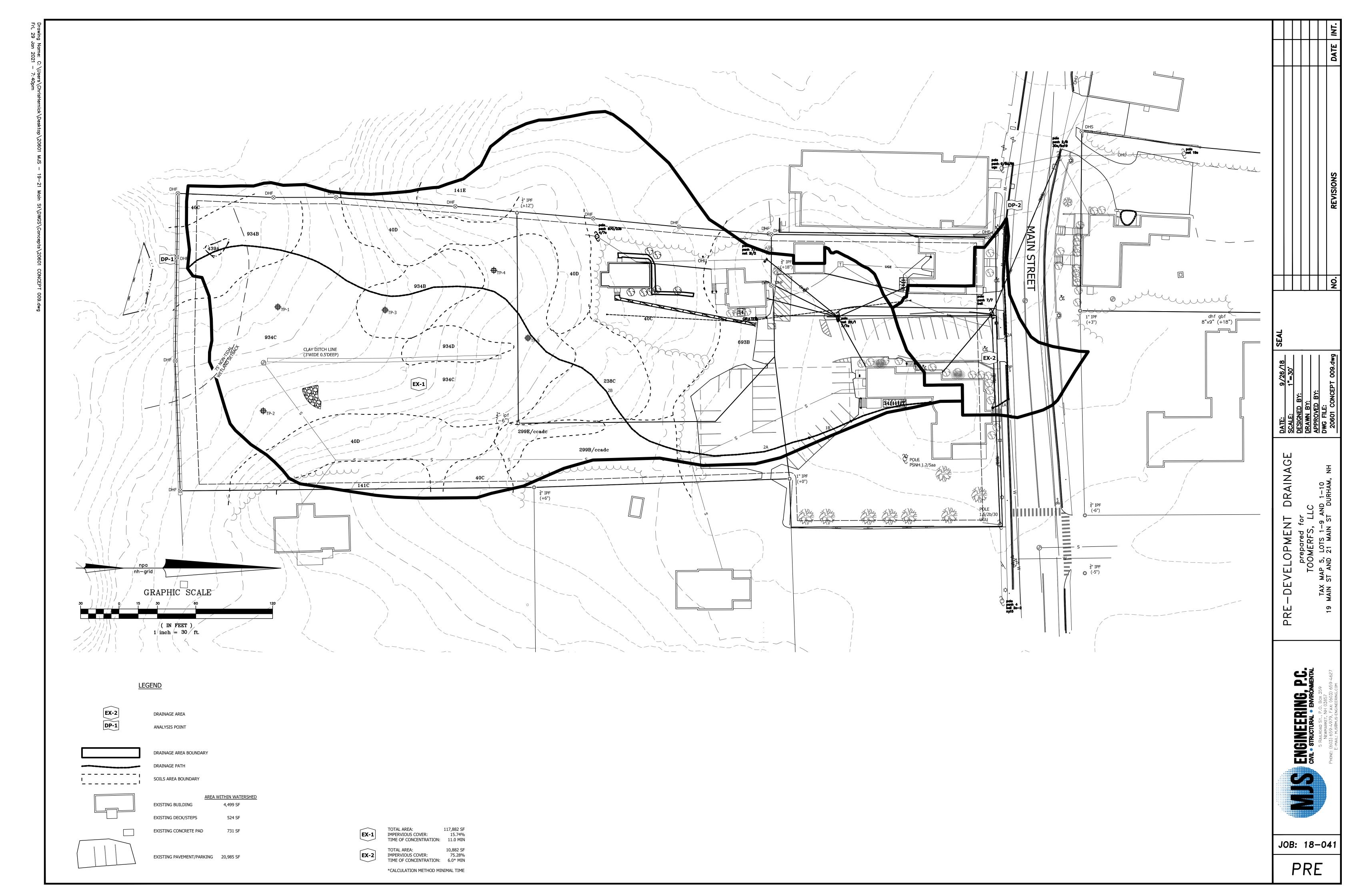
ENGINEERING, P.C. CYAL . STRUCTURAL . ENVIRONMENTAL

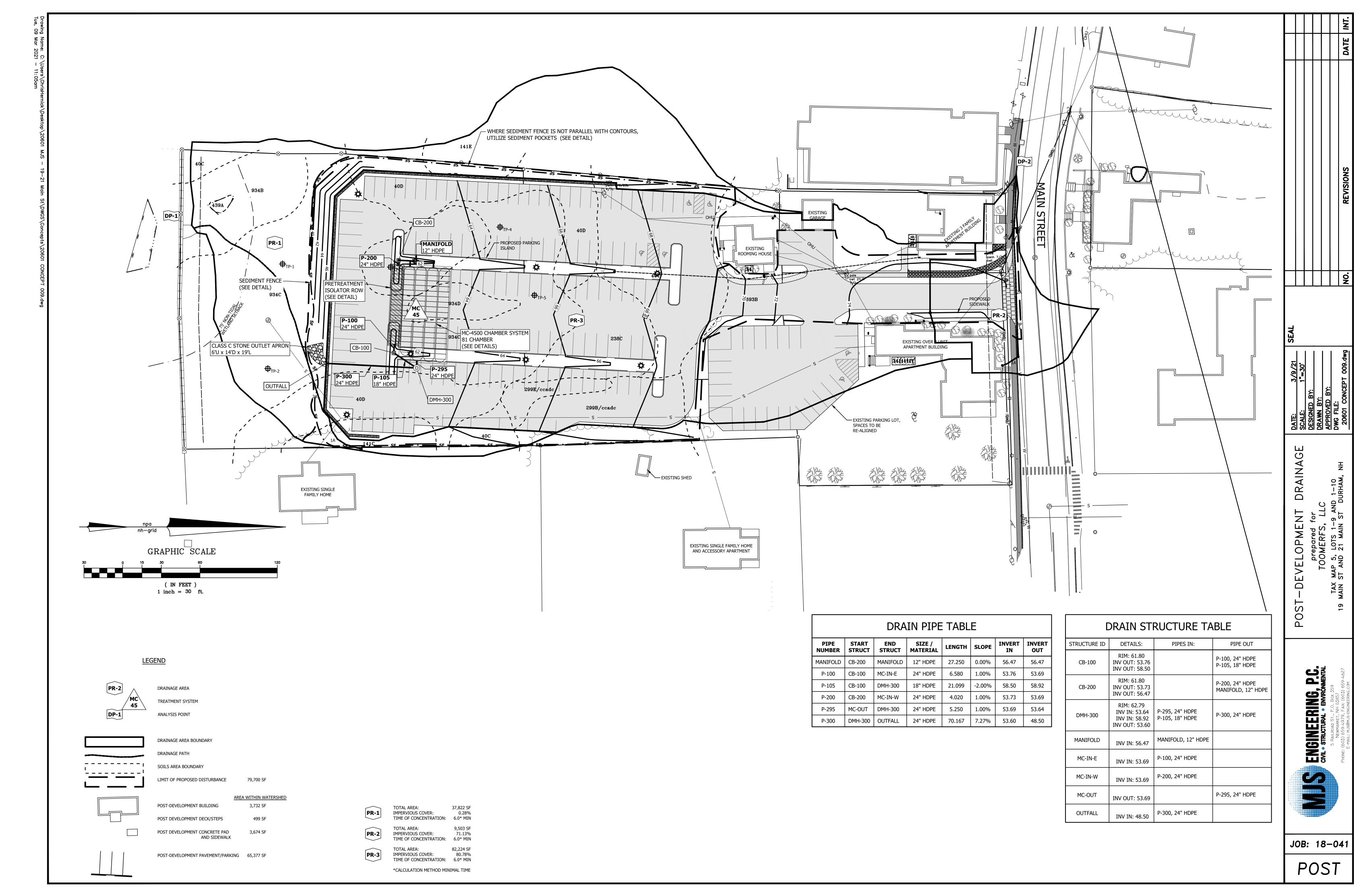


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C3.3.2

3.4 Pre- & Post-Development Drainage Area Plans





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